



Diethyl ether pyrolysis study in a jet-stirred reactor



Nicolas Vin, Olivier Herbinet, Frédérique Battin-Leclerc*

Laboratoire Réactions et Génie des Procédés (LRGP), CNRS, Université de Lorraine, ENSIC, 1 rue Grandville, BP 20451, 54001 Nancy Cedex, France

ARTICLE INFO

Article history:

Received 20 May 2016

Received in revised form 18 July 2016

Accepted 21 July 2016

Available online 30 July 2016

Keywords:

Diethyl ether

Pyrolysis

Jet-stirred reactor

ABSTRACT

This paper reports new experimental measurements for the pyrolysis of diethyl ether at temperatures between 600 and 1100 K under dilute conditions. This work was performed using a jet-stirred reactor at pressures from 26.7 kPa (200 Torr) to 107.7 kPa (800 Torr) with dilution in helium, for residence time from 1 to 10 s and an inlet fuel concentration from 1 to 5%. Temperature was the parameter with the largest influence on reactivity. The complete destruction of diethyl ether was observed from 1080 K. A decrease of residence time and pressure also slightly decreased reactivity, but the effect of pressure remained very limited. Major products were carbon monoxide, methane, ethylene and acetaldehyde. Minor products were ethane, acetylene, propane, propene, ethanol, 1,3-butadiene, and benzene. Two literature models including diethyl ether reactions have been used to simulate these results, with in both cases a satisfactory agreement between experiments and simulations for fuel conversion and the formation of most of the products. Simulations using a literature model for the thermal decomposition of diethyl sulfide indicated that in the studied conditions, the sulfur compound would be completely decomposed at a temperature about 100 K lower than the oxygenated reactant.

© 2016 Elsevier B.V. All rights reserved.

1. Introduction

The primary purpose of this study was to investigate the gas-phase pyrolysis of diethyl ether ($C_2H_5OC_2H_5$) as a non-toxic model molecule for yperite ($ClC_2H_5SC_2H_5Cl$) in order to favour the development of a new process for the remediation of soils polluted by heavily toxic chemical. This new apparatus is based on the thermal desorption of the gaseous toxic compounds followed by their thermal decomposition in a dedicated high-temperature tubular reactor maintained at low pressure [1].

However a better knowledge about the gas phase reactions of diethyl ether (DEE) is also useful to favour the use of this molecule as biofuel. Like dimethyl ether, DEE has attractive properties for use in diesel engines, especially a high cetane number (above 125) [2], as well as a higher energy density than dimethyl ether and ethanol. DEE has also been proposed as a possible octane improver in biogas homogeneous charge compression ignition (HCCI) operation [3]. DEE can be produced from the catalytic dehydration of ethanol [2] and is easier to use in engine than dimethyl ether since it is liquid under ambient conditions.

Due to its promising properties as biofuel, the combustion kinetics of DEE has already been investigated using different exper-

imental devices: burners with laminar premixed flames for flame speed measurements [4] or product analyses [5], a burner with non-premixed flames [6], shock tubes for ignition delay time determinations [7,8], a rapid compression machine for ignition delay time measurements [8]. On the other hand, there is only one experimental study about DEE pyrolysis performed in a shock tube [7].

The purpose of the present study is to investigate the pyrolysis of DEE in a jet-stirred reactor (JSR), a type of reactor which has been shown a suitable tool for kinetic studies involving product analyses [9].

2. Experimental methods

The experimental study has been performed using a spherical fused silica JSR (volume of 85 cm^3) inside which the reactants enter through an injection cross made of four nozzles which is located at its center. High turbulence is created by gas jets through the nozzles and leads to homogeneity in composition and temperature of the gas phase. The isothermal JSR is preceded by a quartz annular preheating zone in which the temperature of the gas is increased up to the reactor temperature. The gas mixture residence time inside the annular preheater is very short compared to its residence time inside the reactor (a few percent). Both the reactor and the preheating zone are heated by the means of Thermocoax resistances rolled up around the reactor. The reaction temperature is measured by a thermocouple located inside the intra-annular space of the pre-

* Corresponding author.

