



Effect of angular losses on the output performance of solar array on long-endurance stratospheric airship



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ABSTRACT

The solar array is one of the major components of long-endurance stratospheric airship which converts the solar energy to electric energy. Exact calculation of the output performance of solar array is significant to the operation of the airship. The move of the sun and the curve surface of the airship lead to the dramatic change of the incidence angle of solar radiation. Therefore, the angular losses, caused by the change of incidence angle, decreasing the efficiency of solar cell and then reducing the output energy of solar array, should be taken into account. But the relevant investigations are rare. In this paper, a simplified numerical model including solar radiation model, thermal model and angular losses model was established. A MATLAB computer program was developed based on the model to research the deviation of output energy of solar array with/without angular losses. The effects of date, airship's attitude and latitude on the deviation were also discussed in detail. The result indicates that the output energy of solar array on stratospheric airship was overestimated without considering the angular losses and the angular losses should be taken into account for an accurate calculation. It is believed that the present models and program will lead to a better design for the energy management system of stratospheric airship.

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1. Introduction

The stratosphere, with the characteristic of stable atmosphere and weakly vertical convection, is the ideal location to deploy aerial platforms for the purpose of surveillance, early alarming, communications relay, navigation and environmental monitoring [1,2]. Conventional airplanes and satellites can't fly for a long period at this location. With the advantage of long-endurance (months to years) and station-keeping, stratosphere airships have received much attention in recent years [3]. Since the US Navy first proposed the high-altitude airship in 1978 with the HASPA program [4], many other countries, such as China, Japan, South Korea and European countries, have developed many investigations and experiments of stratospheric airships [5–7]. Fig. 1 shows the airship designed by our team.

For the purpose of long-endurance, the thin film solar array which can utilize solar energy, regenerative fuel cell and lithium rechargeable battery are the common collocation to supply energy for many stratospheric airships [8]. Since the solar energy is the main energy source of the airship, it is significant to calculate the output power of solar array and design the energy management

system based on it. Many researches were carried out for it in the past decades. Wu [9] presented a comprehensive literature review focusing on the thermal issues, including direct solar radiation model, diffuse solar radiation model and reflected model for clear skies, which provides guides for solar radiation model selections and suggests topics be worth for further research. Naito [10] studied the concept design and analyzed the generated energy of the solar array. The result shows that sufficient energy is available at solar array over a year to distribute to the propulsive motors, control unit and payload mission. Considering that the solar radiation on the solar cells of a curved surface is different from that on the horizontal projection plane, Wang [11] proposed a computation method for solar radiation on solar cells taking into account the effect of surface curvature and studied the effect of the airship's attitude on the performance of solar array. Li [12] developed a numerical model for investigating the effects of solar array layouts on the output performance and optimized the solar array layouts under four common airship operating conditions. They found that the solar array layout optimization for stratospheric airships can comprehensively improve the output power of the solar panel, which is helpful in guiding to install suitable solar array for long-endurance airship. Ma [13] proposed a new management technology of the multi-power system based on the variation of airship flight modes and system related energy demands.

