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C–O bond formation in a microfluidic reactor: high yield S_NAr substitution of heteroaryl chlorides

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ABSTRACT

This study describes our development of a novel and efficient procedure for C–O bond formation under mild conditions, for coupling heteroaryl chlorides with phenols or primary aliphatic alcohols. We utilized a continuous-flow microfluidic reactor for C–O bond formation in electron-deficient pyrimidines and pyridines in a much more facile manner with a cleaner reaction profile, high yield, quick scalability, and without the need for the transition metal catalyst. This approach can be of general utility to make C–O bond containing intermediates of industrial importance in a continuous and safe manner.

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Introduction

In both academia and industry, carbon–oxygen (C–O) bond forming reactions are of great utility as these bonds are ubiquitous in natural products, polymers, and biologically active molecules.¹ Some examples of bioactive molecules incorporating the C–O bond are shown in Figure 1. Puromorphamine is a Hedgehog-signaling pathway activator, an important regulator of stem cell renewal and cancer growth,² BMS-777607 at therapeutic doses acts as a multi-kinase inhibitor,³ and bispyribac-sodium is used as a herbicide.⁴

Traditionally, C–O bonds are formed using nucleophilic aromatic substitution (S_NAr). Copper-mediated Ullmann coupling has typically been used for the synthesis of aryl ethers from aryl bromides/iodides and phenols, but it is characterized by a harsh reaction conditions and the need for stoichiometric amount of metal.⁵ In the last decade, many groups have switched to Buchwald methodology, which utilizes a catalytic amount of copper and various ligands to generate the aryl ethers.⁶ There are substantial precedents where S_NAr reactions were performed on activated aryl halides in flow under both traditional and microwave heating.⁷ More recently, Charaschanya et al. have reported high-temperature and high-pressure S_NAr reactions of heterocycles with various nitrogen nucleophiles.⁸ Although significant advances have been achieved in this area, the development of a more efficient, mild, economical, and green strategies for the C–O bond formation still

constitutes a significant synthetic challenge. Pertinent to our hit-to-lead optimization work, improvement of such strategies would facilitate synthesis of analogs for biological analysis as part of our drug discovery efforts. Our interest is in finding an alternative, green chemistry approach to the precious transition-metal catalyzed C–O coupling reactions. To the best of our knowledge microfluidic reactor-based, rapid and high yield C–O bond formation under mild conditions, as described in this manuscript, has not been previously reported. Our approach, described herein, supplements the traditional C–O bond-forming reactions described above. Furthermore, it also reveals the benefits of using a continuous-flow microfluidic reactor, which include the following: short reaction times, superior mixing, efficient heat transfer, increased pressures, and the use of less reactive reagents that result in a high yield reaction.^{9–17}

Results and discussion

In conventional batch reactions, dichloropyrimidine exhibits a low reactivity as compared to its bromo- or iodo-counterpart.¹⁸ Consequently, the C–O bond formation using this intermediate is slow and takes many hours even under the metal catalysis.¹⁹ In the initial phase of development of our method, we used 4,6-dichloro-2,5-dimethylpyrimidine and 4-methoxy-2-methylphenol to study the effects of temperature, pressure, and solvent on the yield of C–O bond formation (Table 1) in the continuous-flow microreactor. Traditionally, 4,6-dichloro-2,5-dimethylpyrimidine is coupled with 4-methoxy-2-methylphenol after treatment with sodium hydride (60% suspension in oil) in DMF for 5–10 h.²⁰

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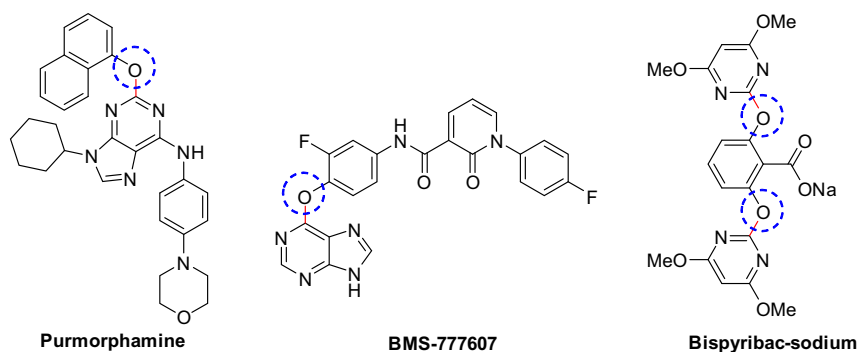
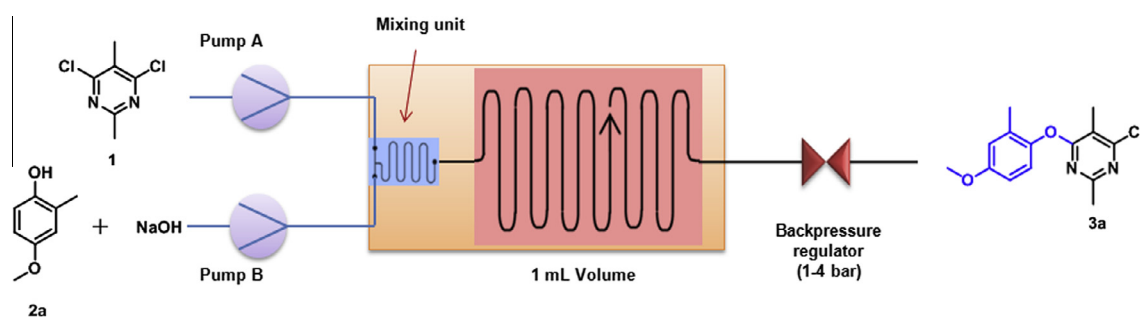


