



# Heat transfer control of micro-thermoelectric gas sensor for breath gas monitoring

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## ARTICLE INFO

### Article history:

Received 14 October 2016

Received in revised form 13 March 2017

Accepted 19 March 2017

Available online 23 March 2017

### Keywords:

Gas sensor

Catalyst

Thermoelectric device

Micro-electromechanical systems (MEMS)

Finite element method (FEM)

## ABSTRACT

A micro-thermoelectric gas sensor (micro-TGS) uses thermoelectric voltage induced by the catalytic combustion of hydrogen or methane for selective gas detection in breath. This is accomplished under an elevated temperature using a micro-heater built on the same membrane as a hotplate, which enables selective combustion of the target gas. A temperature differential built by the catalyst on the membrane induces the offset voltage ( $V_{\text{off}}$ ) of the micro-TGS, which limits the amplifier circuit application. In this study, we strived to suppress  $V_{\text{off}}$  by an additive integration process of heat dissipation dots prepared using  $\alpha\text{-Al}_2\text{O}_3$  paste. In this paper, we discuss the effects of these  $\alpha\text{-Al}_2\text{O}_3$  dots on the thermal balance over the micro-TGS membrane by finite element method (FEM) modeling. When the dots were deposited in a symmetrical position to the combustion catalyst,  $V_{\text{off}}$  was compensated depending on the size, numbers, and locations of the dots. The micro-TGS heat transfer control by the dots was additionally verified by 3-D FEM modeling. The changes in  $V_{\text{off}}$  by the  $\alpha\text{-Al}_2\text{O}_3$  dots in FEM modeling were greater than those of the experiments, suggesting the high thermal conductivity of the micro-TGS membrane. The deviation of the membrane thermal conductivity due to the process non-uniformity significantly influenced the  $V_{\text{off}}$ ; however, it was effectively reduced by the additive integration of dots.

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## 1. Introduction

Medical diagnostic technologies for early disease stages have been widely studied in response to global population aging issues and the expansion of the health care industry. Among these technologies, breath analysis techniques have garnered considerable attention as non-invasive and simple health check methods that can be conducted both at home and in a medical facility. Human breath includes several kinds of inorganic and volatile organic compounds (VOCs). These gases are known as markers of disease and human body metabolism [1,2]. To detect the part-per-million (ppm) levels of breath gases, such as  $\text{H}_2$ , CO, and  $\text{CH}_4$  [3], we developed a unique micro-thermoelectric gas sensor (micro-TGS) with various combustion catalysts for a breath analysis system.

Calorimetric gas sensors take advantage of micro-machined devices using the heat of the chemical reactions generated by cat-

alytic metals. Their thermal characteristics must be optimized for better sensing performance. The micro-TGS uses the catalytic combustion of the gas operated at a catalyst temperature over  $100^\circ\text{C}$  by using a micro-heater built on the membrane. It thereby shows the linear relationship of the voltage signal to the gas concentration [4,5] and the sensing performance for the ppm level of hydrogen in the breath gas analysis [5]. Sensor performance of micro-TGS, a synergistic combination of the catalytic combustion of gas and thermoelectric conversion (from heat to electrical), can be easily modulated by the choice of the combustion catalyst.

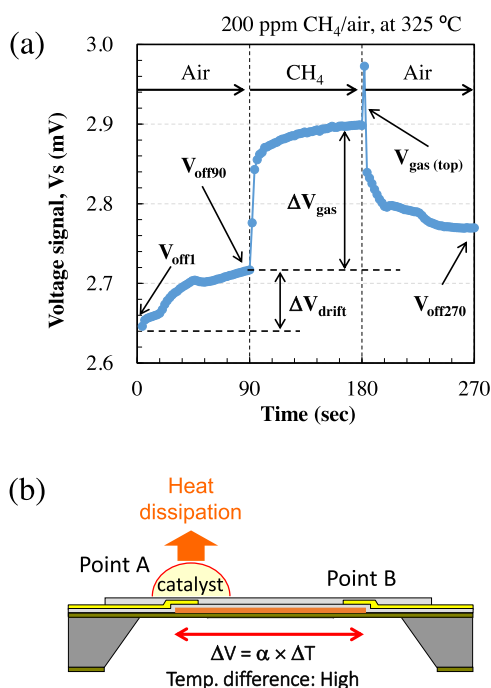
Previously, micro-TGS for  $\text{H}_2$ ,  $\text{CH}_4$ , and CO detection were reported using Pt/ $\alpha\text{-Al}_2\text{O}_3$  [4,5], Pd/ $\theta\text{-Al}_2\text{O}_3$  [6], and Au/ $\text{Co}_3\text{O}_4$  [7] catalysts, respectively. To produce an effective design, the heat balance of the sensor during operation must be estimated. The heat balance can predict the inflammable gas combustion energy of the catalyst. The heat as a function of the sensor output is also important for the development of the catalyst.

The membrane area of the micro-TGS is comprised of ends of thermoelectric SiGe forming a symmetrical pattern. However, one end of the SiGe pattern is covered by a ceramic combustor (combustion catalyst), which induces the asymmetrical temperature

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**Fig. 1.** (a) Voltage signal ( $V_s$ ) of micro-TGS for detection of  $\text{CH}_4$  and (b) schematic illustration of the micro-TGS.

distribution in the membrane and results in the temperature differential, as shown in Fig. 1. Fig. 1(a) depicts an example of a voltage signal of micro-TGS for detection of  $\text{CH}_4$  at  $325\text{ }^\circ\text{C}$ . It indicates a problem of micro-TGS in real applications; i.e., voltage from the sensor from the initial stage in air, named the offset voltage ( $V_{\text{off}}$ ), occurs at a high temperature operation. The fluctuation or drift of the  $V_{\text{off}}$  can also be a serious problem when the target gas concentration is low. The voltage signal was thus gradually elevated after 90 s ( $V_{\text{off}90}$ ) from the initial stage ( $V_{\text{off}1}$ ). This difference of  $V_{\text{off}}$  is shown in  $\Delta V_{\text{drift}}$  in Fig. 1(a). After  $\text{CH}_4$  detection, the voltage continues to rise, and the offset voltage at 270 s ( $V_{\text{off}270}$ ) is higher than that of the initial stage ( $V_{\text{off}1}$ ).

