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# A theoretical study of rotatable renewable energy system for stratospheric airship



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#### ABSTRACT

Renewable energy system is very critical for solving the energy problem of a long endurance stratospheric airship. Output performance of the traditional solar array fixed on the upper surface of the airship remains to be improved to reduce the area and weight of renewable energy system. Inspired by the solar tracking system and kirigami, a rotatable renewable energy system (mainly including solar array) is designed to improve the current status of the energy system. The advantages of the rotatable solar array are studied using a MATLAB computer program based on the theoretical model established in this paper. The improvements in output energy and required area of the solar array were compared between the traditional airship and improved one. Studies had shown that the rotatable renewable energy system made the total weight of energy system decreased by 1000 kg when the maximum design speed of the airship was greater than 22 m/s. The results demonstrate that the rotatable renewable energy system for the airship can be a good way to improve the output performance of solar array, and the conceptual design and theoretical model suggest a pathway towards solving the energy problem of a stratospheric airship.

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### 1. Introduction

A stratospheric airship is a lighter-than-air aircraft which can fly in the stratosphere to provide potential applications especially for the border patrol, homeland security, maritime and airborne surveillance, data and communications relay, and environmental research. The last 20 years have witnessed the projects establishment and researches of stratospheric airship in various countries, especially the developed countries in Europe and America, which greatly promote the development of the stratospheric airship [1,2].

Compared with the traditional aircrafts, the stratospheric airship can stay in the stratosphere with the advantages of long endurance and low energy consumption. In order to accomplish an extended duration of time (months to years) at high altitudes (18-20 km), the renewable energy technologies such as the thin film solar arrays, the fuel cells, electrolyzers and the power management become the key. Hence, many researches and developments have been in progress in the renewable energy system on stratospheric airships in the past decades [3]. Colozza [4] made an initial look at the feasibility of operating a high altitude long endurance airship along the east coast by the way of analyzing the payload capacity and power requirements, size (drag), compo-

\* Corresponding author. E-mail address: lv312@buaa.edu.cn (H. Du). nent efficiencies and power management. The result showed that the solar array, as a renewable energy system, could provide enough energy for a stratospheric platform airship. Wang [5] presented a computation method for solar radiation on solar cells of the curved surface of the high-altitude airship, and studied the effect of the HAA's attitude on the performance of its energy system when the airship was flying in 40 deg north latitude region. Zhang [6] established a new simplified analytical model with thermal effects to analyze the output performance of the solar array and studied the effects of latitude, date, attitude and attitude angle on the output performance of the solar array.

These researches provided a base for investigating the output performance of solar array on stratospheric airship. In these research works, based on the fact that the efficiency of lightweight flexible thin film photovoltaic cells was generally low [7], there was a simplified problem that the airships needed to sacrifice some useful functional loads to carry a heavier energy system when the lightweight flexible thin film photovoltaic cells was used as a renewable energy device. This problem should be considered carefully in the design phase due to the adverse effects on the practical performance and utilization efficiency of the entire airship. Therefore, the renewable energy system of airship is required for further research to solve the above-mentioned problems. The similar studies have been carried out by some scholars and research institutions [8]. In these traditional designs, the solar array is fixed on

