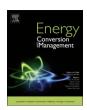
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Efficiency improvement and evaluation of electric hydraulic excavator with speed and displacement variable pump



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ABSTRACT

Hydraulic excavator driven by an internal-combustion engine is widely used in the construction field. However, some problems, such as high pollutant emissions, noise and low efficiency, exist universally. To address these problems, an electric hydraulic excavator configuration combining with an independent metering in and metering out system is proposed to improve the overall energy efficiency. In this paper, a displacement variable pump driven by a speed variable electric motor is used as power source, and a matching method based on the segmented speed and continuous displacement control of the pump is proposed to meet the requirements of high dynamic, high energy efficiency and zero emission of hydraulic excavator under different working conditions. Then, an independent metering in and metering out system is employed to reduce throttling loss. A test rig with a 6-ton hydraulic excavator was built up and used to validate the proposed scheme. The energy consumption characteristics of the electro-hydraulic power source under different rotational speeds and different loads are further investigated to provide analytical and experimental references for control strategy designing. Furthermore, the working performance and energy distributions of the excavator with the pure displacement variable concept, and speed and displacement variable concept are studied comparatively. Results show that, compared with pure displacement variable concept, the electric power consumption during the idle period can be reduced from 2.05 kW to 0.7 kW, the energy saving ratio under partial load condition can be up to 33%, while it is 28.5% under digging condition.

1. Introduction

Nowadays, hydraulic excavator is widely used in the construction field, and there are millions in use in the world, which is about 1.6 million in China in 2015. In the excavator system, a displacement variable pump driven by an internal-combustion engine is normally applied as power source to supply high-pressure oil, and the four-sides spool valves are used to distribute the flow and to control the actuators. However, the energy efficiency of the internal-combustion engine is poor when the load changes in a wide range, which is only about 35% [1], resulting in a huge waste of resources and serious environmental pollutions [2,3]. Besides, the average energy efficiency of the hydraulic system is only about 54%, and the energy efficiency of the whole machine is only about 10% [1]. Thus, energy saving and emission reducing have been the research focuses in the excavator.

For the power transmissions path, there are two approaches to increase the energy efficiency of hydraulic excavator: one is to improve

the matching performance between the load and engine, and the other is to reduce the throttling loss.

In a conventional excavator system, the engine speed of excavator is selected by operator manually according to the excavating job at hand. Usually, there are five operating modes distinguished by the speed. It should be emphasized that load torque is distributed widely for each operating mode. Thus, the engine often works under partial load condition, during which the energy efficiency is poor. Many research efforts have been undertaken to address this issue. A conventional approach is to adjust the engine speed according to load condition [4]. The other is the diesel engine cylinder deactivation technology [5]. However, these two approaches can only improve the economy of the diesel engine in light load. An approach to comprehensively improve the engine efficiency is to add an auxiliary power unit to the system, called the hybrid technology [6–10]. Furthermore, a relatively thorough approach is to use some accumulators to separate the engine from the actuators, allowing optimal engine operation independent of the

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Abbreviations: SVPS, pure speed-variable power source; SDVPS, speed and displacement variable power source; PSVC, pure speed variable concept; PDVC, pure displacement variable concept; SSCD, the segmented speed and continuous displacement concept of the pump; IMC, independent metering in and metering out circuit; PMAM, a permanent magnet asynchronous motor

