Petroleum 3 (2017) 51-55

Contents lists available at ScienceDirect

Petroleum

journal homepage: www.keaipublishing.com/en/journals/petIm

A novel rate of the reaction between NaOH with CO₂ at low temperature in spray dryer

Yadollah Tavan ^{a, b, *}, Seyyed Hossein Hosseini ^b

^a National Iranian Gas Company (NIGC), Tehran, Iran

^b Chemical Engineering Department, Faculty of Engineering, Ilam University, Ilam, Iran

ARTICLE INFO

Article history: Received 6 May 2016 Received in revised form 1 October 2016 Accepted 9 November 2016

Keywords: CO₂ Kinetic Spray dryer NaOH

ABSTRACT

Carbon dioxide (CO₂) is an influential greenhouse gas that has a significant impact on global warming partly. Nowadays, many techniques are available to control and remove CO₂ in different chemical processes. Since the spray dryer has high removal efficiency rate, a laboratory-scale spray dryer is used to absorb carbon dioxide from air in aqueous solution of NaOH. In the present study, the impact of NaOH concentration, operating temperature and nozzle diameter on removal efficiency of CO₂ is explored through experimental study. Moreover, the reaction kinetic of NaOH with CO₂ is studied over the temperature range of 50–100 °C in a laboratory-scale spray dryer absorber. In the present contribution, a simple reaction rate equation is proposed that shows the lowest deviation from the experimental data with error less than 2%.

Copyright © 2016, Southwest Petroleum University. Production and hosting by Elsevier B.V. on behalf of KeAi Communications Co., Ltd. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

1. Introduction

It is well known that CO_2 plays a dominating role in the greenhouse gases [1–7]. Global climate change leads to the high interest in the technologies relevant to the CO_2 capturing that is one of the potential methods to reduce greenhouse gas emissions [8–12]. Many alternative strategies are proposed to reduce the emission of CO_2 . Among them, reactive absorption as an economically feasible method has been extensively studied for CO_2 capturing [8].

Spray dryer is a chamber in which the liquid solution is sprayed by atomizer as droplets into hot flow gas, resulting in drying the liquid droplets. In spray drying system, the moisture on the droplets is evaporated gradually, while the absorbents in the droplets react with impurities, simultaneously. Spray dryer is

 Corresponding author. National Iranian Gas Company (NIGC), Tehran, Iran. *E-mail address:* yadollahtavan@gmail.com (Y. Tavan).
 Peer review under responsibility of Southwest Petroleum University.

Production and Hosting by Elsevier on behalf of KeAi



a well-known process in industry, e.g. for the production of ceramic precursors, and temperature-sensitive pharmaceuticals. This device has no wastewater products and can control CO₂ emission into atmosphere. The performance of spray drying was improved and high removal efficiency rates were obtained for this device [10,13–16]. These researches only have used spray dryer as a simple device and no data regarding its performance on reactive absorption have been reported. Up to now, only a semi-empirical kinetic model has been proposed in Ref. [16] for a spray-dryer setup over the temperature range of 100-200 °C. It has been found that when the operating temperature highly increases, the removal efficiency of CO₂ decreases. Therefore, it seems that exploring a new reaction rate between CO2 and NaOH at low temperatures can be helpful for increasing the removal efficiency of CO₂. In fact, the description and prediction of the reaction kinetics in reactive systems, under given process conditions, is still a serious weakness in the modeling of processes including CO₂ capturing. The lack of existing literature in reactive absorption in spray dryer motivates the authors to study this process in more details. Accordingly, such study is undertaken and a new rate equation is proposed for low temperatures CO₂ removal in spray dryer device. Furthermore, effect of absorbent concentration, operating temperature and nozzle diameter on removal efficiency of CO₂ is investigated.

http://dx.doi.org/10.1016/j.petlm.2016.11.006

2405-6561/Copyright © 2016, Southwest Petroleum University. Production and hosting by Elsevier B.V. on behalf of KeAi Communications Co., Ltd. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).





