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# Oxidation and reduction behaviors of a prototypic MgO-PuO<sub>2-x</sub> inert matrix fuel



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#### ABSTRACT

Oxidation and reduction behaviors of prototypic MgO-based inert matrix fuels (IMFs) containing  $PuO_{2-x}$  were experimentally investigated by means of thermogravimetry. The oxidation and reduction kinetics of the MgO- $PuO_{2-x}$  specimen were determined. The oxidation and reduction rates of the MgO- $PuO_{2-x}$  were found to be low compared with those of  $PuO_{2-x}$ . It is note that the changes in O/Pu ratios of  $MgO-PuO_{2-x}$  from stoichiometry were smaller than those of  $PuO_{2-x}$  at high oxygen partial pressure.

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#### 1. Introduction

Inert matrix fuels (IMFs) are a composite of actinide phase and an inert matrix that are being considered as an option for the rapid incineration of actinides in a future fast reactor cycle system and an accelerator driven sub-critical system [1-5]. Magnesium oxide (MgO)-based IMF, which is one of the promising candidates, is the subject of this study. MgO has been selected due to its high manufacturability, chemical and physical stability, high melting temperature, and high thermal conductivity. Americium oxide (AmO<sub>2-x</sub>) and plutonium and americium mixed oxide ((Pu,Am)O<sub>2-x</sub>) are considered as actinide oxide phases for the MgO matrix [1-5]. The development of prototypic MgO-based IMFs containing actinides is now underway [1,2,6-10].

The oxygen-to-metal (O/M) ratio of nuclear oxide fuel, e.g.  $UO_{2\pm x}$ ,  $PuO_{2-x}$ ,  $(U,Pu)O_{2-x}$ , is a very important parameter because it significantly affects various fuel properties, oxygen potentials [11–16], thermophysical properties [17–19] and sintering behaviors [20,21]. Therefore, the O/M ratio of oxide fuels should be accurately evaluated with their changing behaviors, i.e. oxidation and reduction behaviors, as a function of O/M ratio. Although the situation is similar with IMFs, there is little data on MgO-based IMFs, i.e. the composite media of MgO and actinide oxide. In this

study, therefore, the oxidation and reduction behaviors of a prototypic MgO-based IMF containing  $PuO_2$  (hereafter, MgO- $PuO_{2-x}$ ) were experimentally investigated by means of thermogravimetry. Results were compared with those for  $PuO_{2-x}$  specimen which was prepared for reference and discussed from the viewpoint of the effects of the MgO matrix on the oxidation and reduction behaviors of  $PuO_{2-x}$  in MgO- $PuO_{2-x}$ .

#### 2. Experimental

#### 2.1. Specimen preparation

A dense disk-shaped MgO-PuO<sub>2-x</sub> (size of PuO<sub>2-x</sub> phase was below  $\phi$ 10  $\mu$ m) specimen was prepared by a powder metallurgy method. Table 1 shows the fundamental specifications of the raw powders. Raw PuO<sub>2</sub> and MgO (Ube Material Co., Ltd.) powders were weighed to obtain a composition of 15 vol% of PuO<sub>2</sub> and 85 vol% of MgO. These powders were mixed by pestle in an agate mortar in acetone medium for 15 min. The mixed powders were compacted at 200 MPa for 2 min. Sintering was carried out at 1873 K for 3 h in air atmosphere. A sintered PuO<sub>2</sub> disk specimen was also prepared for reference by the same procedure. Table 2 shows the characteristics of PuO<sub>2</sub> and MgO-PuO<sub>2-x</sub> specimens for thermogravimetric analysis (TGA). The sintered density of PuO<sub>2</sub> was calculated to be approximately 81% of theoretical density (%TD), and that of MgO-PuO<sub>2-x</sub> specimen was approximately 90 %TD. Calculations of the

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**Table 1** Fundamental specifications of raw powders.

|   | $PuO_2$                  | MgO <sup>a</sup> |
|---|--------------------------|------------------|
| Metal impurities (ppm)                    | <1065                    | <113             |
| Composition                               | $(Pu_{0.98}U_{0.02})O_2$ | MgO              |
| Particle radius (µm)                      | <0.2                     | 0.1              |
| Specific surface area (m <sup>2</sup> /g) | 7.3                      | 12.5             |

<sup>&</sup>lt;sup>a</sup> Ube Material Industry Co. Ltd., 1000 A.

**Table 2** Characteristics of PuO<sub>2-x</sub> and MgO-PuO<sub>2-x</sub> specimens for TGA.

|  | PuO <sub>2-x</sub> | MgO-PuO <sub>2-x</sub> |
|--|--------------------|------------------------|
| Volume (weight) fraction of PuO <sub>2-x</sub> | _                  | 0.15 (0.37)            |
| Diameter (mm)                                  | 5.2                | 5.1                    |
| Height (mm)                                    | 1.0                | 1.3                    |
| Density (g/cm <sup>3</sup> )                   | 9.42               |                        |
| (80.8 %TD)                                     | 4.34               |                        |
| (89.7 %TD)                                     |                    |                        |

theoretical density assumed that the  $PuO_2$  did not form a solid solution with MgO like as the case of authors' previous studies on the MgO-(Pu,Am) $O_{2-x}$  specimen [9,10], which have shown no experimental evidences of the solid solution formation by an X-ray diffraction analysis.

