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## Influence of accelerating gas flow rate on the particle cohesion in room temperature cold sprayed scattering layer for plastic-based dye-sensitized solar cells

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#### a r t i c l e i n f o

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#### **1. Introduction**

Plastic-based dye-sensitized solar cells (DSCs) are being rapidly developed, owing to their advantages such as low cost, lightweight, flexibility, environmental friendliness and possibly colorful decorative appearance [\[1\].](#page--1-0) However, the cell efficiency is limited by the insufficient electron transport property of the nano-porous  $TiO<sub>2</sub>$ film in which only a weak connection is formed during the preparation of TiO<sub>2</sub> film at low temperature  $[2,3]$ . A feasible approach to improve the conversion efficiency is to add a scattering layer composed of large particles with a diameter of 100–400 nm on the surface of TiO<sub>2</sub> nanocrystalline (NC) layer  $[4-6]$ . Typically, TiO<sub>2</sub> scattering layer was prepared by casting  $TiO<sub>2</sub>$  paste with an organic binder on glass substrate, followed by sintering at a temperature above 450 ◦C to burn offthe organic binder. However, for the plastic substrate-based DSCs, this conventional preparation method using high-temperature annealing is not applicable, owing to the low heat-resistance temperature (150 $\degree$ C) of the plastic substrates [\[7\].](#page--1-0) Therefore, it is still a challenge to effectively prepare light scattering layer for plastic-based DSCs.

Room temperature cold spraying (RTCS, also called vacuum cold spray) method can be used to deposit nano-TiO<sub>2</sub> coating with good

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#### A B S T R A C T

Mesoporous TiO2 coating was prepared by room temperature cold spraying with submicro-sized anatase TiO2 powder for scattering layer in plastic-based DSCs. The effect of accelerating gas flow rate on the microstructure, cohesion and optical property of the as-prepared TiO2 scattering layers was investigated. Results showed that the cohesion of the TiO<sub>2</sub> scattering layer increased with the increase of accelerating gas flow rate due to the improved particle–particle connection by the particle impact at an increased velocity. The light-reflecting ability of the TiO<sub>2</sub> scattering layers increased with the increase of coating thickness from 2 to 10  $\mu$ m and decreased with the increase of accelerating gas flow rate from 3.5 to 7.5 L/min. By adding the scattering layer to the photoanode of the plastic-based DSCs, the conversion efficiency of the plastic-based DSCs was increased by a factor of 21% to 4.70%.

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particle–particle connection on plastic substrate for photoanode of flexible DSCs  $[8,9]$ . During the RTCS process, TiO<sub>2</sub> powder particles are accelerated to a high velocity (100–300 m/s) by a gas flow and deposited on a substrate surface to form  $TiO<sub>2</sub>$  coating in a low pressure environment of several hundreds of pascals. The impact of powder particles at a high velocity on the substrate surface generates a high pressure pulse, leading to the formation of good connection between TiO<sub>2</sub> particles  $[8,10]$ . Owing to the feature of low-temperature process, RTCS process may be used to solve the problem involved in the deposition of scattering layer with good particle–particle connection in plastic-based DSCs.

In this study, RTCS method was used to prepare  $TiO<sub>2</sub>$  coating as light scattering layer using submicro-sized anatase  $TiO<sub>2</sub>$  powder. The ultrasonic test was used to quantitatively evaluate the cohesion of the coatings. The influence of accelerating gas flow rate on microstructure, cohesion and optical property of the coatings was explored to aim at understanding the microstructure/property relationship. The performance of these coatings as scattering layers for the plastic DSCs was investigated.

#### **2. Experimental**

#### 2.1. TiO<sub>2</sub> coating preparation

Commercially available submicro-TiO<sub>2</sub> (anatase) powder ([Fig.](#page-1-0) 1) of 100–200 nm in diameter was used as feedstock in this study for





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Fig. 1. Surface morphology of the submicro-TiO<sub>2</sub> powder.

light scattering layer. TiO<sub>2</sub> coatings were deposited by a homedeveloped RTCS system. The RTCS system consists of a vacuum pump, a vacuum chamber, a power feeder, an accelerating gas feeding unit, a particle accelerating nozzle, a two dimension worktable and a control unit  $[11,12]$ . Helium was used as the accelerating gas at a pressure of 0.2 MPa. The chamber pressure during spraying was about  $10^2$ –10<sup>3</sup> Pa. The standoff distance from the nozzle exit to the substrate surface was 10 mm. The relative traverse speed of the nozzle over the substrate was 20 mm/s.

To assemble the plastic-based DSC, the TiO<sub>2</sub> NC layer was deposited with the P25 nano-TiO<sub>2</sub> powder (Degussa, 70% anatase and 30% rutile) with a diameter of 25 nm at a gas flow rate of 7 L/min on indium-doped tin oxide coated polyethylene naphthalate (ITO-PEN, PECF-IP, 15  $\Omega$  sq<sup>-1</sup>, Peccell) substrate. For the deposition of  $TiO<sub>2</sub>$  scattering layer, the submicro-TiO<sub>2</sub> powder with a diameter of 100–200 nm was used, and the accelerating gas flow rate was set at 3.5, 4.5, 6, and 7.5 L/min.

