



XXIV Italian Group of Fracture Conference, 1-3 March 2017, Urbino, Italy

Study of defect formation in Al 7050 alloys

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Abstract

The Al 7050 alloy is an Al-Zn-Mg-Cu-Zr alloy having good mechanical properties. This alloy has been developed in order to overcome stress corrosion cracking problems that characterise 7xxx Al alloys. Despite Al 7050 is widely used for aerospace applications, it can be subjected to crack initiation and propagation during the manufacturing process. In this work cracked Al 7050 components have been analysed in order to identify possible causes of crack formation such as coarse intermetallic phase presence, voids or wrong mechanical machining processes.

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Peer-review under responsibility of the Scientific Committee of IGF Ex-Co.

Keywords: Aluminium alloys, Al 7050, Fracture.

1. Introduction

Over the last decades many efforts have been spent to realise newer aluminium alloys and to improve the performances of the existing ones in order to find, for Al 7XXX alloys, new application fields as said by J.C. Williams et al. (2003). The Al 7XXX mechanical properties are affected by the alloy chemical composition and by the alloy microstructure related to the used production process parameters. Among the different Al alloys we are going to focus on the Al 7050. Aluminium alloy 7050 is an aerospace grade of aluminium characterised by high strength, stress corrosion cracking resistance and toughness as described by M. Dixit et al. (2008). It is particularly suited for heavy plate applications due to its lower quench sensitivity and retention of strength in thicker sections. Al 7050 therefore is the premium choice aerospace aluminium for applications such as fuselage frames, bulkheads and wing skins. Aluminium alloys based on the Al-Zn-Mg composition can be heat treated and age hardened in different

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ways as reported by P. Rometsch et al.(2014): using particular heat treatments, mechanical fracture risks could be reduced drastically. Although aluminium alloys that contain appreciable amounts of soluble alloying elements, primarily copper, magnesium, silicon and zinc, are susceptible to stress corrosion cracking (SCC) as shown by J.Chen et al.(2016), the main characteristics of Al 7050 alloy are high fracture toughness and resistance to SCC. This gives them very useful characteristics, as said above, for aerospace applications. Aim of this work is to analyse Al 7050 defects that could become critical during manufacturing processes. Three are the critical stages: shaping process, heat treatment and mechanical machining processes. During these stages cracks could nucleate and propagate. In this work we examined various types of defects that could be critical for Al 7050 alloy.

2. Experimental.

In this paper we examined an Al 7050 alloy, subjected to shaping and machining processes, having the following nominal composition: Al-2.3Cu-2.3Mg-6.2Zn-0.12Zr, Fe and Si <0.1. In the studied components major cracks were detected after the machining process necessary to obtain the final product. The as-received material was certified as Al 7050 subjected to T7451. This heat treatment, according to the ASTM standard B918, is performed in two steps:

- 1- solution heat treatment and quenching: solution temperature 476 °C, quenching solution maximum temperature 43 °C;
- 2- two step precipitation ageing: first step temperature 121 °C for 3-6 hours, second step temperature 165 °C for 24-30 hours.

The metal in this state of preparation was cut with a diamond cutter to consistent size for observation. In order to perform metallographic examinations on the specimen surfaces they were ground to a mirror-like surface using SiC papers up to 1200 followed by 1 µm alumina and then etched in Keller's reagent. Metallographic structure, crack paths and fracture surfaces were inspected by scanning electron microscope (SEM) and microanalyses were carried out by energy dispersion spectroscopy (EDS). Microstructure observations were also performed by means of an optical microscope.

3. Results

Figs. 1-3 show the optical micrographs of the examined components taken in three metallurgical directions (respectively longitudinal L, short S and transverse T). This is the typical microstructure of a rolled and heat treated component characterised by coarse elongated grains together with bands of fine recrystallized grains. It can be also highlighted that coarse second phases particles, which are always present in aluminium alloys, are aligned along the rolling direction.

From the micrographs it can be easily seen that the grains have a preferential orientation due to rolling operation, necessary to obtain a plate to be machined. It can be noticed a great number of coarse intermetallic phases similar to those reported by D. Dumont et al. (2003) and N.M. Han et al. (2011).

Figs. 4-6 show SEM back scattered micrographs of these components. This confirms what observed with the optical microscope and allows to identify the different kinds of coarse particles that are present in the microstructure. In Fig. 5 a fine precipitation of bright intermetallics can be observed along the grain boundaries. EDS semi quantitative microanalysis has been carried out in order to identify their chemical composition. Figs. 7a-d show the EDS spectra of these intermetallics. Four different intermetallics have been identified..

- A bright globular intermetallic containing Al, Cu and Mg (probably Al₂CuMg)
- A bright polygonal intermetallic often fragmented by the rolling process composed mainly by Al, Cu and Fe (probably Al₇Cu₂Fe)
- A dark intermetallic whose principal elements are Mg and Si (EDS revealed also the presence of oxygen)
- A bright globular phase composed by Cu, Al and Mg (this phase differs from the first identified intermetallic for the very high content of Cu).

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