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# Dynamics of nanosecond pulsed pump ytterbium-doped double-clad fiber amplifier



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#### ABSTRACT

Pulsed pump is an effective method to suppress the amplified spontaneous emission (ASE) between pulses of high power pulsed fiber lasers. For the pulsed pump, the most important factors need to be determined during amplifier design are the pump power ( $P_p$ ) and pump duration ( $t_p$ ). In this paper, the high power ytterbium-doped double-clad fiber amplifier with pulsed pump is numerically studied. The relationship between pulse energy, efficiency and ASE with pump power and duration is investigated and experimental results are provided. The conclusions are valuable for the design of pulsed pump fiber amplifiers.

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#### 1. Introduction

High-power ytterbium-doped pulsed fiber lasers (YDPFLs) have been intensively studied by researchers [1-4], and are widely used in industry because of their many advantages [5,6]. However, the inter-pulses amplified spontaneous emission (ASE) is a concern for the lasers as it consumes the upper level populations leading to lower efficiency of the final output laser, heats the components in the laser cavity which in turn affects the robustness of the system, causes self-lasing which results in the instability of the laser operation and reduces the maximum achievable pulse energy extracted from the laser cavity, and so on. By adopting pulsed pump instead of continuous-wave (CW) pump to suppress the ASE is a widely-used method suggested by researchers. For example, in 2009, Huang et al, achieved 30 dB gains from an ytterbiumdoped double-clad fiber amplifier (YDFA) through the pulsed pump to suppress the ASE for a 100 ns pulse at 100 Hz pulse repetition rate [7]. In 2014, a fiber laser with 55 mJ pulse energy and 10 ns pulse duration at 10 Hz pulse repetition rate was reported [8]. The laser was made up of seven cascaded amplifiers and pulsed pump with different pump power  $(P_p)$  and pump duration  $(t_p)$  was implemented.

Theoretical modeling and numerical analysis provide the necessary guidance for YDFA design. A number of papers have been reported on the dynamics of the laser pulses amplified by an YDFA with CW pump [9,10]. However, few are available for pulsed pump. In 2013, Wei T. et al, reported the study on the optimal duration of the pulsed pump, the study was focusing on one particular pump power level [11]. For pulsed pump, the most important factors to be identified for the amplifier design are the  $P_p$  and  $t_p$ . Driven by this, in this paper, the laser pulse evolution in a pulsed pumped YDFA is numerically studied by solving the time-dependent rate equations. The dynamics of the ASE, pulse energy and efficiency of the YDFA with pulsed pump at different  $P_p$  and  $t_p$  are investigated. Experimental results are provided.

#### 2. Theoretical model

The configuration of the YDFA is demonstrated in Fig. 1. The 7 mlength gain fiber has a core/cladding diameter of  $30/250 \mu m$ . The 200 ns trapezoidal shape laser pulses with rising and falling edges of 1 ns are used as the seed laser pulses. The optical spectrum bandwidth of the seed laser pulses is 2 nm (full width half modulation (FWHM)). Sixteen ASE channels with  $\Delta \lambda_k$  of 5 nm are considered in the calculation. Two isolators are put at the ends of the amplifier to block the reflection light and pump power is coupled into the amplifier with the backward pump scheme. The other parameters are listed in Table 1 and the simplified rate equations for the YDFA are as follows [10,11], where *z* and *t* 

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Fig. 1. The YDFA with backward pulsed pump scheme (ISO: isolator, PC: pump combiner, LD: laser diode).

#### Table 1

Part of the parameters used in the simulations.

| $\lambda_p$ 915 nm                    | $\lambda_s$ 1064 nm  | $\lambda_1 \ 1020 \ nm$           | $\lambda_K 1100 \text{ nm}$ |
|---------------------------------------|--|-----------------------------------|-----------------------------|
| $\tau 880 \ \mu s$<br>$\Gamma_p 0.01$ | $S_{\alpha RS} = 1.2 \times 10^{-7} \text{ m}^{-2}$<br>$\Gamma = 0.83$ | $\Delta \lambda_s = 2 \text{ nm}$ | $\Delta \lambda_k$ 5 nm     |

represent the coordinate and time respectively.  $N_0$  is the ytterbium dopant concentration.  $N_1$  and  $N_2$  are the ground and upper level population respectively.  $\sigma_a$  and  $\sigma_e$  are the absorption and emission cross-section of the ytterbium-doped double-clad (YDDC) fiber (the values are from Nufern Inc.).  $\lambda_p$ ,  $\lambda_s$  and  $\lambda_k$  represent the central wavelengths of the pump, signal and ASE respectively.  $\tau$  is the life time of the upper level ions.  $\Gamma_p$  and  $\Gamma$  are the filling factors of the pump and laser signal.  $S_{\alpha RS}$  is the Rayleigh scattering factor. A is the fiber core size and  $\alpha$  is the attenuation coefficient of the fiber.  $v_p$  and v are the group velocities of the pump and signal (ASE).  $P_p^{\pm}$ ,  $P^{\pm}(z,t,\lambda_k)$  and  $P^{\pm}(z,t,\lambda_s)$  are the power of the forward and backward pump, ASE and signal.  $P_{pin}$  and  $P_{sin}$  are the power of the pump and signal injected into the amplifier.

