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Estimation of asphaltene precipitation and equilibrium properties of hydrocarbon fluid phases using PC-SAFT equation of state

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ABSTRACT

Most of the components of heavy oil contain coarse grained molecules and it is impossible to estimate the density 21 and phase behavior of such fluids by cubic equations of state (EOSs). Meanwhile, equations of Statistical Associ- 22 ated Fluid Theory (SAFT) have shown much success due to their high ability to calculate fluid's density. Among 23 them is the PC-SAFT theory which despite being introduced about a decade ago, has not been vastly used in 24 the industry and commercial software packages. In this survey, an alternative to describe fluids containing coarse 25 grained molecules in high pressures is presented, using the PC-SAFT theory. Then, some properties of oil such as 26 fluid's density, bubble- and dew point, phase envelop and asphaltene precipitation, are estimated by declaring 27 the definition of applicable algorithms. Precipitation of asphaltene in different stages of crude oil production 28 causes formation damage, choking in pipe lines and wells and the production system. Therefore, estimating 29 the asphaltene behavior in a crude oil looks vital. One of the major purposes of the present work is to investigate 30 the asphaltene phase behavior which is solely accomplished by modeling as a function of temperature, pressure 31 and composition. Despite the previous SAFT modeling, the method of calculating the amount of asphaltene pre- 32 cipitation is based on the solid model. Qualitatively, this model is compared with experimental data which are 33 obtained from adjoining a solvent (nC_5 to nC_9) with heavy oil, to observe its prosperity in predicting asphaltene 34 precipitation. In this comparison, the average error percentage yielded an interval of 5 to 12% for the asphaltene 35 precipitation weight percentage. Except the association term, the repulsive and attractive molecular interaction 36 terms are considered for the present approach. Therefore, the model input includes the oil pseudo-components, 37 PC-SAFT parameters and interaction coefficients between components. To model asphaltene precipitation using 38 the PC-SAFT equation of state, the system is considered as vapor-liquid-quasi-liquid so that its equilibrium helps 39 modeling, considering asphaltene as a quasi-liquid pure phase. The main privilege of estimating asphaltene pre- 40 cipitation by the method presented in this study over the solid model is that it does not need to adjust the volume 41 shift parameter, whereas it is essential when using cubic EOSs. 42

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48 **1. Introduction**

The modeling of phase equilibrium and thermodynamic properties of hydrocarbon phases or phase behaviors of fluids requires a reliable method so that researchers can optimize the best condition for production. Generally, there are two categories of models by which scientists successfully carry out the computations of fluid properties such as

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http://dx.doi.org/10.1016/j.molliq.2015.05.003 0167-7322/© 2015 Published by Elsevier B.V. those of densities, phase equilibrium and prediction of hydrocarbon 54 components asphaltene precipitation. The first one is a cubic equation 55 of state (EOS). Commercial software packages usually use sorts of EOS 56 models in their phase behavior estimations. Among the most favorable 57 EOSs are the Peng–Robinson (PR) and Soave–Redlich–Kwong (SRK) 58 equations that fail to estimate adequate results for aromatics at high 59 pressures in the presence of polymers with polar or associating solvents 60 and generally a volume correction is needed to match results with those 61 obtained by EOSs [1]. Prediction of the thermodynamic properties of 62 such systems is appealing to industry. Therefore, the second group of 63 models which is based on Statistical Associated Fluid Theory (SAFT) 64 EOS, can be a suitable substitute for the cubic EOSs in which a volume 65 correction is not needed to match the SAFT equation of state with exper-66 imental PVT data [1]. 67

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68 SAFT is a molecular approach to demonstrate macroscopic systems 69 and so far has had limited applications in chemical engineering. It can be declared that the first article about application of SAFT was published 70 71 by Chapman and co-workers in the 1990s [2,3] that was based on the first order perturbation theory of Wertheim [4]. In SAFT theory, the 72Helmholtz free energy of components is totally introduced with the 73 74sum of hard sphere repulsion, dispersion interactions, chain connectiv-75ity and association terms. This theory defines fluid as molecules with 76chain of bonded spherical segments. The physical parameters required 77 for calculating properties of fluid involve the number of segments in a 78chain molecule, volume of a segment and the segment-segment Van der Waals attraction. The SAFT equation also has the ability to predict 79 the association interaction between each of the molecules, but it 80 81 needs at least two more parameters for each associating component. The SAFT model can be applied to numerous groups of components 82 such as amphiphilics, aromatics, polymers and alcohols to obtain their 83 phase behaviors [5]. Many years later after introduction of SAFT, modi-84 fied equations such as S-SAFT, soft-SAFT, MS-SAFT and PC-SAFT in the 85 aim of promoting the calculation procedure of the SAFT terms were pre-86 sented by authors [6–9]. At the first, the perturbed chain SAFT (PC-87 SAFT) equation of state was invented by Gross and Sadowski in 2001. 88 89 PC-SAFT is the promotion of SAFT and is somehow derived based on 90 it. Because a hard chain fluid serves as a reference for perturbation theory rather than the spherical molecules, in the PC-SAFT the dispersion 91 energy depends on a mixture of hard chains not only on hard spheres. 92PC-SAFT has wide use in modeling phase equilibriums and phase behav-93 iors of mixtures of alkanes, branched alkanes, cycloalkanes and other 9495 hydrocarbon compound series [9,10]. Recently, the studies about PC-SAFT have been developed, especially by introducing new methods to 96 97determine PC-SAFT parameters for the heavy end components of reser-98 voir fluids [1,11,12]. But among its most important applications, PC-SAFT can reliably be applied to polymers and coarse-grained molecules 99 100such as asphaltenes.