Figure 1. Examples of bioactive molecules containing C–O bond.

Table 1
Effect of temperature and pressure on yield of C–O bond formation



Entry ^a	Solvent	T (°C)	P (bar)	Flow rate ^b (μL/min)	t _R ^c (min)	Yield ^d (%)
1	THF	66	1	500	2	6
2	THF	66	1	250	4	12
3	THF	66	1	100	10	19 (clog)
4	THF	66	1	50	20	30 (clog)
5	THF	76	2	50	20	45 (clog)
6	THF	90	4	50	20	55 (clog)
7	THF–H ₂ O	90	4	50	20	54
8	THF–H ₂ O	100	4	50	20	71
9	THF–H ₂ O	110	4	50	20	87

^a Synthesis of compound **3a** was done under varying conditions (entries 1–9); two solutions were prepared and introduced by Pump A & B into the Asia microfluidic reactor; one contained the aryl halide **1** (0.56 mmol, 1.0 equiv) in THF–H₂O (2.5 mL, 3:2 v/v) and the other contained a mixture of phenol **2a** (0.84 mmol, 1.5 equiv) and NaOH (0.84 mmol, 1.5 equiv) in THF–H₂O (2.5 mL, 3:2 v/v).

^b Flow rates of the combined solutions.

^c Retention time (in a 1 mL microfluidic reactor).

^d Yield determined by LCMS.

However, sodium hydride (60% suspension in oil) cannot be used in a microfluidic reactor due to clogging of either the back pressure regulator or the microfluidic reactor chip. Thus, we used THF as the solvent and NaOH as the base to generate the required phenoxide. Under these conditions, using a temperature of 60 °C, and 1 bar pressure, the expected monophenoxy derivative, **3a**, was formed in varying yields depending on residence time in the reactor. We obtained yields of 6%, 12%, 19% and 30% with flow rates of the combined solution being 500 μL/min, 250 μL/min, 100 μL/min, and 50 μL/min, respectively (Table 1, entries 1–4). This corresponded to residence times of 2, 4, 10, and 20 min, respectively, in the 1 mL microfluidic reactor. To improve yields we evaluated the reaction at 76 °C and 90 °C under 2 bar and 4 bar pressure, respectively. The temperature and/or pressure changes in the microreactor were done easily, using the Asia chip climate controller (–10 °C to +150 °C range) and the Asia pressure controller (1–10 bar range). Using the higher temperature and pressure, the product yield was shown to be increased to 45% and 55%, respectively (Table 1, entries 5 and 6). However, under these conditions,

clogging of the microfluidic reactor or back pressure regulator was observed after a few runs, likely due to the deposition of NaCl. To solve the clogging issue, the reaction solvent was combined with water to remove NaCl formed as a byproduct. Switching the solvent to THF–H₂O (3:2 v/v) provided a similar yield of 54% at 90 °C, 4 bar pressure, using the combined flow rate of 50 μL/min without any observed clogging. Further increase of temperature while maintaining the 4 bar pressure was also evaluated to determine if there was any improvement of reaction yield. To our delight, using the THF–H₂O solvent system and the combined flow rate of 50 μL/min (Pump A & B at 25 μL/min each), the target coupling product yield increased to 87% when reactor temperature was maintained at 110 °C and 4 bar pressure (entry 9). Under these conditions no clogging of the glass microfluidic reactor chip or the back pressure regulator was observed. Additional increases in reactor temperature to 120 °C and above did not improve the product yield and, interestingly, clogging of the microfluidic reactor chip was once again observed. Therefore, for further studies with pyrimidine **1**, temperature, pressure and combined flow rate were

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