$$\frac{dN_{2}(z,t)}{dt} = \frac{\Gamma_{p}\lambda_{p}}{hcA} \left[ \sigma_{a}\left(\lambda_{p}\right) N_{1}\left(z,t\right) - \sigma_{e}\left(\lambda_{p}\right) N_{2}\left(z,t\right) \right] \\
\cdot \left[ P_{p}^{+}\left(z,t\right) + P_{p}^{-}\left(z,t\right) \right] - \frac{N_{2}\left(z,t\right)}{\tau} \\
+ \frac{\Gamma}{hcA} \sum_{k=1}^{K} \lambda_{k} \left[ N_{1}\left(z,t\right) \sigma_{a}\left(\lambda_{k}\right) - N_{2}\left(z,t\right) \sigma_{e}\left(\lambda_{k}\right) \right] \\
\cdot \left[ P^{+}\left(z,t,\lambda_{k}\right) + P^{-}\left(z,t,\lambda_{k}\right) \right]$$
(1)

$$N_{0} = N_{1} + N_{2}$$

$$\pm \frac{\partial P_{p}^{\pm}(z,t)}{\partial z} + \frac{1}{v_{p}} \frac{\partial P_{p}^{\pm}(z,t)}{\partial t}$$

$$= \sum_{p=1}^{n} \left[ \left( \begin{array}{c} z \\ z \end{array} \right) N_{p}(z) \right]$$
(2)

$$= \frac{-1}{p} \left[ b_a(\lambda_p) P_1(z,t) - b_e(\lambda_p) P_2(z,t) \right]$$

$$\times P_p^{\pm}(z,t) - \alpha\left(\lambda_p\right) P_p^{\pm}(z,t)$$

$$\pm \frac{\partial P_p^{\pm}(z,t,\lambda_k)}{\partial z} + \frac{1}{v} \frac{\partial P_p^{\pm}(z,t,\lambda_k)}{\partial t}$$

$$(3)$$

$$= -\Gamma \left[ \sigma_{e} \left( \lambda_{k} \right) N_{2} \left( z, t \right) - \sigma_{a} \left( \lambda \right) N_{1} \left( z, t \right) \right]$$

$$\times P^{\mp} \left( z, t, \lambda_{k} \right) - \alpha \left( \lambda_{k} \right) P^{\pm} \left( z, t, \lambda_{k} \right) + 2\sigma_{e} \left( \lambda_{k} \right) N_{2} \left( z, t \right) \frac{hc^{2}}{\lambda_{k}^{3}} \Delta \lambda_{k}$$

$$+ S\alpha_{RS} \left( \lambda_{k} \right) \times P^{\mp} \left( z, t, \lambda_{k} \right) k = 1, \dots, K, k \neq S$$

$$\frac{\partial P^{\pm} \left( z, t, \lambda_{k} \right)}{\partial P^{\pm} \left( z, t, \lambda_{k} \right)} = 1 \frac{\partial P^{\pm} \left( z, t, \lambda_{k} \right)}{\partial P^{\pm} \left( z, t, \lambda_{k} \right)}$$
(4)

$$\pm \frac{\partial T^{-}(z,t,\lambda_{K})}{\partial z} + \frac{1}{v} \frac{\partial T^{-}(z,t,\lambda_{K})}{\partial t}$$

$$= \Gamma \left[ \sigma_{e} \left( \lambda_{s} \right) N_{2} \left( z, t \right) - \sigma_{a} \left( \lambda_{s} \right) N_{1} \left( z, t \right) \right]$$

$$\times P^{\pm} \left( z, t, \lambda_{s} \right) - \alpha \left( \lambda_{s} \right) P^{\pm} \left( z, t, \lambda_{s} \right)$$

$$+ 2\sigma_{e} \left( \lambda_{s} \right) N_{2} \left( z, t \right) \frac{hc^{2}}{\lambda_{s}^{3}} \Delta \lambda_{s} + S\alpha_{RS} \left( \lambda_{s} \right) \times P^{\mp} \left( z, t, \lambda_{s} \right).$$
(5)

