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Security-constrained optimal energy management system for three-phase residential microgrids



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ABSTRACT

This paper presents a mixed-integer linear programming (MILP) model for the optimal energy management of residential microgrids, modeled as unbalanced, three-phase, electrical distribution system (EDS). Initially, the problem is formulated as a mixed-integer nonlinear programming (MINLP) problem. Then, a set of linear approximations and equivalent mathematical representations are used to obtain a precise MILP model. The proposed formulation considers three-phase generation units (GU), single-phase photovoltaic (PV) resources, and single-phase energy storage systems (ESS), as well as load management. The aim of the proposed model is to minimize the final operational costs of the microgrid while considering operational constraints of the EDS and an unexpected outage of the main grid through a security-constrained set of equations. The optimal solution of the MILP model is found using commercial convex optimization solvers. The proposed model was tested in a residential, three-phase EDS. Results show that the proposed linearizations and approximations produce accurate solutions when compared with a nonlinear three-phase OPF formulation, with an error in the objective function near to 2% and a maximum error in the voltage near to 1%. Efficiency and flexibility of the proposed methodology are also discussed.

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1. Introduction

Microgrids are supervised electrical networks used to energize low voltage loads in a limited, small-scale, geographic area. Besides regular networks, microgrids can be comprised of renewable/nonrenewable generation units (GUs), energy storage systems (ESSs) and controllable loads. Thus, an energy management system (EMS) can be designed to efficiently control and dispatch all resources within the microgrid, in order to optimize active and reactive power injections, voltage profiles, operational costs, and others [1].

Since the management functionalities of a microgrid deal with issues from different technical areas, time scales and infrastructure levels, the hierarchical control scheme has been widely accepted as a standardized solution [2]. In general, the hierarchical control scheme comprises of three different levels: (i) the primary level, responsible for local control of the DERs units; (ii) the secondary level, which deals with primary deviations in variables as

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http://dx.doi.org/10.1016/j.epsr.2017.02.012 0378-7796/© 2017 Elsevier B.V. All rights reserved. frequency and voltage, and (iii) the tertiary level, which is also known as the energy management system, which introduce intelligence to the system to manage and coordinate the operation of optimal power flows [3]. In terms of the structure of the EMS, there are two approaches commonly used in practical applications: centralized and decentralized schemes [4,5]. The difference between these approaches lies in the way they receive and process all the information from the different modules that comprise an EMS.

To provide an optimal schedule, the EMS formulates and solves an energy management (EM) problem, considering load consumption, renewable resources, the operational variables of the electrical distribution system (EDS), energy and thermal costs, and the charging/discharging features of the ESSs [6]. In general, the EM problem schedules the dispatchable generation and storage units in order to achieve economical operation, while guaranteeing that electrical and operational constraints of the system are satisfied. Thus, the EM problem falls into the category of mixed-integer nonlinear programming (MINLP) problems, in which the objective function includes nonlinear terms and binary decision variables, subject to a set of non-convex constraints that represent the EDS operation, and the commitment decisions of the GUs and the ESS.

Several works have addressed the EM problem using MILP and MINLP formulations [7]. In [8], the EM problem of a renewable-

Sets	
F	set of phases, F={A, B, C}
Κ	set of outages of the main grid, $K = \{1, \ldots, T\}$
L	set of circuits
Ν	set of nodes
Т	set of time intervals, $T = \{1, \ldots, T\}$
Indexes	
f, h	phase $f \in F$, and phase $h \in F$
k	outage $k \in K$ of the main grid
mn	circuit $mn \in L$
n, m	nodes $n \in N$ and $m \in N$
S	sth binary variable used for the discretization of the
	SOC
t	time interval $t \in T$
11	main grid's node II = N

- main grid's node $U \in N$ U y yth block used for the piecewise linearization of the GU's quadratic term
- λ th block used for the piecewise linearization of the λ squared circuit currents

Parameters

α_t	cost of energy at time t
α_n^B	investment cost for each ESS at node <i>n</i>
$\alpha^{\ddot{C}}$	load curtailment cost
α_0^G	constant operational cost of the GU
α_1^G	linear operational cost of the GU
α_{2}^{I}	guadratic operational cost of the GU
Δ_t^2	duration of each time interval <i>t</i>
$\bar{\Lambda}_{G}^{G}$	discretization step used for the piecewise lineariza-
-n	tion of each GU's quadratic term at node <i>n</i>
Λ^{S}	length of the interval used for the discretization of
-n	the SOC at node <i>n</i>
$\bar{\delta}_{mn}$	discretization step used for the piecewise lineariza-
omn	tion of each squared current at circuit <i>mn</i>
n^B	efficiency of the FSS
Λ	number of blocks used for the piecewise lineariza-
	tion of the squared circuit currents
σ_{mn}	slope of the λ th block used for the piecewise lin-
mn,A	earization of the squared current at circuit <i>mn</i> and
	block λ
θ_{f}	reference phase angle
$\dot{\theta_1}$	maximum negative deviation of the phase angle
θ_2	maximum positive deviation of the phase angle
ζ	load curtailment percentage
C^B	nominal charge of the ESS
E_n^B	nominal energy of the ESS at node <i>n</i>
\bar{E}_n^B	maximum charging/discharging energy rate of the
	ESS at node <i>n</i>
Īmn	maximum current magnitudes at circuit mn
k ^B , d ^B	parameters related to the costs of the ESS
$m_{n,v}^G$	slope of the yth block used for the piecewise lin-
,5	earization of the GU's quadratic term at node <i>n</i>
MDT_n	minimum off-line time of the GU at node <i>n</i>
MUT _n	minimum on-line time of the GU at node <i>n</i>
$P_{n,t}^{PV}$	active power supplied by the PV at node <i>n</i> , and time
,.	t
$P_{n,f,t}^D$	forecasted active demand at node n, phase f and time
	t
\bar{P}_{n}^{G}	maximum active generation of the GU at node <i>n</i>
\underline{P}_n^G	minimum active generation of the GU at node <i>n</i>
pf_n	minimum power factor of the GU at node <i>n</i>