#### Nomenclature

$\begin{array}{c} C_{high} \\ C_{low} \\ C_{total} \\ C_{envelope} \\ D \\ e_e \\ F_{propulsion} \\ F_{drag} \end{array}$	the calibration factor at high altitude the calibration factor at low altitude the total drag coefficient of the airship the volumetric coefficient of the airship envelope the maximum diameter of airship, m orbital eccentricity the propulsion force, N the total drag of the airship, N	$\begin{array}{l} \mathbf{y}_{1} \\ \mathbf{y}_{2} \\ \alpha_{e} \\ \alpha_{R} \\ \theta \\ \theta_{day} \\ \theta_{dec} \\ \theta_{DIP} \end{array}$	the y coordinate of leading edge of solar array the y coordinate of trailing edge of solar array absorptivity of solar array to direct incident absorptivity of solar array to reflected radiation central angles of solar array, degrees day angle of the sun, degrees the declination of the sun, degrees the angle of view at the altitude <i>h</i> , degrees
n	normal vector of tilted grid	$\theta_{ele}$	solar elevation angle, degrees
1 <sub>0</sub> 1	Solar constant, $I_0 = 1507 \text{ W/m}^2$	θ <sub>hour</sub> Φ	the local latitude, degrees
I <sub>h</sub> I	scattered radiation W/m <sup>2</sup>	Ψ Φ	the allowable misalignment of flight latitude degrees
k	the factor of energy	$\Psi$ error	the rotation angle of solar array degrees
Kenergy Is A	the length of the solar array, m	φ	the upper bound of rotation angle, degrees
L	total length of the airship, m	Ψup Nsc	the efficiency of the solar cell
m	the masses, kg	$\eta_{FC}$	the fuel cell efficiency
$\vec{n}_{s}$	unit vector of solar direct radiation	$\eta_F$	the electrolyzer efficiency
$\vec{n}_{ii}$	the normal vector of grid <i>ij</i>	$\eta_{propulsion}$	the propulsive efficiency
$\vec{n}_{ijI}$	the expression of the normal vector of tilted grid <i>ij</i> in	$\lambda_{am}$	air mass ratio, degrees
	the inertial frame of reference	$\lambda_e$	the true anomaly
N <sub>day</sub>	the day number	δ	the index which takes into account the self-shadowing
$N_0$	the correction term of the day number		of the curved surface solar array from the reflected
$p_h, p_0$	the atmospheric pressure at the altitude h and the sea		radiation
	level, reflectivity	$ au_h$	the transmissivity of a solar beam thru the atmosphere
$p_{SC}$	the total power of solar array, kw	$ ho_a$	the density of the amplent all at the design antitude, $la/m^3$
P <sub>req</sub>	radiation on the tilted grid W	Ľ	the included angle between the plane normal and the
ч О	total radiation on solar array W	ç	gravity direction
0,	the energy available for storage GI	(Daine 1	projection coefficient of solar direct radiation on the
$Q_3$	the energy supplied for the power consuming function on the airshin GI	oo sign 1	tilted grid
0a	the total energy required to run an airship and its pay-	Subscript	rs.
Cieq	loads. Gl	Relt	the drive belt
QSA	the output energy of the renewable energy system, G	BP	the butter paper
$Q_{SA \min}$	the minimum output energy of solar array in daytime,	FI	the fixed infrastructure used for installing and fixing the
	GJ	••	solar arrav
r	the equivalent rotary radius of airship, m	h	the altitude <i>h</i>
r <sub>e</sub>	the radius of earth, m	ij	tilted grid ij
$v_{wind}$	the relative velocity between the airship and the	İmproved	the improved airship
	flowing air, m/s	Insulation	n the lightweight insulation substrate for solar array
x	chordwise coordinate	Motor	the electric motor
x <sub>ij</sub> , z <sub>ij</sub>	the x and z coordinates of the central point of tilted	SA	solar array
	grid <i>ij</i>	SC	solar cell
y -	chordwise coordinate	Storage	the storage system
Z	vertical coordinate	Tradition	al the traditional airship

the upper surface of the airship, as shown in Fig. 1(a). In order to maximize the output energy of the solar array, different solar array layouts should be designed when the dates and locations of the flight task are different. However, based on the result shown in Fig. 1(b), the output power is the maximum only at noon. The main reason is that, most of the time, the normal vectors of the solar cells do not point to the sun and the solar cells suffer optical coupling losses due to a decrease in projected area that scales with the cosine of the misalignment angle between the cell and the sun, as shown in Fig. 2(a).

On the other hand, one conclusion can be obtained that the solar array has a great influence on the thermal performance of the envelope and lifting gas. The high solar irradiation flux, low convective heat transfer, and low ambient temperature make superheat and supercool phenomena easily happen in stratosphere [9]. The simulation results reported by Harada [10] indicated that the highest temperature on PV-panel would reach about 370 K at

noon due to the high solar absorptivity of solar cells. However the highest temperature on envelope without PV-panel was only 320 K in the summer solstice. This phenomenon made the superheat problem even worse. Excessive high temperature of inner lifting gas induces the rise of pressure which can break the envelope and even destroy the airship. Therefore a thermal insulation layer between solar cells and envelope has become an essential structure [11,12]. However, large areas of thermal insulation layer make the energy system heavier. It is clear that the area of the solar array is necessary to be reduced to save the weight of solar array and thermal insulation substrate.

Inspired by the solar tracking system and kirigami (the art of paper cutting shown in Fig. 2) [13–15], to cut these losses and maximize the power output, curved solar array on stratospheric airship can be rotated to track the positions of the sun over the course of the day. Depending on the geographic location of the system, and whether there are one or two tracking axes, traditional

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