## **ARTICLE IN PRES**

[international journal of hydrogen energy xxx \(2017\) 1](http://dx.doi.org/10.1016/j.ijhydene.2017.06.130) e[5](http://dx.doi.org/10.1016/j.ijhydene.2017.06.130)



Available online at [www.sciencedirect.com](www.sciencedirect.com/science/journal/03603199)

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# Enhancement of hydrogen sorption properties of  $MgH_2$  with a  $MgF_2$  catalyst

## Jong-Sang Youn <sup>a</sup>, Duy-Thach Phan <sup>a</sup>, Cheol-Min Park <sup>b,\*\*</sup>, Ki-Joon Jeon <sup>a,\*</sup>

a Department of Environmental Engineering, Inha University, 100 Inha-ro, Nam-gu, Incheon 22212, Republic of Korea

<sup>b</sup> School of Materials Science and Engineering, Kumoh National Institute of Technology, Gumi, Gyeongbuk 39177, Republic of Korea

#### article info

Article history: Received 18 May 2017 Received in revised form 13 June 2017 Accepted 17 June 2017 Available online xxx

#### Keywords:

Magnesium hydride Additive MgF2 Hydrogen storage Ball milling Crystallinity Grain growth

#### **ABSTRACT**

Effect of a MgF<sub>2</sub> catalyst, prepared by ball-milling, on the hydrogen desorption ability of commercial MgH<sub>2</sub> was investigated. When MgH<sub>2</sub> was catalyzed with a MgF<sub>2</sub> composite, it exhibited good cyclability and sharp faceting, with a small grain size (around 10 nm), which differs from those of pure MgH<sub>2</sub>. The addition of the MgF<sub>2</sub> catalyst suggests that the F anion could significantly contribute to the cyclability of Mg particles and aid in the inhibition of  $MgH<sub>2</sub>$  grain growth.

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#### Introduction

The interest in using hydrogen as an alternative fuel has increased for many applications over the past decade, from mobile electronics to aerospace industries  $[1-3]$  $[1-3]$ . Solid storage of hydrogen using a reversible metal hydride is one of the most promising methods for hydrogen storage  $[3-5]$  $[3-5]$ . Advantages of using reversible metal hydrides include improved safety, reduced environmental impact, and high hydrogen storage capacity. The high temperature required for the formation of metal hydrides with acceptable hydrogen uptake and release kinetics, however, is an important limitation that makes the process expensive [\[3,6,7\]](#page--1-0).

Magnesium-based hydrides, with a reversible hydrogen capacity of up to 7.6 wt% for on-board applications, are promising for hydrogen storage  $[8-10]$  $[8-10]$ . Magnesium hydride, MgH2, has the highest energy density (9 MJ/kg Mg) of all of the reversible hydrides used for hydrogen storage. MgH<sub>2</sub> has a high  $H_2$  capacity of 7.7 wt%, and is low cost, using readily available magnesium that has good reversibility [\[8,9\]](#page--1-0). However, the main disadvantages of using  $MgH_2$ -based hydrogen storage include the high temperature of hydrogen desorption  $(>673 K)$  and its high reactivity in air and oxygen  $[8,9]$ . Technologies currently under research for improving the hydrogen storage of MgH<sub>2</sub>/Mg can be classified into four categories: alloying, nanoscaling, nanoconfinement, and additive-

E-mail addresses: [cmpark@kumoh.ac.kr](mailto:cmpark@kumoh.ac.kr) (C.-M. Park), [kjjeon@inha.ac.kr](mailto:kjjeon@inha.ac.kr) (K.-J. Jeon). <http://dx.doi.org/10.1016/j.ijhydene.2017.06.130>

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Please cite this article in press as: Youn J-S, et al., Enhancement of hydrogen sorption properties of MgH<sub>2</sub> with a MgF<sub>2</sub> catalyst, International Journal of Hydrogen Energy (2017), http://dx.doi.org/10.1016/j.ijhydene.2017.06.130

<sup>\*</sup> Corresponding author.

<sup>\*\*</sup> Corresponding author.

addition [\[11,12\].](#page--1-0) Ball milling/mechanical milling, a current technology, can be used for improving the surface and kinetic properties of MgH<sub>2</sub>/Mg, due to changes caused by structural defects, phase change, and crystallinity  $[8-13]$  $[8-13]$  $[8-13]$ .