#### 2.2. Characterization of TiO<sub>2</sub> coatings

The microstructure of  $TiO<sub>2</sub>$  scattering layer was examined by a field emission scanning electron microscope (FESEM, QUANTA 600F). The light-reflecting ability of the  $TiO<sub>2</sub>$  scattering layer was evaluated by measuring the reflectance spectrum of the  $TiO<sub>2</sub>$  scattering layer by a UV–vis spectrophotometer equipped with an integrating sphere setup (JASCO V-570). The sphere as well as the reference plates is coated with BaSO<sub>4</sub>. Considering the flexibility of the ITO-PEN plastic substrate, the TiO<sub>2</sub> scattering layers were deposited on a rigid conductive FTO-glass substrate (TEC 15, LOF) to facilitate the measurement. In all measurements, the light was incident from the bare FTO-glass side to the coated side. The coating thickness was measured by a profilometer (XP-2, AMBIOS Technology, Inc., USA).

The cohesion of the TiO<sub>2</sub> scattering layer was evaluated by ultrasonic test using an ultrasonic cleaner (VGT-1730T, 120W, Xi'an Coming Ultrasonic Equipment Instrument Co., Ltd. China). To facilitate the measurement, the  $TiO<sub>2</sub>$  scattering layers were deposited on FTO-glass substrate. Before coating deposition, the FTO-glass substrates were weighed on an electronic analytical balance (BT224S, Sartorius, Germany) with a precision of 0.1 mg. After the scattering layer deposition, the TiO<sub>2</sub> scattering layers were ultrasonic tested in ethanol solution for different durations. Then the scattering layers were dried at 100 ℃ for 10 min to obtain the dry weight. The relative weight loss was used to evaluate the cohesion of the TiO<sub>2</sub> scattering layer, as the thickness of all samples was kept at 10  $\mu$ m. The cross-sectional morphologies ofthe scattering layers after different ultrasonic test durations were also observed by FESEM.

#### 2.3. Fabrication and characterization of plastic-based DSCs

To prepare the photoanode for the plastic-based DSCs, the  $TiO<sub>2</sub>$ NC layer with a  $TiO<sub>2</sub>$  scattering layer on the ITO-coated plastic substrate was immersed in an absolute ethanol solution of 0.3 mM N719 dye (Solaronix) for 24 h, followed by cleaning with absolute ethanol. Then, the photoanode was assembled with plastic Pt CE using a 60  $\mu$ m thick Surlyn film (1702, DuPont) as a spacer. The electrolyte solution was introduced into the cell through a hole predrilled on the back of the plastic CE, and then the hole was sealed up using a UV resin (ThreeBond). The electrolyte solution was composed of  $0.6 M$  DMPII (Institute of Plasma Physics),  $0.05 M$  I<sub>2</sub> (Aldrich), 0.1 M LiI (Aldrich), and 0.5 M 4-tert-butylpyridine (Acros) in dehydrated acetonitrile (Aldrich).

The photovoltaic performance of the plastic-based DSCs was measured using a solar simulator (100 mWcm−2, Oriel 94023A, Newport) equipped with a Keithley 2400 digital source meter. The active area of the photoanode was  $0.4 \text{ cm}^2$ . The monochromatic incident photon-to-current conversion efficiency (IPCE) of the DSCs was measured by an IPCE measurement system (7-SCSpec, Beijing 7-star Optical Instruments Co. Ltd).

#### **3. Results and discussion**

#### 3.1. Microstructure of the TiO<sub>2</sub> scattering layer

[Fig.](#page--1-0) 2 shows the surface morphologies of the  $TiO<sub>2</sub>$  scattering layers prepared by RTCS method under different accelerating gas flow rates. As can be seen from [Fig.](#page--1-0) 2, the surface morphologies of the  $TiO<sub>2</sub>$  scattering layers prepared under different accelerating gas flow rates were similar. The scattering layers were formed by the stacking of  $TiO<sub>2</sub>$  particles with a size of 100–200 nm which was comparable to that in spray powder (Fig. 1). It is known that the impact of solid particles on the substrate surface forms a coating during the RTCS process [\[13\].](#page--1-0) In order to investigate whether the  $TiO<sub>2</sub>$  primary particles fractured during the high velocity impact in the RTCS process, the cross-sectional morphologies of the fracture TiO<sub>2</sub> scattering layers were observed. [Fig.](#page--1-0) 3 shows the cross-sectional morphologies of the fracture  $TiO<sub>2</sub>$  scattering layers prepared under different accelerating gas flow rates. It was obvious that the  $TiO<sub>2</sub>$  particles in all the scattering layers presented a similar nearly spherical morphology comparable to the spray powder particles (Fig. 1). This result suggested that the powder particle did not fracture or deform significantly during the coating deposition.

#### 3.2. Cohesion of the TiO<sub>2</sub> scattering layer

The good particle–particle connection in the scattering layer is essential for the application of scattering layer. In this study, in order to estimate the cohesion of the  $TiO<sub>2</sub>$  scattering layer, an ultrasonic test was used. [Fig.](#page--1-0) 4 shows the relative weight loss of the  $TiO<sub>2</sub>$  scattering layer prepared under different accelerating gas flow rates as a function of ultrasonic test duration. As can be seen from [Fig.](#page--1-0) 4, the change of the relative weight loss of the  $TiO<sub>2</sub>$  scattering layer prepared under different accelerating gas flow rates exhibited the similar dependency with the ultrasonic test duration. The relative weight loss of the scattering layer increased with the increase of ultrasonic test duration. However, the specific weight loss was significantly different. After 120 s ultrasonic test, the relative weight loss of the scattering layer decreased from 80 to 11% Download English Version:

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