$Q_{n,f,t}^D$	forecasted reactive demand at node n , phase f and
āc	time t
Q_n^{G}	maximum reactive generation of the GU at node n
$\frac{Q_n^{a}}{D_n}$	minimum reactive generation of the GU at node t
R _{mn,f,h}	resistance of circuit <i>mn</i> between phases <i>f</i> and <i>n</i>
RD_n	ramp-down constraint of the GU at node n
RU _n	ramp-up constraint of the GU at node <i>n</i>
5	number of auxiliary variables used for the dis- cretization of the SOC
SOC _n	minimum SOC of the ESS at node <i>n</i>
\overline{SOC}_{n}^{n}	maximum SOC of the ESS at node <i>n</i>
$\bar{T}_n^{G,ON}$	maximum total on-line time of the GU at node <i>n</i>
T	maximum time interval in the operational period
$V_{n,f,t}^{re*}$	real part of the estimated voltages at node <i>n</i> , phase
1	f and time t
$V_{n,f,t}^{im*}$	imaginary part of the estimated voltages at node <i>n</i> ,
	phase f and time t
\underline{V}	minimum voltage magnitude of the system
\bar{V}	maximum voltage magnitude of the system
$X_{mn,f,h}$	reactance of circuit <i>mn</i> between phases <i>f</i> and <i>h</i>
Y	number of blocks used for the piecewise lineariza-
	tion of the GU's quadratic term
Continu	ous variables
$\delta_{mn}^{im} f_{k} f_{k}$	imaginary part of the λ th block used for the piece-
mm,j,к,t,	wise linearization of the squared current at circuit
	<i>mn</i> , phase <i>f</i> , outage <i>k</i> and time <i>t</i>
δ_{mnfkt}^{re}	imaginary part of the λ th block used for the piece-
пп,j,к,ι,	wise linearization of the squared current at circuit
	<i>mn</i> , phase <i>f</i> , outage <i>k</i> and time <i>t</i>
$\Delta_{n,k,t,v}^{G}$	value of the yth block used for the piecewise lin-
п,к,г,у	earization of the GU's quadratic term at node n ,
	outage k, time t and block y
Φ_{nt-1}^{CH}	variable used to represent the product between $b_{n,t}^{CH}$
,	and $SOC_{n,t-1}$
$\Pi_{n,t}$	variable used to represent the product between
..	$E_{n,t}^{\text{DCH}}$ and $SOC_{n,t}$
$\Psi'_{n,k,t-1}$	variable used to represent the product between
- //	$T_{n,k,t-1}^{G,ON}$ and $u_{n,k,t-1}$
$\Psi_{n,k,t}$	variable used to represent the product between
	$T_{n,k,t-1}^{G,ON}$ and $u_{n,k,t}$
$E_{n,t}^{CH}$	energy of the ESS at node <i>n</i> and time <i>t</i> in charging
	mode
$E_{n,t}^{DCH}$	energy of the ESS at node <i>n</i> and time <i>t</i> in discharging
₽DCH	mode
$E_{n,t,s}^{DCII}$	variable used to consider the sequential corrections
rim	$OI E_{n,t}$
$I_{mn,f,k,t}^{ini}$	imaginary part of the current at circuit <i>mn</i> , phase <i>j</i> , outage <i>k</i> and time <i>t</i> .
JDim	imaginary part of the current demanded at node n
n,f,k,t	nhaginary part of the current demanded at node n_i
I ^{Bim}	imaginary part of the current demanded/supplied
n,J,t	by the FSS at node n phase f and time t
IGim	imaginary part of the current supplied by the GU at
'n,f,k,t	node n phase f outage k and time t
IPVim	imaginary part of the current supplied by the DV at
' n,f,k,t	node n phase f outage k and time t
IUim	imaginary part of the current supplied by the main
1 U,f,k,t	arid at node II phase f outage k and time t
	Sina at noue o, phase J, outage k and time t

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