Several experiments have been conducted for improving kinetics through ball milling of the bulk of magnesium metal, alloying with transition metal oxides or transition metal fluoride catalysts (such as TiF<sub>3</sub>, NbF<sub>5</sub>, and NiF<sub>2</sub>), and destabilizing the magnesium-transition metal-hydrogen matrix  $[14-20]$  $[14-20]$ . MgH<sub>2</sub> could react with metal fluoride (TiF<sub>3</sub>, NbF<sub>5</sub>, etc.) and form  $MgF<sub>2</sub>$  during the milling and hydrogenation/dehydrogenation processes [\[15,20\].](#page--1-0) Liu and Susa [\[21\]](#page--1-0) reported the formation of a  $MgF_2$  layer on a  $Mg_2Ni$  particle, which suggests that  $MgF<sub>2</sub>$  has a high affinity to hydrogen with a rapid initial activation. Jian et al.  $[22]$  reported the effect of MgF<sub>2</sub> on the hydrogenation properties of MgH<sub>2</sub>, and found that adsorption at a low temperature could be possible, since  $MgF<sub>2</sub>$  was evenly distributed within the MgH<sub>2</sub> powder. They also reported that the presence of chemically stable MgF<sub>2</sub> during hydrogen cycling affected the improvement of sorption ability; however, the actual role of MgF<sub>2</sub> on the dehydrogenation/hydrogenation of MgH<sub>2</sub> powder has not yet been systematically understood. The main objectives of this study were to investigate how the addition of MgF<sub>2</sub> catalyst enhanced the kinetics of the hydrogen desorption mechanism of metal hydride.

#### Experimental method

The methodology used for sample preparation and elements of the hydrogenation system have been described in depth in a previous study [\[23\].](#page--1-0) Therefore, only the experimental conditions are outlined here. MgH<sub>2</sub> particles (nominally 90% pure, with most of the remainder being Mg) were ball milled with 1, 3, and 10 mol%  $MgF_2$  at 400 rpm for 60 min. Hydrogen absorption was measured using a PCT pro 2000 instrument (Hy-Energy, CA). Two conventional transmission electron microscopes (TEM, Zeiss Libra 200 FEG and CM 200 FEG, 200 kV accelerating voltage) were used for electron energy loss spectroscopy (EELS) and high-resolution imaging, respectively. MgH<sub>2</sub> powder was dispersed in hexane to minimize any possible exposure to air [\[24\],](#page--1-0) and a drop of the suspension was deposited onto a Cu TEM grid in an argon glove box directly before the TEM session. The EELS technique was used to map the fluorine distribution of  $MgH_2-MgF_2$  composites. The x-ray diffraction patterns of  $MgH_2-MgF_2$  composites (as-synthesized, and after 3rd and 6th desorption of  $MgH_2-MgF_2$ ) were identified with reference to the diffraction patterns of hexagonal Mg (JCPDS 04-0770), tetragonal MgH<sub>2</sub> (JCPDS 12-0697), and tetragonal  $MgF_2$  (JCPDS 38-0882), respectively.

### Result and discussion

#### Determination of optimal  $MqF_2$  loading conditions

Distribution and dispersion of the catalyst over the surface of magnesium particles are critical in determining hydrogen absorption and desorption kinetics. The effect of  $MgF_2$  loading was evaluated using 1, 3, and 10 mol%  $MgF_2$  (Fig. 1).



Fig. 1 – Effect of the addition of MgF<sub>2</sub> on hydrogen desorption capacities/kinetics. (desorption at 673 K and 0 bar).

The MgH<sub>2</sub>-x mol% MgF<sub>2</sub> (x = 1, 3, and 10) composites show greater hydrogen desorption capacities than that of pure Mg at 673 K. The amount of hydrogen desorbed from  $MgH_2$  with 3 and 10 mol%  $MgF_2$  was 6.49 and 5.85 wt%, respectively, while uncatalyzed MgH<sub>2</sub> released 4.44 wt% of hydrogen (Fig. 1). In contrast, a 1 mol% MgF<sub>2</sub> sample desorbs 4.31 wt% of hydrogen, less than that of the pure  $MgH<sub>2</sub>$  sample, which is likely due to the insufficiency of  $MgF<sub>2</sub>$  in prohibiting the Mg grain growth. The composite processed with 3 mol%  $MgF<sub>2</sub>$  has a significantly higher hydrogen desorption capacity than that of the composite with 10 mol%  $MgF_2$ , which could render this composite less practical for onboard storage. Higher catalyst loading might increase the number of favorable  $H_2$  dissociation sites; therefore, it increased the hydrogen dissociation [\[25\].](#page--1-0) In contrast, lower catalyst loading might not sufficiently cover



Fig.  $2$  – Effect of the addition of fluoride on the cycling behavior of MgH<sub>2</sub> (desorption at 673 K and 0 bar, and absorption at 573 K and 45 bar, composites milled for 1 h at 400 rpm with no transition metal catalyst added).

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