E-mail address: Frederique.Battin-Leclerc@univ-lorraine.fr (F. Battin-Leclerc).

heating zone; its extremity being placed at the level of the injection jets.

DEE is provided by Sigma-Aldrich (purity of $\geq 99.5\%$) and used diluted in helium provided by Messer with a purity reported as 99.999%. The gas flow rate is controlled by a mass flow controller, the liquid flow rate by a Coriolis flow controller followed by a vaporization chamber maintained at 323 K. The uncertainty in the flow measurements is around 0.5% for each controller, so about 1% on the residence time.

The outlet gas leaving the reactor is analyzed by two gas chromatographs via a heated transfer line maintained at 433 K to avoid product condensation during transfer. The first chromatograph, equipped with a Carbosphere packed column, a thermal conductivity detector (TCD) and a flame ionization detector (FID), is used for the quantification of CO, methane, ethylene, acetylene and ethane. The second chromatograph is fitted with a PlotQ capillary column and a FID is used for the quantification of other types of molecules. The FID was preceded by a methanizer (nickel catalyst for hydrogenation) which made it possible to detect species like CO and CH₂O with a good sensitivity. The identification of reaction products is performed using a gas chromatograph equipped with a PlotQ capillary column and coupled to a mass spectrometer (quadrupole). Calibrations are performed by injecting standards. The maximum relative error in mole fractions is estimated to be $\pm 5\%$.

3. Results and discussion

DEE pyrolysis has been studied at temperatures from 600 to 1100 K, pressures of 800 and 200 Torr, residence times from 1 to 10 s, reactant inlet mole fractions of 1%, 2%, and 5% with a dilution in helium. All the results are given in a spreadsheet in Supplementary material. Fig. 1 presents the temperature evolution of the DEE conversion which has been obtained for all the studied conditions. This figure shows that DEE starts to be consumed at 825 K and is fully destroyed for a temperature of 1080 K. Fig. 1 also indicates that apart from temperature, the only parameter presenting some significant impact on the DEE reactivity is residence time. This is confirmed by Fig. 2 which displays the evolution of the DEE conversion with residence time and which shows a rise from 16 to 63% when the residence time is increased from 1 to 10 s. At 925 K, a decrease of the pressure from 800 to 200 Torr, for 5% DEE inlet mole fraction and a residence time of 4 s, leads to a decrease of the DEE conversion from 45 to 40%. At the same temperature, a decrease of the DEE inlet mole fraction from 5 to 1%, at 800 Torr and a residence time of 2 s, leads to a decrease of the DEE conversion from 30 to 28%. A steady reactivity increase is observed for DEE inlet mole fraction from 1 to 5%.

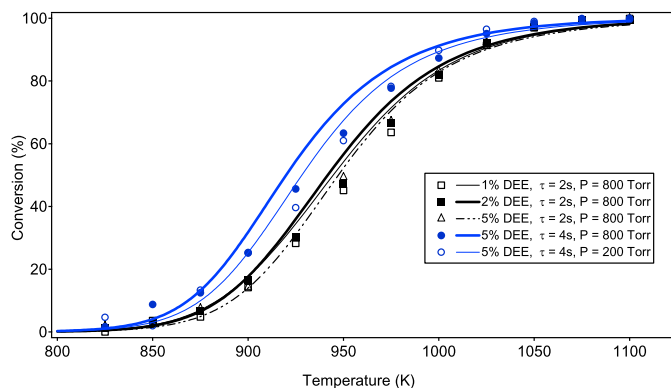


Fig. 1. Temperature evolutions of the DEE conversion for various inlet mole fractions, residence time (τ) and pressure (P). Symbols are experiments and lines simulations with the model of Tran et al. [5].

