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Thermal analysis of airflow inside a refrigerated container



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ABSTRACT

A numerical study of conjugated heat transfer in ceiling-slot refrigerated containers is carried out to analyze the temperature distribution effectiveness and to determine the ventilation characteristics. The effect of slot size on thermal characteristics is studied by considering half-span and full-span injection. The container walls are defined as conductive opaque and are interacting with outside environment. The outer surface heat transfer coefficients of conductive walls are computed by studying the flow around the refrigerated truck. The Reynolds number at the slot exit varied between $2 \times 10^4 \leq Re \leq 2 \times 10^5$. The gravity effect is taken into account, and the coupled mass, momentum, and energy equations are discretized in finite volumes. The heat transfer coefficients of inner flow are presented as plots of the mean Nusselt number versus the modified Reynolds number. The maximum dispersion in the numerical data being at 14.54-percent, the mean Nusselt number, the modified Reynolds number, and the aspect ratio of the container are correlated.

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Analyse thermique du débit d'air à l'intérieur d'un conteneur réfrigéré

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1. Introduction

Absence of effective food refrigeration causes several changes in food structure and accelerates food deterioration in cold chain

(Derens-Bertheau et al., 2015; Hoang et al., 2012; Laguerre et al., 2013). The process of creating adequate conditions for slowing down these changes can be divided into two categories: efficient ventilation of air within the storage space and cooling to achieve the desired temperature. Ceiling-slot-ventilated

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| Nomenclature | | Greek letters | |
|----------------------|--|---------------------|---|
| A | Cross-sectional area [m ²] | α_s | Surface absorptivity [-] |
| C's | Turbulence model coefficients [-] | β | Thermal expansion coefficient [K ⁻¹] |
| c_p | Specific heat of air [Jkg ⁻¹ K ⁻¹] | δ_{ij} | Kronecker symbol |
| d_h | Hydraulic diameter of the injection slot [m] | ε | Turbulence energy dissipation rate [m ² s ⁻³] |
| E | Temperature effectiveness [-] | ε_s | Surface emissivity [-] |
| e | Percent error in mean Nusselt number correlation [%] | η | Ventilation effectiveness [-] |
| Gr _J | Grashof number of J th surface, $Gr_J = \frac{g\beta(T_{smj} - T_m)H^3}{\nu^2}$ [-] | θ | Non-dimensional temperature, $\theta = \frac{T_{in} - T}{T_{in} - T_{inj}}$ [-] |
| g | Gravity constant [ms ⁻²] | λ | Thermal conductivity [Wm ⁻¹ K ⁻¹] |
| H | Container height [m] | μ | Dynamic viscosity [Pa.s] |
| h | Convective heat transfer coefficient [Wm ⁻² K ⁻¹] | ν | Kinematic viscosity [m ² s ⁻¹] |
| I_{solar} | Solar irradiation reaching the earth surface [Wm ⁻²] | ϑ | Volume flow rate [m ³ s ⁻¹] |
| k | Kinetic energy of turbulence [m ² s ⁻²] | ρ | Air density [kgm ⁻³] |
| L | Container length [m] | σ | Stephan-Boltzmann constant [-] |
| l | Related to evaporator size (see Fig. 1) [m] | τ | Shear stress [Pa] |
| Nu | Nusselt number, $Nu = \frac{hH}{\lambda}$ [-] | Subscripts | |
| Pr | Prandtl number, $Pr = \frac{\mu c_p}{\lambda}$ [-] | a | air |
| p | Pressure [Pa] | cr | critical |
| q | Heat transfer rate through a conductive surface [W] | in | Inlet to evaporator |
| Re | Reynolds number of injection, $Re = \frac{\rho u_{inj} d_h}{\mu}$ [-] | inj | Exit from evaporator |
| Re* | Modified Reynolds number, $Re^* = \frac{\rho u_{inj} H}{\mu}$ [-] | i,j,k | Vector directions in x,y,z |
| Ri | Richardson number, $Ri = \frac{Gr}{Re^{*2}}$ [-] | J | Identifies a conductive surface |
| T | Local temperature [°C] | m | Mean value |
| T _x | Mass averaged air temperature at a cross-section x (Eq. (16)) [°C] | ref | Reference |
| ΔT | Temperature difference (T _s -T _m) [°C] | s | Surface inside |
| V | Volume [m ³] | so | Surface outside |
| W | Container width [m] | t | Turbulent |
| $\overline{u_i u_j}$ | Reynolds stress component [m ² s ⁻²] | w | Wall |
| u, v, w | Velocity components [ms ⁻¹] | ∞ | Surroundings |
| y^+ | The wall unit, $y^+ = \frac{y\sqrt{\tau_s/\rho}}{\nu}$ [-] | Superscripts | |
| x, y, z | Cartesian axis directions | ' | Fluctuations in velocity and temperature |
| | | " | Flux |
| | | t | Truck |

enclosures are commonly used in transport refrigeration systems where the cold air is supplied into the enclosure by a turbulent air jet. The information on this paper focuses on such ventilation system with high injection velocities of air. Moureh and Flick (2003) have studied the essential aerodynamic features of air flow inside a rectangular cavity with cold air injected through a slot at the upper half of the container front surface. The suction slot located at the lower half of the same front surface completes the air circulation in the container. Similarly, Moureh and Flick (2005) also analyzed the effect

of the inlet-slot positioning on container ventilation effectiveness. In both of these analyses, a single value of the cold air blown rate is considered, and more importantly the flow geometry studied lacks representing the flow of a common ceiling-slot-ventilated enclosure used for refrigeration purposes. The container type generally accepted for perishable food transport is equipped with an evaporator that protrudes into the cold space. The injection and suction slots of the evaporator located at different surfaces provide the circulation of inside air. Smale et al. (2006) indicated that the Coanda effect which

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