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Nomenclature		$P_{ m out} \ oldsymbol{\omega}_{ m m}$	power output of the electric motor rotational speed of the electric motor
$E_{ m e}$	electric energy input to the inverter	$arPsi_{ m rd}$	rotor flux d axis component for induction machine
P_{ei}	electric power input to the inverter	$R_{ m s}$	equivalent resistance of stator winding
$E_{ m h}$	hydraulic energy output of the pump	$R_{ m r}$	equivalent resistance of rotor winding
$p_{\scriptscriptstyle \mathrm{D}}$	pump pressure	$R_{ m m}$	equivalent resistance of stator core loss
$q_{ m o}$	pump flow	$L_{ m m}$	mutual inductance between the stator winding and rotor
$\eta_{ ext{e-h}}$	energy efficiency of the electro-power source		winding
$v_{ m be}$	boom cylinder extending control signal	$\eta_{ m m}$	energy efficiency of the electric motor
$v_{ m br}$	boom cylinder retraction control signal	$\eta_{ m p}$	energy efficiency of the hydraulic pump
p_{A1}	pressure of the rod-less cavity of boom cylinder	$\eta_{ m pv}$	volume efficiency of the hydraulic pump
$p_{ m B1}$	pressure of the rod cavity of boom cylinder	$\eta_{ m pm}$	mechanical efficiency of the hydraulic pump
$q_{ m B}$	flow into the boom cylinder	n	rotational speed of the hydraulic pump
$E_{ m hloss}$	throttling loss of the hydraulic system	\boldsymbol{k}	proportionality coefficient
$E_{ m Bhloss}$	throttling loss of the boom system	C_{s}	Laminar leakage coefficient
$E_{ m Ahloss}$	throttling loss of the arm system	Δp	pressure difference of the hydraulic pump
$E_{\rm Buhloss}$	throttling loss of the bucket system	μ	kinematic viscosity of oil
$E_{ m Shloss}$	throttling loss of the swing system	β	Displacement factor, $V/V_{\rm max}$
E_{Thloss}	throttling loss of the travel system	$C_{ m V}$	Laminar drag coefficient
$\eta_{ m h}$	Energy efficiency of the hydraulic system	$C_{ m f}$	coefficient of mechanical resistance
$\eta_{ m total}$	energy efficiency of the excavator	$T_{ m s}$	Torque loss independent of speed and pressure difference
P_{loss}	power loss of the electric motor	$V_{ m max}$	maximum displacement of the pump

current power demand [11-16].

Although numerous technologies have been taken to improve the energy efficiency of the hydraulic excavator, this is not the eventual solution. Like the development direction of the automotive industry, the development direction of mobile machine is pure electric drive to eliminate emissions completely and to achieve low noise. And now, this system configuration is used in industrial equipments and some hydraulic shovels. In addition, there are some small hydraulic excavator productions with this configuration, such as Wacker Neuson dual-power 803 and Volvo EX2. This configuration is especially suitable for urban construction and water conservatory reconstruction projects with high environmental protection requirements. In these applications, the electric motor usually operates at its rated speed, resulting in large energy consumption under idle period and partial load conditions.

What's more, the displacement-variable pump usually operates in small displacement condition, during which the energy efficiency is poor [17–19]. Currently, one of the ways to deal with this situation is to use a quantitative pump driven by a speed-variable motor, named pure speed-variable power source (SVPS) [20,21]. The other approach is to use a displacement-variable pump driven by a speed-variable motor, named speed and displacement variable power source (SDVPS). It is reported that the energy consumption can be reduced by 20% and more comparing to pure speed variable concept (PSVC) or pure displacement variable concept (PDVC) [22]. Therefore, improved efficiency and reduced energy consumption are two of the main goals during the design period of modern electrohydraulic systems.

However, when the speed-variable power source is applied to a mobile machine, there exist some problems such as dynamic response,

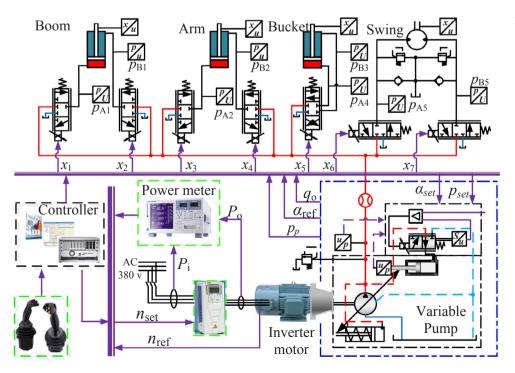


Fig. 1. System structure of electric excavator.

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