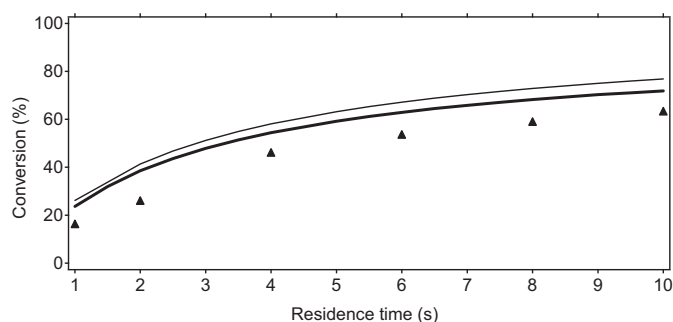


Fig. 2. Evolutions of DEE conversion with residence time ($T=925$ K, 5% DEE inlet mole fraction, $P=800$ Torr). Symbols are experiments, thick lines simulations with the model of Tran et al. [5], and thin lines simulations with the model of Yasunaga et al. [7].

Fig. 3 displays the temperature evolution of the mole fractions of the products obtained during DEE pyrolysis. Two types of products can be distinguished: those presenting a maximum around 1000 K (ethylene, propane, propene, acetaldehyde, ethanol), and those the mole fraction of which continually increases (carbon monoxide, methane, 1,3-butadiene, benzene). Note that while this product should have been detected with our analytical method if it was formed in amounts above 1 ppm, no trace of formaldehyde was detected. Hydrogen was not analyzed. Fig. 4 presents the selectivity at 1000 K of these products showing that the major products are carbon monoxide, methane, ethylene and acetaldehyde. Under every studied condition, the carbon atom material balance is checked to about 10% of the global inlet in atoms of carbon.

Simulations of experimental data were performed using the CHEMKIN package [10] and the OpenSMOKE++ framework [11]. Two literature detailed kinetic models were used:

The model of Yasunaga et al. [7] developed in 2010 to simulate data obtained in shock tubes for the pyrolysis and oxidation of DEE, and based on the C₁–C₄ hydrocarbon chemistry developed in Galway [12].

The brand new model of Tran et al. [5] developed to simulate species profiles obtained in a rich low-pressure laminar flame, and based on a tetrahydrofuran mechanism developed in Nancy [13] which includes a reaction base for C₁–C₄ unsaturated species, and benzene.

The simulations of our experimental results are shown in Figs. 1–3 when using the model of Tran et al. [5] and 2, S1 and S2 (in Supplementary material) when using model of Yasunaga et al. [7]. The agreement between our experiments and simulations using both models are satisfactory for the prediction of DEE conversion and most product formation. While, in the model of Yasunaga et al. [7], the rate constants of the reactions specific to DEE were mainly derived from estimations, in the model of Tran et al. [5], several of them were obtained using quantum chemistry computation method. However, the most recent model does not always lead to significant modeling improvements. Both models reproduce well the decrease of reactivity with pressure at a given temperature, with the model of Tran et al. [5] predicting better the extent of this decrease than the model of Yasunaga et al. [7]. The 2010 model simulates well the steady increase of reactivity when increasing DEE inlet mole fraction at a given temperature (see Fig. S1), which is not the case of the model of Tran et al. [5] which, as shown in Fig. 1, predicts a slight maximum of reactivity for an inlet DEE mole fraction of 2% which is not experimentally observed. Concerning product formation, the model of Tran et al. [5] reproduces well the formation of all the observed species, including 1,3-butadiene and benzene which were not considered in the model of Yasunaga et al. [7]. The only product for which significant deviation is observed between experiments and simulations with the model of Tran et al.

Download English Version:

<https://daneshyari.com/en/article/5134720>

Download Persian Version:

<https://daneshyari.com/article/5134720>

[Daneshyari.com](https://daneshyari.com)