



Exergoeconomic and enviroeconomic analyses of hybrid double slope solar still loaded with nanofluids



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ABSTRACT

In recent times, incorporation of nanotechnology in solar distillation systems for potable water production is a new approach harvesting solar thermal energy. In present manuscript, concentration of assisting nanoparticles and basin fluid (basefluid/nanofluid) mass have been optimized for hybrid solar still operating (a) without heat exchanger (system A), and (b) with helically coiled heat exchanger (system B). Corresponding to the optimized parameters, overall thermal energy, exergy, productivity (yield), and cost analysis of the proposed hybrid systems loaded with water based nanofluids have been carried out; and found to be significantly improved by incorporating copper oxide-water based nanofluid. Moreover, on the basis of overall thermal energy and exergy, the amount of carbon dioxide mitigated per annum is found to be 14.95 tones and 3.17 tones respectively for the hybrid system (A); whereas, it is found to be 24.61 tones and 2.36 tones respectively for the hybrid system (B) incorporating copper oxide-water based nanofluid. Annual performance of the proposed hybrid systems has been compared with the conventional solar still (system C).

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1. Introduction

The solar photovoltaic (PV) technology is one of the most promising and fastest growing renewable energy technologies which will play a primary role in clean energy. Photovoltaic thermal systems or renewable energy (RE) systems on harvesting an ample source of (solar) energy are the viable option for various applications viz. solar water collector, solar air collector, space heating, greenhouse dryer, heat exchanger and building integrated photovoltaic thermal system, etc. Including clean food and air, potable water is a fundamental human need and it is essential to sustain life for all creatures on the Earth. Moreover, consumption of contaminated drinking water originates various diseases i.e. bacterial infections, viral infections, protozoal infections, etc. Worldwide, various nations are affected with water shortages. This problem basically originates due to change in climate conditions; rapid growth in population; floods, poor management of water resources and excess use of potable water. Therefore, the protection of safe drinking (potable) water requires proper “framework”; adequate, effective, and comprehensive policies for water distribution; and a system of independent surveillance.

Today, with advancement in science and technology, high and medium techniques have been developed to produce drinking water from the contaminated water. But, these techniques depend on the conventional source of energy i.e. electricity. Solar distillation is the simplest, cost-effect and environment friendly method for the production of potable water. Solar distillation systems or simply solar stills are categorized into passive and active solar stills [1]. There are some advantages of solar distillation over the other techniques i.e. no need of high tech exchange parts like batteries, filters, or membranes; purify highly saline water, feasible for local manufacturing, no conventional source of energy is required, and low initial investment.

The productivity of solar still mainly depends on the working temperature and internal heat transfer mechanism [2]. The heat transfer coefficients (HTCs) can be enhanced by improving the thermo-physical properties of water (basefluid).

In recent times, nanotechnology has been implemented in the solar stills in order to improve further their performance. Nanofluids are simply the suspension of 1–100 nm nanoparticles (NPs) in the basefluid (water, thermal oil, ethylene glycol, etc.). These are the embryonic fluids with ultrafast heat transfer capabilities due to their better thermo-physical and optical properties. These properties can be improved by tailoring the size and shape of the NPs in a particular basefluid.