The initial boundary conditions are as follows:

$$\begin{aligned} P_{p}^{+}(0) &= 0, \quad P^{-}\left(L, t, \lambda_{s}\right) = 0, \\ P_{p}^{-}\left(L, t\right) &= P_{pin}\left(t\right), \quad P^{+}\left(0, t, \lambda_{s}\right) = P_{sin}\left(t\right), \\ P^{+}\left(0, t, \lambda_{k}\right) &= 0, \quad P^{-}\left(L, t, \lambda_{k}\right) = 0, \quad k = 1, \dots, K, k \neq s. \end{aligned}$$
(6)

For the simulation, the rate equations are numerically solved in the step of 250 ps. The calculation of the laser pulses is ceased only when the variation of the peak power is less than 0.3% for the successive pulses. The seed laser pulses are kept at 10  $\mu$ J pulse energy and 100 Hz pulse repetition rate. The YDFA absorbs more than 98% pump power and it has a reasonable signal gain of 10 ~ 30 dB. In the following paragraph, the pump duration  $t_p$  corresponding to reaching at the maximum pulse energy and efficiency is referred as  $t_{maxPE}$  and  $t_{maxEff}$ , respectively.

#### 3. Simulation and experimental results

#### 3.1. Amplifier working with different $P_P$ and $t_p$

From the simulation results, the output pulse energy increases as a function of  $t_p$  at different  $P_P$  levels (Fig. 2(a)). However, the maximum achievable pulse energy increased for higher  $P_P$  is insignificant because of the saturation of the stored energy in the YDFA as show in Fig. 2(c). As expected, the  $t_{maxPE}$  is quickly shortened with higher  $P_P$ , and it is 300 µs, 500 µs and 1500 µs for the 30 W, 20 W and 10 W  $P_P$  respectively.

Fig. 2(b) shows the maximum achievable efficiency grows with the increase of  $P_P$ . However, the improvement slows down as the  $P_P$  increases. The  $t_{maxEff}$  is shorter than  $t_{maxPE}$  as after that more pump energy contributes to the ASE.

The stored energy in the YDFA before seed laser injected is shown in Fig. 2(c). Obviously, it grows rapidly with longer  $t_p$  and then saturates. The  $t_p$  for reaching saturation is longer than  $t_{maxPE}$  and  $t_{maxEff}$ . The reason is that the increase in ASE power becomes significant when pump duration is longer than  $t_{maxPE}$ . It results in the change of the  $N_2$  distribution along the gain fiber. This will be further discussed in the following paragraph.

The simulation results of the forward and backward ASE before the seed laser pulses injected into the YDFA are shown in Fig. 3. The ASE power is in a low level when the pump duration is less than the  $t_{maxEff}$ . It grows quickly after that, and eventually gets saturated and reaches a plateau, where the amplifier can be considered as working in CW mode. Obviously, the higher the  $P_P$ , the higher the ASE power. The forward ASE power is higher than the backward one as the backward pump scheme is used.

The  $N_2$  distribution along the gain fiber before the seed laser injecting into the amplifier is shown in Fig. 4(a) with 20 W  $P_p$  and several  $t_p$  from 300 µs to 700 µs in the step of 100 µs. It increases along the fiber and reached its peak at the pump end of the fiber when the  $t_p$  is less than 400 µs. When  $t_p$  increases from 500 µs to 700 µs, the  $N_2$ distribution peak moves toward the opposite end. The reason is that the stronger ASE generated consumes more upper level ions and leads to lower  $N_2$  distribution at the pump end of the fiber.

Figs. 4(b) and (c) shows the pulse energy and efficiency of the simulation and experimental results. The trend of these curves is in consistence. The efficiency and pulse energy peak at 400  $\mu$ s and 500  $\mu$ s respectively. From the experimental results, it confirms the conclusion in the simulation that the  $t_{maxEff}$  is shorter than  $t_{maxEP}$ . The pulse energy and efficiency of the experimental results are much lower than that of the simulation results. This is mainly due to the stimulated Raman scattering (SRS) caused by the high peak power of the laser pulses, and the insert loss of the combiner and isolator in the experiments.

#### 3.2. Amplifier working with same pump energy

From Fig. 2(a), the  $t_{maxEff}$  is shortened and the pulse energy increases with higher  $P_p$ . To further study this, the simulation and experiments with the YDFA working at fixed pump energy of 12 mJ are carried out. The sets of  $P_p$  and  $t_p$  are listed in Table 2.

From Fig. 5(a), although the pump energy is the same, the stored energy in the YDFA continues to increase with shorter  $t_p$ . From Fig. 5(b), it shows that the pulse energy keeps growing rapidly when  $t_p$  is shortened from 4000 µs to 1000 µs. When  $t_p$  is longer than 4000 µs,

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