CrossMark

2. Experiments

Commercial CO₂ gas with 99% purity and pellets of sodium hydroxide that were purchased from the Ruham gas Company (50 kg) and the Kimiaexir Company in Iran, respectively, are used. The required air for the study is supplied by a laboratory scale compressor. The NaOH pellets are dissolved in distilled water and continuously fed into spray drver by pump. A schematic diagram of the experimental apparatus is shown in Fig. 1. In this setup, flow rate of air is monitored by a velocity meter and the flow of CO₂ is adjusted with a rotameter (to avoid solidification, an internal heater is used for CO₂ cylinder). The mixture of air and CO₂ is preheated by an electronic heater and fed into the spray dryer from the top. The feed stream (aqueous solution of NaOH) is concurrently fed to the drying chamber. The CO₂ concentrations at the inlet and outlet of spray dryer are measured by an infrared CO₂ gas monitor (0-3000 ppm and 0-100% in volume; $\pm 2\%$ uncertainty Edinburgh Instruments Ltd). Typically, the gas mixture (air and CO₂) is heated to 50–100 °C and this stream sprayed 3 wt % of aqueous NaOH into the reaction chamber of spray dryer (0.25 m \times 0.45 m). In this process, heat and mass transfer and the chemical reaction occur in the reactive spray dryer, simultaneously. Generally the process includes:

- 1 Mass transfer of CO_2 from the gas stream to the droplet surface.
- 2 Absorption of CO₂ at the droplet surface, dissolution of CO₂ in the droplet and dissociation:

$$\operatorname{CO}_2(\operatorname{gas}) \to \operatorname{CO}_2(\operatorname{aq})$$
 (1)

 $CO_2 (aq) + H_2O (liq) \leftrightarrow H_2CO_3(liq)$ (2)

$$H_2CO_3 (liq) \leftrightarrow HCO_3^- + H^+ \leftrightarrow CO_3^{2-} + 2H^+$$
(3)

- 3 Chemical reaction between dissolved CO₂ and the dissolved CO₂ reagent:
 - i- Dissolution of sorbent:

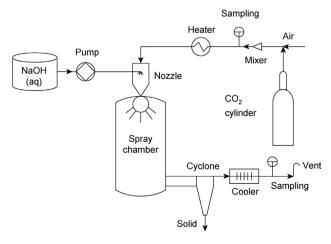


Fig. 1. Spray dryer setup.

$$NaOH (s) \leftrightarrow NaOH (aq) \leftrightarrow Na^{+} + OH^{-}$$
(4)

ii- Precipitation of sodium carbonate:

$$CO_3^{2-} + 2Na^+ \leftrightarrow Na_2CO_3(s) \tag{5}$$

4 Evaporation of the water in the droplet.

Generally, the overall chemical reaction can be written in a simple form as:

$$CO_2 + 2NaOH \leftrightarrow Na_2CO_3 + H_2O \tag{6}$$

Each experiment is carried out for 10 min by considering the liquid/gas weight ratio less than 0.2 to prevent weeping and also to reach the complete drying. Hence, no weeping is found during experiments. It is interesting to note that due to solid formation during the reaction, washing the dryer chamber and nozzle is crucial. In order to run a new experiment, the dryer chamber is washed by distilled water for 1 h, while no CO₂ and NaOH present in feed streams. Afterwards, the pump is turn down and dryer chamber is dried by clean air for 30 min at 150 °C. When no liquid is seen in the chamber, clean air and CO₂ are mixed together and fed to the dryer. After the temperature in the spray dryer reached to 50-100 °C range and the inlet concentration of CO₂ became stable, the absorbent is sprayed into the dryer chamber. In order to explore the absorption performance, removal efficiency (η) is used. Removal efficiency defines the percentage of removed CO₂ during absorption operation [17,18]. The removal efficiency for CO₂ is simply determined from the difference between the amounts of CO₂ entering and leaving the dryer chamber as follows

$$E(\%) = \frac{Y_{in} - Y_{out}}{Y_{in}}$$
(7)

It is worth mentioning that all experiments were conducted at summer of 2013 from 7 to 11 a.m., accordingly, a constant value for relative humidity of clean air is assumed during all experiments.

3. Results and discussions

3.1. Absorption performance

The removal efficiency of CO_2 as a function of operating temperature is shown in Fig. 2 with the inlet CO_2 concentration

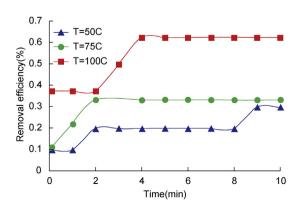


Fig. 2. Effect of operating temperature on absorption performance.

Download English Version:

https://daneshyari.com/en/article/5026508

Download Persian Version:

https://daneshyari.com/article/5026508

Daneshyari.com