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Fracture assessment based on unified constraint parameter for pressurized pipes with circumferential surface cracks

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ABSTRACT

The fracture assessment capability and methodology based on the unified constraint parameter A_p have been comparably investigated with the conventional procedures without considering constraint effect and the assessment approach based on the constraint parameter Q for pressurized pipes with circumferential surface cracks. The results show that the A_p can be used in failure assessment diagram based fracture assessment by modifying the fracture toughness using the unified correlation formulae of fracture toughness with A_p . A fracture assessment methodology based on the parameter A_p for incorporating both in-plane and out-of-plane constraints has been proposed. The constraint characterization and fracture assessment using the parameter A_p for the pipe cracks may get the best accuracy and can reduce excessive conservatism of the conventional assessments. The benefits from the unified constraint assessments increase with decreasing crack depth and length.

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1. Introduction

Defects occurring at fabrication or service stage in engineering structures might be responsible for structural failure. The structural significance of such imperfections, particularly crack-like flaws need to be assessed to prevent failure of the component during service [1]. The fracture criterion based on conventional fracture mechanics assumes that the structural component exhibits the same fracture resistance, K_c , δ_c or J_c , at the onset of unstable fracture as the laboratory fracture toughness specimen [2]. However, defects in large engineering structures (such as pressurized pipes and vessels) are often subjected to a significantly lower level of crack tip constraint than those in laboratory fracture specimens [3]. This ensures that the fracture assessment in low constraint structural components using conventional fracture mechanics methodologies may be excessively conservative. This conservative assessment may lead to unnecessary replacement or repairs of in-service components at great operational cost. Therefore, the constraint effect needs to be considered in fracture assessment for structural components.

Constraint can be regarded as the resistance of a structure against crack-tip plastic deformation [4]. The constraint contains in-plane and out-of-plane constraints. The in-plane constraint is directly affected by the specimen dimension in the direction of growing crack, that is, the length of the un-cracked ligament, while the out-of-plane constraint is affected by the specimen dimension parallel to crack front, that is, the specimen thickness. The quantification of constraint has been studied for a long time, and different constraint parameters have been put forward in the last few decades, such as

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Nomenclature

2

M.Y. Mu et al./Engineering Fracture Mechanics xxx (2017) xxx-xxx

Nonenclature	
а	crack denth
u A	narranger quantifying second and third term of stress relative to the first term in a cracked elastic-plastic body
A	parameter quantifying second and time term of sites relative to the first term in a cracked classic-plastic body
A A	a constraint of the sector sector plasma sector is plane and out of plane constraint
Δ.	a unified characterization parameter of mepiane and out-of-plane constraint
A _{ref}	half grade longth
L E	
E	the elastic modulus
n	stress triaxiality factor
J	elastic-plastic J- integral
Jic	racture tougnness
Je	elastic J-integral
Jref	racture tougnness measured in a standard test
KI	elastic stress intensity factor
K _c	fracture toughness characterized by stress intensity factor K
K _{Jc}	fracture toughness calculated from J_{IC}
K _{mat}	material's fracture toughness
K _{mat}	modified fracture toughness by constraint
K _P	plastic stress intensity factor
K _r	normalized crack-tip loading
K _{ref}	fracture toughness measured in a standard test
L_r	normalized applied loading
$L_{r(max)}$	maximum value of L _r
Μ	bending moment
M_{f}	fracture moment
M_f^0	fracture moment predicted by conventional assessment
M_f^c	fracture moment predicted by constraint assessment
M	limit bending moment
p	internal pressure
Р Р	applied load
Pr	plastic limit load
0	a constraint parameter under elastic-plastic condition
O^{BLA}	constraint parameter with reference field of boundary layer analysis
R:	inside radius
R _o	outside radius
t	nine wall thickness
т Т	non-singular term of stress (T-stress for elastic condition)
T ₋	factor of the stress-state in 3D cracked body
W	specimen width
c .	specificity when
6 6	equivalent nlastic strain
σ^{p}	citation public strum
σ	vield stress
σ_{i}	ultimate tensile stress
σ_{b}	flow stress
σ_{I}	now succes
$(\boldsymbol{\sigma}_{\theta\theta})$	reference opening stress based on boundary layer analysis
$(\sigma_{\theta\theta})_{BLA}$	avial strase
v_{φ}	ania sitess Daisean's ratio
N	a parameter defining constraint sensitivity of material
k	a parameter defining constraint sensitivity of material
R	another parameter defining constraint sensitivity of matchial a factor defined as $B_{L} = T/\sigma_{0}$ or $B_{L} = 0$
$\frac{\rho}{2}$	a factor defined as $p_{Lr} = 1/00$ or $p_{Lr} = Q$
λ	
Acronym	IS and the second se
API	American Petroleum Institute
ASME	American Society of Mechanical Engineers
ASTM	American Society for Testing and Materials
BLA	boundary layer analysis

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