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Nomenclature

A_m	area of the PV module, (m^2)	T_{goE}	outer condensing cover temperature of east side solar still, ($^{\circ}C$)
A_c	area of the glazing, (m^2)	T_{goW}	outer condensing cover temperature of west side solar still, ($^{\circ}C$)
A_{gE}	surface area of condensing cover of east side of solar still, (m^2)	T_{bf}	basefluid temperature, ($^{\circ}C$)
A_{gW}	surface area of condensing cover of west side of solar still, (m^2)	T_{nf}	nanofluid temperature, ($^{\circ}C$)
A_b	basin area of solar still, (m^2)	T_{giE}	inner condensing cover temperature of east side of solar still, ($^{\circ}C$)
C_p	specific heat capacity of NP, (J/Kg-K)	T_{nf}	fluid temperature, ($^{\circ}C$)
C_{nf}	specific heat capacity of nanofluid, (J/Kg-K)	T_v	vapor temperature, ($^{\circ}C$)
C_{bf}	specific heat capacity of basefluid, (J/Kg-K)	T_a	ambient temperature, ($^{\circ}C$)
D_i	diameter of the FPC tube (mm)	T_{giW}	inner condensing cover temperature of west side solar still, ($^{\circ}C$)
d_p	diameter of nanoparticle (nm)	ΔT_{DSSS}	temperature difference between NF and BF in DSSS, ($^{\circ}C$)
F'	collector efficiency factor	ΔT_{FPC}	temperature difference between NF and BF at the outlet of PVT collectors, ($^{\circ}C$)
$h_{1g,E}$	total external heat transfer coefficient on east side, ($W/m^2^{\circ}C$)	ΔT_{HE}	temperature difference between NF and BF in heat exchanger, ($^{\circ}C$)
$h_{1g,W}$	total external heat transfer coefficient on west side, ($W/m^2^{\circ}C$)	Δt	time interval (s)
$h_{1f,E}$	total internal heat transfer coefficient on east side, ($W/m^2^{\circ}C$)	$U_{tp,a}$	overall heat transfer coefficient from absorption plate to ambient, ($W/m^2^{\circ}C$)
$h_{1f,W}$	total internal heat transfer coefficient on west side, ($W/m^2^{\circ}C$)	$U_{L,m}$	overall heat transfer coefficient from module to ambient, ($W/m^2^{\circ}C$)
h_{EW}	internal radiative heat transfer coefficient between glass covers, ($W/m^2^{\circ}C$)	$U_{L,c}$	overall heat transfer coefficient from glazing to ambient, ($W/m^2^{\circ}C$)
$h_{ef,E}$	evaporative heat transfer coefficient on east side, ($W/m^2^{\circ}C$)	$U_{tc,a}$	overall heat transfer coefficient from cell to ambient from the top surface, ($W/m^2^{\circ}C$)
$h_{ef,W}$	evaporative heat transfer coefficient on west side, ($W/m^2^{\circ}C$)	U_{ga}	overall heat transfer coefficient between condensing cover and ambient air, ($W/m^2^{\circ}C$)
h_{ba}	heat transfer coefficient between basin liner and ambient air, ($W/m^2^{\circ}C$)	U_{ba}	overall heat transfer coefficient between basin liner and ambient air, ($W/m^2^{\circ}C$)
h_{FPC}	convective heat transfer in the flat plate collector, ($W/m^2^{\circ}C$)	U_{gaE}	overall heat transfer coefficient between outer condensing cover of east side and ambient air, ($W/m^2^{\circ}C$)
h_{HE}	convective heat transfer in the heat exchanger, ($W/m^2^{\circ}C$)	U_{gaW}	overall heat transfer coefficient between outer condensing cover of west side and ambient air, ($W/m^2^{\circ}C$)
$h_{b,f}$	heat transfer coefficient between basin liner and fluid, ($W/m^2^{\circ}C$)	$U_{tc,p}$	overall heat transfer coefficient from cell to the absorption plate, ($W/m^2^{\circ}C$)
h_{pf}	heat transfer coefficient from blackened plate to ambient, ($W/m^2^{\circ}C$)	X	characteristic length of solar still, (m)
h_i	heat transfer coefficient for space between absorption plate and glazing, ($W/m^2^{\circ}C$)	<i>Greek letters</i>	
h_o	heat transfer coefficient from top of PV water collector to ambient, ($W/m^2^{\circ}C$)	α_g	fraction of solar energy absorbed by condensing cover
I_{SE}	solar intensity on east side of the glass cover, (W/m^2)	α_b	fraction of solar energy absorbed by basin surface
I_{SW}	solar intensity on west side of the glass cover, (W/m^2)	α_f	fraction of solar energy absorbed by fluid
I_{SW}	solar intensity on FPC, (W/m^2)	α_c	fraction of solar energy absorbed by solar cell
K_p	thermal conductivity of the absorption plate (W/m-K)	τ_g	fraction of solar energy transmitted by top glass cover of the PVT-FPC
k_p	thermal conductivity of nanoparticle, (W/m-K)	ϕ_p	volume fraction of nanoparticles (%)
k_{nf}	thermal conductivity of nanofluid, (W/m-K)	η_c	efficiency of the PVT- FPC collector (%)
k_{bf}	thermal conductivity of basefluid, (W/m-K)	β	packing factor
K_g	thermal conductivity of condensing cover, ($W/m^2^{\circ}C$)	β_p	thermal expansion coefficient of nanoparticle, (K^{-1})
L	length of the helical heat exchanger (mm)	β_{nf}	thermal expansion coefficient of nanofluid, (K^{-1})
L_g	thickness of condensing cover, (m)	β_{bf}	thermal expansion coefficient of basefluid, (K^{-1})
L_b	thickness of basin, (m)	μ_{bf}	dynamic viscosity of basefluid, (Ns/m^2)
L_p	thickness of the absorption plate (m)	μ_{nf}	dynamic viscosity of nanofluid, (Ns/m^2)
M_f	mass of fluid in the basin of solar still (kg)	ρ_p	density of nanoparticle, (Kg/m^3)
\dot{m}_f	mass flow rate of the fluid (kg/s)	ρ_{nf}	density of nanofluid, (Kg/m^3)
\dot{M}_{bf}	yield obtained from the system (kg/h)	ρ_{bf}	density of basefluid, (Kg/m^3)
P_{gi}	partial saturated vapor pressure of the inner glass cover, (N/m^2)	<i>Subscripts</i>	
P_f	partial saturated vapor pressure of the fluid, (N/m^2)	a	ambient
PF_1	penalty factor due to glass covers of the module	b	basin surface
PF_2	penalty factor due to absorption plate below the module	v	vapor
PF_3	penalty factor due to absorption plate for the portion covered by the glazing	gi	inner condensing cover
r_{11}	outer diameter of the heat exchanger tube (mm)	go	outer condensing cover
r_{22}	inner diameter of the heat exchanger tube (mm)		

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