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# Accurate interface normal and curvature estimates on three-dimensional unstructured non-convex polyhedral meshes

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### ABSTRACT

This paper presents a framework for extending the height-function technique for the calculation of interface normals and curvatures to unstructured non-convex polyhedral meshes with application to the piecewise-linear interface calculation volume-of-fluid method. The methodology is developed with reference to a collocated node-based finitevolume two-phase flow solver that utilizes the median-dual mesh, requiring a set of data structures and algorithms for non-convex polyhedral operations: truncation of a polyhedron by a plane, intersection of two polyhedra, joining of two convex polyhedra, volume enforcement of a polyhedron by a plane, and volume fraction initialization by a signed-distance function. By leveraging these geometric tools, a geometric interpolation strategy for embedding structured height-function stencils in unstructured meshes is developed. The embedded height-function technique is tested on surfaces with known interface normals and curvatures, namely cylinder, sphere, and ellipsoid. Tests are performed on the median duals of a uniform cartesian mesh, a wedge mesh, and a tetrahedral mesh, and comparisons are made with conventional methods. Across the tests, the embedded height-function technique outperforms contemporary methods and its accuracy approaches the accuracy that the traditional height-function technique exemplifies on uniform cartesian meshes.

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#### 1. Introduction

The volume-of-fluid (VOF) method is one of the most widely used formulations to simulate interfacial and free-surface flows [1]. In this method, the interface evolution is implicitly tracked using a discrete function, F, representing the volume fraction of the tagged fluid within a cell of the computational mesh. F is a discretized version of the fluid marker function, f, that is constant in each phase, jumps at the interface from 0 to 1, and follows the scalar advection equation,

$$\frac{\partial f}{\partial t} + \vec{v} \cdot \nabla f = 0,$$

where  $\vec{v}$  is the velocity vector.

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The piecewise-linear interface calculation (PLIC) has become the standard interface representation within the VOF community [2]. PLIC-VOF methods describe the interface by a series of disconnected planes, each oriented by a unit normal,  $\hat{n}$ , and positioned by a constant, *C*, such that  $\hat{n} \cdot \vec{x} + C = 0$ . Two key steps in any PLIC representation include volume truncation by a fixed plane, i.e. determination of *F* given  $\hat{n}$  and *C*, and volume enforcement by a movable plane, i.e. determination of *C* given  $\hat{n}$  and *F*. The importance of the volume truncation and enforcement operations has led researchers to develop analytic and geometric tools to expedite computations for rectangular and hexahedral elements [3], for triangular and tetrahedral elements [4], and for convex polyhedral elements [5]. In this paper, we extend the class of geometric tools to non-convex polyhedral meshes in order to implement the PLIC-VOF method in a collocated node-based finite-volume flow solver [6]. As evidenced by the volume enforcement and truncation operations, estimation of  $\hat{n}$  is key to the accuracy of any PLIC-VOF method.

The equations governing the motion of an unsteady, viscous, incompressible, immiscible two-fluid system are the Navier– Stokes equations, augmented by a localized surface tension force,

$$\rho\left(\frac{\partial\vec{v}}{\partial t} + \vec{v}\cdot\nabla\vec{v}\right) = -\nabla p + \nabla\cdot\left(\mu\left[\nabla\vec{v} + \{\nabla\vec{v}\}^T\right]\right) - \sigma\kappa\hat{n}\delta_S, \nabla\cdot\vec{v} = 0, \kappa = \nabla\cdot\hat{n},$$
(2)

where,  $\rho$  is the density, p is the pressure,  $\mu$  is the viscosity,  $\sigma$  is the surface tension coefficient,  $\kappa$  is the interface curvature, and  $\delta_S$  is the Dirac Delta function localized to the surface *S*. As evidenced by Eq. (2), in addition to accurately estimating  $\hat{n}$ , the PLIC-VOF framework also needs to calculate the rate at which  $\hat{n}$  turns along the interface, i.e. the curvature,  $\kappa$ .

