



Enhancement in energy metrics of double slope solar still by incorporating N identical PVT collectors



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ABSTRACT

In this paper, double slope solar still has been analyzed by incorporating N identical partially covered photovoltaic thermal (PVT) collectors under optimized condition to assess the enhancement in energy metrics. Number of collectors, mass flow rate and water depth of N identical partially covered PVT flat plate collector (N-PVT-FPC-DS) have been optimized for climatic condition of New Delhi. Subsequently, annual distillate output, energy, exergy, energy metrics, cogeneration efficiency and cost of distillate output have been computed for the proposed N-PVT-FPC-DS at 0.14 m water depth. Results obtained have been compared with results reported by previous researchers and it has been concluded that the proposed N-PVT-FPC-DS performs better than double slope solar still incorporated with N identical PVT compound parabolic concentrator collectors (N-PVT-CPC-DS) and conventional double slope solar still (CDSSS) on the basis of energy metrics and cost of distillate output. The exergy based energy payback time is lower by 74.66% and 62.62%; energy production factor is higher by 43.30% and 38.14%; life cycle conversion efficiency is higher by 48.57% and 48.57% and cost of distillate output is lower by 35.37% and 4.88% for the proposed N-PVT-FPC-DS than N-PVT-CPC-DS and CDSSS respectively.

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1. Introduction

Solar distillation is the process of getting potable water at the expense of solar energy with the help of device known as solar still. Solar still on proper incorporation with PVT collectors or similar other device is known as active solar distillation system. It can offer a promising option to assuage the contemporary problem of paucity of potable water and energy for far-flung areas as it is very simple in technology which can be maintained by a layman very easily, eco-friendly, more economical. Moreover, it is self sustainable and it can even deliver DC electric power to the society during sunshine hours if required. Solar distillation system is usually categorized as passive and active. The active solar distillation system can further be classified as nocturnal and high temperature distillation. In the case of high temperature active solar distillation system, additional heat can be made available to the basin of solar still through some external source either directly by incorporating flat plate collector (FPC)/Concentrator/evacuated tube collector (ETC) or indirectly by the use of heat exchangers to enhance the rate of vaporization of water with an aim to attain higher yield. A lot of researches by various researchers are available for active solar still.

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The active solar still in forced mode was investigated theoretically for the first time by Rai and Tiwari (1983) and they reported that the daily yield was 24% higher than conventional solar still. At the same time, Zaki et al. (1983) studied the active solar still under natural circulation mode for the first time and reported a maximum enhancement in distillate output of 33% in comparison to conventional solar still. A number of series connected FPC can be coupled to the basin of solar distillation system in a closed loop either directly by discharging hot water to the basin or by providing heat exchanger in the basin. Yadav and Yadav (2004) studied the single slope solar still by incorporating inverted absorber asymmetric line-axis compound parabolic concentrating collector and concluded that the distillate output was increased in comparison to conventional solar still because solar still received solar energy both from top and bottom resulting in increased temperature difference between water surface and glass cover. Badran and Al-Tahaine (2004) investigated solar still having mirrors at interior walls and coupled with FPC experimentally. They reported an increase in yield by 36% as compared to conventional solar still due to increased temperature difference between water surface and inner surface of glass cover. Abdel-Rehim and Lasheen (2007) investigated single slope solar still augmented with solar parabolic trough collector and heat gained by serpentine oil in collector was transferred to water in basin through heat exchanger