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Nomenclature

A	area, m^2	T_0	standard test temperature of solar cell efficiency, 298.15 K
$AL(\theta)$	angular losses factor	T	temperature, K
$C_{env/SC}$	specific heat capacity of envelope or solar cell, $J/(kg\ K)$	T_g	temperature of ground, K
C_{high}	calibration factor at high altitude	TC	temperature coefficient of solar cell efficiency, $\%/K$
C_{low}	calibration factor at low altitude	TL	temperature loss of solar cell efficiency
d	thickness, m	α_{DN}	absorptivity of solar cell to direct solar radiation
g	gravitational acceleration, m/s^2	$\alpha_{IR_{ex}}$	absorptivity of external surface of envelope or solar array
h	altitude, m	$\alpha_{IR_{in}}$	absorptivity of internal surface of envelope or solar array
h_{in}	internal natural convective heat transfer coefficient, $W/(m^2\ K)$	γ	angle of refractive, rad
h_{out}	external convective heat transfer coefficient, $W/(m^2\ K)$	γ_0	central angle of solar array, rad
I_0	solar constant, $1367\ W/m^2$	ε_{ex}	emissivity of external surface of envelope or solar cell
I_{DN}	normal direct solar intensity, W/m^2	ε_{in}	emissivity of internal surface of envelope or solar cell
$I_{IR_{ex}}$	envelope/solar cell internal surface infrared radiation, W/m^2	ε_g	emissivity of ground
$I_{IR_{g}}$	ground infrared radiation, W/m^2	$\varepsilon_{env/SC}$	emissivity of envelop or solar cell
$I_{IR_{grid_{i0}}}$	internal surface infrared radiation of envelope/solar array grid $i0$ from other grids, W/m^2	ζ	true anomaly, rad
$I_{IR_{in}}$	envelope/solar cell internal surface infrared radiation, W/m^2	η	efficiency of solar cell
I_{SUN}	extraterrestrial normal solar intensity, W/m^2	θ	incident angle of solar radiation, rad
k	thermal conductivity, $W/(m\ K)$	θ_{DIP}	angle of view at altitude h , rad
L	length of airship, m	θ_{azi}	sun azimuth angle, rad
L_0	characteristic length of airship, m	θ_{day}	day angle, rad
N	day number	θ_{dec}	declination of sun, rad
N_0	correction term of the day number	θ_{ele}	elevation angle of sun, rad
Nu	Nusselt number of free convection	θ_{hour}	hour angle of sun, rad
n_0	refractive index of air	λ_{AM}	air mass ratio
n_1	refractive index of encapsulation material	μ	dynamic viscosity
\vec{n}_{ij}	normal vector of titled grid ij in the body fixed coordinate system	ρ	density, kg/m^3
\vec{n}_{ijl}	normal vector of titled grid ij in the inertial reference system	σ	Stefan-Boltzmann constant
\vec{n}_s	unite vector of direct solar radiation	$\tau_{IR_{g}}$	transmittance of atmosphere at altitude h
P	output power of solar array, W	τ_{atm}	infrared radiation transmissivity of solar beam through the atmosphere
Pr	Prandtl number	$\tau(\theta)$	transmittance of encapsulation material
p_0	atmospheric pressure at sea level, Pa	Φ	local latitude, rad
p_h	atmospheric pressure at altitude h , Pa	φ	pitch angle, rad
q_{DN}	absorbed direct solar radiation energy, W	ϕ	roll angle, rad
R	transformation matrix	ψ	yaw angle, rad
Re	Reynolds number of airship		
$r(\theta)$	reflectivity of solar cell surface	<i>subscripts</i>	
r_0	radius of earth, m	<i>atm</i>	atmosphere
r_{IR}	albedo of internal surface of envelope	<i>env</i>	envelope
$r_{airship}$	rotary radius of airship, m	<i>env/SC</i>	envelope or solar cell
r_p	reflection coefficient of transverse-magnetic	<i>ij</i>	titled grid ij
r_s	reflection coefficient of transverse-electric	<i>Lgas</i>	lifting gas
		<i>SC</i>	solar cell

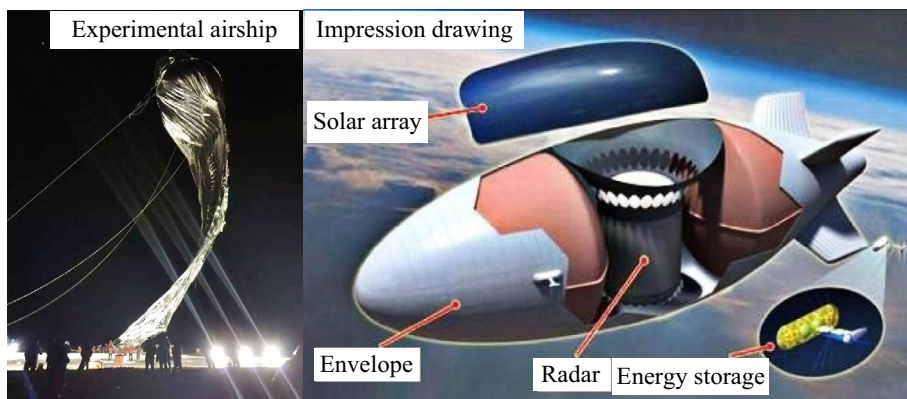


Fig. 1. The experimental stratospheric airship designed by our team and its impression drawing.

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