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Numerical optimization and convective thermal loss analysis of improved solar parabolic trough collector receiver system with one sided thermal insulation



Yogender Pal Chandra^a, Arashdeep Singh^a, Saroj Kumar Mohapatra^a, J.P. Kesari^{b,*}, Lokesh Rana^c

^a Mechanical Engineering Department, Thapar University, Patiala-147004, Punjab, India

^b Department of Mechanical Engineering, Delhi Technological University, Bawana Road-110042, New Delhi, India

^c National Institute of Solar Energy, Ministry of New and Renewable Energy, GOI, Gurgaon 122003, Haryana, India

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ABSTRACT

Two type of receiver systems currently employed in solar parabolic trough collector technology are evacuated annuli receivers and air filled annuli receivers. While former receiver finds its way into hightemperature grid-acquaintance solar parabolic trough collectors, latter are more inclined towards nongrid solar thermal applications like low-temperature process heat. Evacuated receivers utilize vacuum filled annuli to reduce down the convection losses; this makes them substantially expensive - while prizing them as benchmark among receivers. Contrary, air filled annuli based receivers are relatively less expensive but are sub-par in thermal performance relative to evacuated receivers. This work deals with the air filled receiver system and would try to abridge the economy and efficiency between both types of systems using computational fluid dynamics (CFD) based numerical simulation approach. A heat blocking thermal insulation was tailored and fitted in the sun facing receiver annulus which does not receive concentrated radiation of the Sun, and was simulated for the reduction in convective losses and for favourable circumferential temperature distribution (CTD) around the absorber. Consequently, its convective heat losses were investigated for varying wind speeds and mass flow rates of heat transfer fluid (HTF) and were compared with mainstream air filled annuli receivers. Simulation results are compared with experimentation in which wind velocity was in a range of 0.43-4.99 m/s. It has been found that glass envelope temperature decreases with increase in wind velocity which directly insinuates the decrease in convection losses around glass envelope. These comparative implications could be served as a point of reference to develop solar parabolic trough collector for small scale process heat applications in India. © 2017 Elsevier Ltd. All rights reserved.

1. Introduction

Linear concentration technology has made parabolic trough collector vanguard of concentrated solar power (CSP): there is no definitive focusing point, rather a line. Serious development and evolution of this technology, in fact, came into existence when researchers analyzed existing forefront point focusing technology and suddenly stumbled upon a general concept – why, point concentrate the heat when it will be redistributed in line circuitry of the heat transfer fluid. Parabolic trough based concentrated solar thermal power plants, for the most part, consists of parabolic trough solar fields, heat generation system or absorber/receiver system, power block powered with Rankine steam turbine and a

* Corresponding author. E-mail address: kesarijp@gmail.com (J.P. Kesari).

temporary or optional power storage system. Good performance of solar fields or collectors is undeniably indispensable for parabolic trough technology. A decade long of research on parabolic trough technology has been summed up by Fletcher (2001) and Barlev et al. (2011) who clearly adduced the work of Steinmann et al. (2005); Arasu and Sornakumar, 2007; Dudley et al. (1994), Alguacil et al. (2014) and Zhang et al. (2015). This interesting and invaluable research includes - performance and analysis of heat transfer fluids and thermal storage, support structure and reflector development, receiver development, process development for direct steam generation and numerical optimization of thermo-physical factors. In addition, thermo - physical parameters such as solar irradiance, wind velocity, mass flow rate and inlet temperature of heat transfer fluid (HTF) are urgently critical, in order for parabolic trough collector (PTC) to perform efficiently. To illustrate, Fig. 1 describes a PTC receiver with vacuum filled annulus that is being used as a 'nouveau technology' to put down



Nomenclature

Sy	mbols		Greek	
A		area (m ²)	δ	molecular diameter of air in annulus (cm)
C_{μ}	,	specific heat at constant pressure (kJ/kg K)	3	turbulent energy dissipation or emissivity
C _a	ε, C _{3ε}	RNG eq. constants, 1.420, 1.680	η	efficiency
C_{2}	28	constant for turbulent kinetic energy	ho	density (kg/m ³)
с.	m	correlation parameters, 0.26, 0.6	μ	dynamic viscosity (Pa s)
Ď		diameter (m)	μ_t	turbulent eddy viscosity (Pa s)
G	5	turbulent kinetic energy generation owing to buoyancy	σ_k	turbulent Prandtle number for diffusion of k
	-	effect	$\sigma_{arepsilon}$	turbulent Prandtle number for diffusion of ϵ
G	k	turbulent kinetic energy generation owing to mean	Δ	increment value
		velocity gradient	φ	circumferential angle
g		gravitational constant (m/s ²)	∞	condition pertaining to ambient
ha	ı	convective heat transfer coefficient for annular space		
		$(kW/m^2 K)$	Subscript	S
hg	ŗ	convective heat transfer coefficient for glass envelope	а	absorber interaction point
		$(kW/m^2 K)$	a - cond	conduction losses from absorber
k		thermal conductivity (kW/m K)	a - conv	buoyancy induced convective heat transfer from absor-
k_{ii}	n	turbulent intensity (%)		ber to trapped air in annulus
kτ	-	turbulent conductivity (kW/m K)	a,f- conv	heat transfer from absorber to fluid via. convection
k_1		turbulent energy production	a - rad	radiation losses from absorber
ṁ		mass flow rate (kg/s)	avg	average
N	и	Nusselt number	D	hydraulic diameter
р		pressure (N/m^2)	f	heat transfer fluid
Pr	•	Prandtle number	g - conv	convection losses from glass to ambient
0		rate of heat transfer per unit length (W/m)	g ,	condition pertaining to glass envelope
a		heat flux (W/m^2)	g - raa	radiation losses from glass envelope
Re	2	Revnolds number based on hydraulic diameter	1n : :	condition at inlet
Т		temperature (K)	l, j	pertaining to nodes i, j
t		time (s)	0	color incidence
u.	<i>v. w</i>	velocities in x. v. z direction	sol abc	solar radiation transmitted through glass envelop to ab
V	,	velocity (m/s)	301-UDS	sorber
x	v. z	cartesian coordinates	147	wall
,	<i>,,~</i>		vv	wan



Fig. 1. (a) Schematic of vacuum annulus parabolic trough collector, and (b) prevailing heat losses in it.

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