Determination of  $\hat{n}$  and  $\kappa$  in the VOF method is problematic due to the discontinuous nature of F. Nevertheless, various algorithms to calculate  $\hat{n}$  and  $\kappa$  have been proposed. The traditional Parker–Youngs (PY) method [7] uses simple difference formulas to calculate gradients in F for the estimation of  $\hat{n}$ . The method has been implemented on nonorthogonal [8] and unstructured meshes [9]; however, the PY method is at most first-order accurate because  $\hat{n}$  for a rectilinear interface is not calculated exactly, a necessary condition for second-order accuracy [10]. The least-squares fit procedure [11,12] is more accurate than the PY method and has been extended to unstructured meshes [13]; however, it too does not satisfy the necessary condition for a second-order method. Several second-order methods for estimating  $\hat{n}$  have been proposed, namely the least-squares volume-of-fluid interface reconstruction algorithm (LVIRA) and the efficient least-squares volume-of-fluid interface reconstruction algorithm (ELVIRA) for structured grids [10], and the geometric least-squares (GLS) method for unstructured grids [14], each able to reconstruct a rectilinear interface exactly. LVIRA orients  $\hat{n}$  such that the discrepancy in F from using the calculated linear interface over a neighborhood of cells is minimized in the least-squares sense. The procedure requires costly geometric iterations in which volume enforcement and volume truncation steps must be performed for each cell. ELVIRA bypasses the iterations by selecting  $\hat{n}$  amongst a set of candidates constructed from the centered, backward, and forward estimates in each direction. The GLS method follows the procedure of LVIRA, requiring geometric iterations within an unstructured framework - a prohibitively costly procedure. A well-known non-iterative method for estimating  $\hat{n}$  is the height-function (HF) technique. In the HF method, F is integrated in the cartesian direction closest to  $\hat{n}$ (approximated with a simpler method) to calculate a height, H. Slopes of a local H distribution in the other two cartesian directions are used to correct  $\hat{n}$  [15–17]. The HF method was shown to be second-order accurate with proper handling for particular alignments of the interface with respect to the grid lines [18,19]. In two dimensions, the method was extended to nonuniform rectangular grids [20] and, by adapting the definition of H and using a least-squares fit, to unstructured rectangular/triangular grids [21], both exhibiting second-order convergence in  $\hat{n}$ .

As shown in Eq. (2),  $\kappa$  requires higher differentiability than that of  $\hat{n}$ . To address the lack of differentiability of F, various methods have been posited to calculate  $\kappa$ . In the convolved VOF (CV) method, F is convolved with a smoothing kernel to provide a smoothed-out distribution from which the second derivates can be calculated [15,22]. The reconstructed-distance function (RDF) method builds a signed-distance function away from the interface to provide a smooth field from which  $\kappa$ can be calculated [15]. The RDF technique was extended to unstructured rectangular/triangular meshes [23]. Both the CV and RDF methods have shown lack of convergence under refinement on structured [15] and unstructured [21] meshes. In addition to the calculation of  $\hat{n}$ , the HF method has been used to calculate  $\kappa$  [15], demonstrating second-order accuracy over a series of canonical test problems on uniform cartesian meshes [18,24,25]. In two dimensions, the calculation of  $\kappa$ with the HF method was extended to nonuniform rectangular grids without loss of the second-order convergence [20]. The HF technique was extended to two-dimensional unstructured rectangular/triangular grids [21]; however, the reframed definition of H required quadric fitting to calculate  $\kappa$ , and the method was less than first-order accurate. An HF method with  $\hat{n}$ -aligned columns of variable H was shown to improve the  $\kappa$  calculation accuracy on coarse meshes; however, it required a neighborhood search step to compute intersections with the mesh and the columns [26]. The HF method was also adapted to quad and octree discretizations [27], where cartesian stencils of varying H (in addition to parabolic fitting for stencils with ill-defined H) were used to obtain second-order accuracy. To the best of our knowledge, the HF technique for calculating  $\hat{n}$  and  $\kappa$  has not been extended to three-dimensional unstructured meshes. Furthermore, a convergent method to calculate  $\kappa$  on unstructured meshes has not been published.

In this paper, we extend the HF technique for estimating  $\hat{n}$  and  $\kappa$  to three-dimensional unstructured non-convex polyhedral meshes. The method embeds structured HF stencils in the unstructured mesh and interpolates the mesh *F* data to

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