Nomenclature

A_b	area of basin (m^2)	K_g	thermal conductivity of glass ($W/m\cdot K$)
A_c	area of flat plate collector under glazing (m^2)	K_i	thermal conductivity of insulation ($W/m\cdot K$)
A_g	area of glass cover (m^2)	K_p	thermal conductivity of absorption plate ($W/m\cdot K$)
A_m	area of PVT (m^2)	L	latent heat (J/kg)
a	clear days (blue sky)	L_c	length of collector under glazing only (m)
b	hazy days (fully)	L_i	thickness of insulation (m)
C_f/C_w	specific heat capacity of water ($J/kg\cdot K$)	L_g	thickness of glass cover (m)
CPC	compound parabolic concentrator	L_m	length of PVT (m)
CDSSS	conventional double slope solar still	L_p	thickness of absorption plate (m)
C_{wp}	production cost of water ($\text{₹}/kg$)	LCCE	life cycle conversion efficiency
C_e	cost of electricity gain ($\text{₹}/kW h$)	\ln	natural logarithm
C_{DSSS}	cost of DSSS (₹)	M	maintenance cost of PVT-FPC active solar distillation system
$C_{PVT-FPC}$	cost of PVT – FPC	M_w	mass of water in basin (kg)
C_{fab}	fabrication cost which includes the cost of piping and labor (₹)	M_{ew}	annual yield from solar distillation system (kg)
c	hazy and cloudy days (partially)	\dot{m}_f	mass flow rate of water (kg/s)
d	cloudy days (fully)	N	number of collectors
DS	double slope PVT-FPC active solar distillation system	n	life of N-PVT-FPC-DS (year)
\dot{E}_x	hourly exergy (W)	n'	number of days
E_{out}	overall annual energy available from N-PVT-FPC-DS ($kW h$)	PVT	photovoltaic thermal
E_x	daily exergy ($kW h$)	PF_1	penalty factor due to the glass covers of module
E_{xm}	monthly exergy ($kW h$)	PF_2	penalty factor due to plate below the module
E_{in}	embodied energy ($kW h$)	PF_3	penalty factor due to the absorption plate for the glazed portion
EPF	energy production factor (fraction)	PF_c	penalty factor due to the glass covers for the glazed portion
EPBT	energy payback time (yr)	P_s	net present cost (₹)
E_e	annual electricity gain ($kW h$)	P_m	annual power generated from photovoltaic module ($kW h$)
FPC	flat plate collector	P_u	annual power utilized by pump ($kW h$)
F'	collector efficiency factor	N-PVT-FPC-DS	double slope photovoltaic thermal flat plate collectors active solar distillation system
$F_{CR,i,n}$	capital recovery factor (fraction)	N-PVT-CPC-DS	double slope photovoltaic thermal compound parabolic concentrator collectors active solar distillation system
$F_{SR,i,n}$	sinking fund factor (fraction)	\dot{Q}_{uN}	the rate of useful heat from N identical partially (25%) covered PVT-FPC connected in series ($kW h$)
$G_{ex,annual}$	annual overall exergy gain ($kW h$)	R	reflectivity
h_i	heat transfer coefficient for space between the glazing and absorption plate ($W/m^2\cdot K$)	r	ratio of daily diffused to daily global irradiation
h'_i	heat transfer coefficient from bottom of PVT to ambient ($W/m^2\cdot K$)	$(SP)_w$	selling price of water (₹)
h_o	heat transfer coefficient from top of PVT to ambient ($W/m^2\cdot K$)	$(SP)_e$	selling price of electricity (₹)
h_{pf}	heat transfer coefficient from blackened plate to fluid ($W/m^2\cdot K$)	S_s	salvage value (₹)
h_{bw}	heat transfer coefficient from basin liner to water ($W/m^2\cdot K$)	T_a	ambient temperature ($^\circ C$)
h_{ba}	heat transfer coefficient from basin liner to ambient ($W/m^2\cdot K$)	T_c	solar cell temperature ($^\circ C$)
h_{rwgE}	radiative heat transfer coefficient from water to inner surface of glass cover on east side ($W/m^2\cdot K$)	T_p	absorption plate temperature ($^\circ C$)
h_{rwgW}	radiative heat transfer coefficient from water to inner surface of glass cover on west side ($W/m^2\cdot K$)	T_{fi}	fluid temperature at collector inlet ($^\circ C$)
h_{cwgE}	convective heat transfer coefficient from water to inner surface of glass cover on east side ($W/m^2\cdot K$)	T_f	temperature of fluid in collector ($^\circ C$)
h_{cwgW}	convective heat transfer coefficient from water to inner surface of glass cover on west side ($W/m^2\cdot K$)	T_{foN}	outlet water temperature at the end of Nth PVT-FPC ($^\circ C$)
h_{ewgE}	evaporative heat transfer coefficient from water to inner surface of glass cover on east side ($W/m^2\cdot K$)	T_s	temperature of sun, $^\circ C$
h_{ewgW}	evaporative heat transfer coefficient from water to inner surface of glass cover on west side ($W/m^2\cdot K$)	T_w	temperature of water in basin, $^\circ C$
h_{1wE}	total heat transfer coefficient between water surface and glass cover on east side	T_{wo}	water temperature at $t = 0$, $^\circ C$
h_{1wW}	total heat transfer coefficient between water surface and glass cover on west side	\bar{T}_{CN}	average solar cell temperature
$I(t)$	radiation falling on collector (W/m^2)	T_{giE}	glass temperature at inner surface on east side, $^\circ C$
$I_{sE}(t)$	solar intensity falling on glass cover on east side (W/m^2)	T_{giW}	glass temperature at inner surface on west side, $^\circ C$
$I_{sW}(t)$	solar intensity falling on glass cover on west side (W/m^2)	ΔT	temperature difference between T_w and T_{giE}/T_{giW}
i	rate of interest (%)	t	time, h
		UAC	uniform end-of-year annual cost (₹)
		U_{tca}	overall heat transfer coefficient from cell to ambient ($W/m^2\cdot K$)
		U_{tpa}	overall heat transfer coefficient from plate to ambient ($W/m^2\cdot K$)
		U_{Lm}	overall heat transfer coefficient from module to ambient ($W/m^2\cdot K$)

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