Crude oil is a mixture of several hydrocarbons and other compounds 101 and in a famous category, these components are listed into saturates, 102aromatics, resins and asphaltenes (SARA) [13-15]. Asphaltene is 103104 referred to heavy and highly viscous materials that can exist in 105 petroleum reservoir fluids and cause choking in wells and pipelines [14,16,17]. Asphaltenes contain simple heteroatoms (C, H, N, O, and 106 S) accompanied, most times, by metal constituents (Fe, Ni, and 107 V) having aromatic cyclic structures with alkyl side chains [13–15]. 108 109 Asphaltene is often insoluble in n-pentane and n-heptane in room temperature, but is highly soluble in benzene and toluene. More informa-110 tion about nature of other oil fractions (saturates, aromatics and 111 resins) exists at previous literatures [13,14]. 112

Changes of operational conditions such as pressure and temperature 113 114 as well as fluid composition changes can develop the opportunity of asphaltene precipitation. Specifically, the effect of temperature on 115asphaltene stability is an issue under survey and study. The influence 116 of temperature increase on solubility of asphaltene has been investigat-117 ed by several authors and different results have been reported [18-21]. 118 119 Deeper investigations revealed that the very specific effect of tempera-120ture is on the parameter of asphaltene solubility in oil. For example, Verdier et al. [22] injected CO₂ to two oil samples in different conditions 121and proved that the parameter of asphaltene and oil solubility is a func-122tion of temperature and by use of an appropriate approximation, they 123124found the effect of temperature on solubility of asphaltene. By this explanation, they showed that such controversial views about the temper-125ature influence on the amount of asphaltene precipitation can be 126 justified by the Le Chatelier Principle and the solubility parameter. 127Asphaltene precipitation occurs in a bounded region called asphaltene 128deposition enveloped (ADE). This region is qualitatively shown in 129Fig. 1 for an oil sample in P vs. mole-solvent coordinates in a constant 130temperature. As the oil pressure drops during production above the 131 bubble point of some crude oils, especially those containing high frac-132133 tions of saturates, asphaltenes may precipitate. During enhanced oil



Mole of Solvent injetion

Fig. 1. Qualitative view of asphaltene deposition enveloped region in pressure vs. mole of solvent.

recovery when compressed gases, such as methane (or natural gas) or 134 carbon dioxide, are injected into the reservoir, asphaltenes may also 135 precipitate because it alters the reservoir fluid characterization [13]. 136 The boundary between oil–asphaltene and oil–gas–asphaltene which 137 is on the fluid's bubble point, includes the maximum amount of 138 asphaltene precipitation [23–25].

There are many definitions to describe the nature of asphaltene [26] 140 of which some assume asphaltene as a solid phase [27,28] and some 141 take it as a class of highly viscous liquids [29-31]. Authors attributed 142 the asphaltene precipitated phase to operation temperature, where 143 solid phase would appear into crude oil at room temperature, while 144 the liquid state appears at higher temperatures [24,32]. This latter 145 point of view even exists in reversibility of asphaltene precipitation. 146 Some authors believe that the precipitated asphaltene is irreversible 147 and thus cannot return to a soluble state, while others oppositely have 148 admitted the possibility of secondary asphaltene precipitation solubility 149 in rich oil [33,34]. Hirschberg et al. indicated [24] that the reversibility of 150 asphaltene precipitation with changing the pressure at high tempera- 151 tures. Most of the investigators claimed the reversibility of asphaltene 152 precipitation at high temperatures while changing the pressure and 153 composition [29,32,35,36]. But it is an irreversible, or, from a kinetic 154 point of view, slow reversible process at low temperatures [16]. Gener- 155 ally, it is believed, the formation of asphaltene particles is a two-step 156 process. At first, asphaltene particles separate from oil phase and then, 157 flocculate and grow into aggregate substances, eventually resulting in 158 asphaltene precipitation [37]. 159

Due to such controversial views about mechanisms of asphaltene 160 precipitation formation, it is not unpredictable to face a huge number 161 of submitted papers about predicting the amount of asphaltene precip- 162 itation. The complex and not yet clearly understood physics of 163 asphaltene causes the assumption that most theoretical investigations 164 regard asphaltene as one single pseudo-component, instead of mixed 165 substances [14,38]. Mohammadi and coworkers [13,39] generally divid- 166 ed the thermodynamic models for estimating formed asphaltene pre- 167 cipitation into five classes: "activity coefficient-based models", "EOS- 168 based models", "colloidal/micellization-models", "scaling laws" and "as- 169 sociation models". One of the most prevalent offered models (activity 170 coefficient-based models) is the Flory-Huggins [40] model that takes 171 advantage of equations of state (EOSs) to calculate the liquid phase 172 mole fraction and solubility. This model was first developed for polymer 173 solutions only, but was modified later by researchers such as 174 Mohammadi, Nikookar and others [13,14,24,41-45] to determine the 175 effects of pressure and composition on the onset conditions and the 176 amounts of the precipitations, and was thus applied to materials other 177 than polymer solutions. In this field, several researchers [46-48] con- 178 ducted various experiments in different conditions on heavy oils of dif- 179 ferent fields around the world and replaced EOSs by correlations found 180

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