#### 2.2. Oxidation and reduction kinetics measurement

Oxidation and reduction kinetics of  $PuO_{2-x}$  and  $MgO-PuO_{2-x}$  were measured by means of TGA. TGA was carried out at 1273 K, 1373 K and 1473 K, using a Rigaku model TG-8120 connected to a gas supply system.  $PuO_{2-x}$  and  $MgO-PuO_{2-x}$  specimens were loaded into an alumina capsule and placed in the TGA apparatus. Oxygen partial pressure was adjusted in the range from  $10^{-20}$  to  $10^{-12}$  MPa at a constant temperature. The adjustment was effected by changing the ratio of  $H_2O/H_2$  in slowly flowing mixed gases (265 cm<sup>3</sup>/min). Equilibrium oxygen partial pressure was measured using a stabilized zirconia oxygen sensor. The oxygen sensor was calibrated prior to TGA using the oxidation and reduction of pure chromium metal and a standard gas containing a known amount of oxygen.

The oxygen partial pressure in the atmosphere was changed and it achieved equilibrium rapidly, in less than 10 min. Microgram-order weight changes in the specimen occurring after change in oxygen partial pressure were continuously monitored during several hundred min. Continuous weight changes with time were used for evaluation of oxidation and reduction kinetics.

O/M ratios of MgO-PuO<sub>2-x</sub> were calculated from weight changes relative to stoichiometry, which should be obtained by heattreatment at approximately -300 kJ/mol based on previous results for PuO<sub>2-x</sub> oxygen potential [15]. Because MgO doesn't have non-stoichiometry and is reduced to Mg only at approximately  $10^{-32}$  MPa at 1473 K [22], the changes in O/Mg ratio in MgO would be extremely low and, therefore, negligible in this condition. In addition, since the solid solution formation in the PuO<sub>2</sub>-MgO system was quite limited [23], weight change of the specimen can be regarded as that of the O/Pu ratio change in MgO-PuO<sub>2-x</sub>.

#### 3. Results and discussions

Fig. 1 shows the O/Pu ratio changes in the reduction processes of  $PuO_{2-x}$  and  $MgO-PuO_{2-x}$  at 1373 K from stoichiometry to the O/Pu ratio of 1.991. Whereas the reduction of  $PuO_{2-x}$  was completed in approximately 200 min, that of  $PuO_{2-x}$  in  $MgO-PuO_{2-x}$  was

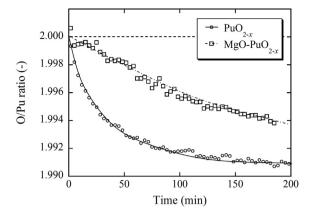


Fig. 1. The O/Pu ratio changes in the reduction process of  $PuO_{2-x}$  and  $MgO-PuO_{2-x}$  at 1373 K.

continuing at 200 min. The reduction rate of  $PuO_{2-x}$  in  $MgO-PuO_{2-x}$  was lower than that of  $PuO_{2-x}$ . Fig. 2 shows the O/Pu ratio changes in the oxidation process of  $PuO_{2-x}$  and  $MgO-PuO_{2-x}$  at 1473 K from O/Pu of 1.975 to the stoichiometry. The oxidation rates of both  $PuO_{2-x}$  and  $PuO_{2-x}$  in  $MgO-PuO_{2-x}$  were higher than their respective reduction rates at the same temperature. Whereas the oxidation of  $PuO_{2-x}$  was completed in approximately 20 min, completion of  $PuO_{2-x}$  oxidation in  $MgO-PuO_{2-x}$  required approximately 120 min. The oxidation rate of  $PuO_{2-x}$  in  $MgO-PuO_{2-x}$  was lower than that of  $PuO_{2-x}$ .

These lower oxidation and reduction rates of MgO-PuO<sub>2-x</sub> can be caused by the effects of MgO matrix. The mechanisms of oxidation and reduction of actinide oxides such as  $UO_{2+x}$  [24,25],  $PuO_{2-x}$  [26] and  $(U_1Pu)O_{2-x}$  [27] have been investigated, and the mechanisms of O/M ratio changes in  $(U,Pu)O_{2-x}$  in the oxidation and reduction processes are found to be distinctly different [27]. The oxidation and reduction processes would be dominated, respectively, by a zero-order reaction such as one on the surface and oxygen chemical diffusion according to [27]. Since the crystal structure and the oxidation and reduction species are the same in both PuO<sub>2-x</sub> and  $(U,Pu)O_{2-x}$ , the mechanisms of O/Pu ratio changes in  $PuO_{2-x}$  should be the same as those in (U,Pu)O<sub>2-x</sub> [27]. Fig. 3 shows the crosssectional image of a prototypic MgO-PuO<sub>2-x</sub> specimen with higher PuO<sub>2-x</sub> content (24 vol%) than the present specimen (15 vol%) prepared by the same procedure. It is seen that the  $PuO_{2-x}$  phase is isolated, namely  $PuO_{2-x}$  phase is surrounded by the MgO phase. The present specimen should have the same isolated PuO2-x phase

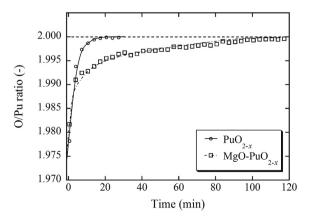


Fig. 2. The O/Pu ratio changes in the oxidation process of  $PuO_{2-x}$  and  $MgO-PuO_{2-x}$  at 1473 K.

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