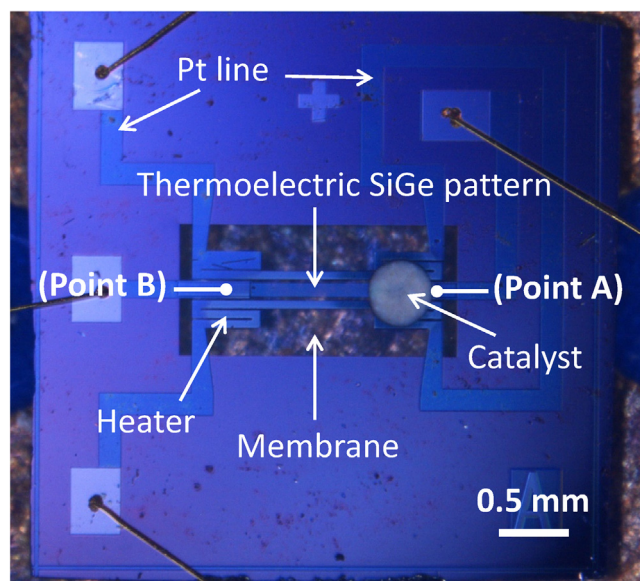
The origin of this problem was an initial temperature difference ( $\Delta T$ ) formed between point A (catalyst site) and point B:

$$V_S = \alpha \cdot \Delta T_{AB} = \alpha \cdot (T_A - T_B) \quad (1)$$

where  $\alpha$  is the Seebeck coefficient of the thermoelectric film. This  $V_{\text{off}}$  of micro-TGS increases in high temperature operation because the combustion catalyst on the membrane plays the role of “heat dissipater” (Fig. 1(b)). In addition, non-uniformity of the membrane in micro-TGS also affects the heat balance inside the membrane.

Generation of this voltage cannot be ignored because the voltage signal increases with the increasing operating temperature. The suppression of offset voltage of micro-TGS is important to stabilize the base voltage and improve the quantitative performance. To make an effective design of each part of micro-TGS, especially the catalyst and micro-heater, meanders are important for optimizing the sensor performance. To make effective design of each parts of micro-TGS, especially a double meander-shaped Pt heater and a circular shape catalyst are important to optimize the sensor performance, and moreover it is important to quantitatively evaluate the heat transfer of these parts.

Optimization of the micro-heater can involve thermal distribution in the membrane that is aimed at temperature control of a uniform and stable response at elevated temperatures, thereby improving the sensor reliability and sensitivity. The development of a theoretical model for thermo-mechanical calculations and heat transfer mechanisms is important for the design of catalytic sen-



**Fig. 2.** Optical image of the micro-TGS.

sors, which can include predicting device process non-uniformity. The influence of the micro-hotplate design on the catalytic reaction or sensor response is not fully understood, the model calculation is expected to be effective tool for the sensor development. Most studies have primarily focused on flowmeters [8], while heat and mass transfer in heated systems [9] and thermochemical devices in gas-fueled combustor systems [10] have additionally been investigated.

In the case of micro-TGS, the heat of gas combustion at the catalyst film which is thin and smaller than 1 mm, is extremely difficult to directly measure. In our previous study, however, we have quantitatively estimated the catalytic combustion heat (power) required for 1 mV of signal voltage to be  $46\text{ }\mu\text{W}$ , using the linear calculation and thermal time constants of the experimental signal curves of the micro-TGS [11]. The design of micro-heater meanders can efficiently and uniformly heat the catalyst; moreover, they can prevent the loss of combustion heat through the heater line. Various heater designs have been tested. The power consumption of the micro-heater meanders was reduced to 30–40 mW at the catalyst temperature of  $100\text{ }^\circ\text{C}$ , which is approximately 30% less than that of the first generation one [12]. In addition, an asymmetric micro-heater meander enabled different catalyst temperatures for a single sensor with a double catalyst structure.

In this study, to control this heat balance and suppress  $V_{\text{off}}$  of micro-TGS, the  $\alpha\text{-Al}_2\text{O}_3$  thick film, dummy dots, for heat dissipation were additively integrated on the membrane of micro-TGS. The effects of the  $\alpha\text{-Al}_2\text{O}_3$  dots on the heat balance are herein described with the quantitative results estimated by 3-D solid modeling of the finite element method (FEM). The effects of thermal conductivity of micro-TGS on the  $V_{\text{off}}$  control by  $\alpha\text{-Al}_2\text{O}_3$  dots are then discussed.

## 2. Experimental

### 2.1. Design of micro-TGS

Details of the preparation procedure of micro-TGS for  $\text{H}_2$  and  $\text{CH}_4$  detection were described in previous reports [4–6]. Here, the p-type B-doped SiGe thermoelectric pattern was used for the micro-TGS device. As shown in Fig. 2, the  $4 \times 4\text{ mm}^2$  dimension of the micro-TGS device was comprised of the thermoelectric pattern, Pt heater, and electrode line pattern on a double-sided polished Si substrate. The optimal geometrical design comprised of the

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