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# Research paper Influence of supercritical CO<sub>2</sub> on bentonite properties

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## ABSTRACT

Wet bentonite was used to simulate a caprock for geologic  $CO_2$  sequestration. Its properties were characterized after reacting with supercritical (SC)  $CO_2$  alone and in the presence of salt solutions. High-pressure reaction tests were conducted to investigate the interaction of SC  $CO_2$ , bentonite, and water. Wet bentonite mixed with 1 N NaCl solution and then reacted with SC  $CO_2$  resulted in noticeable changes in volume and bentonite mineral components compared with unreacted bentonite, due to SC  $CO_2$  induced dehydration. Plagioclase, K-feldspar, montmorillonite, and pyrite were dissolved but Ca-bearing minerals, i.e., calcite, dolomite, and gypsum, and halite were precipitated. In contrast, wet bentonite mixed with the salt solution reacted with SC  $CO_2$  in the presence of the salt solution resulted in less distinct changes in mineral components, likely due to the dissolution of SC  $CO_2$  in the salt solution. The fewer changes in mineral components in the bentonite reacted with SC  $CO_2$  in the salt solution. These results suggest implicitly that caprock in the immediate vicinity of an injection well may significantly deteriorate due to the interaction between caprock and dry SC  $CO_2$ , and caprock far from the injection well may deteriorate less because the SC  $CO_2$  may react in the presence of large quantities of water.

#### 1. Introduction

Geologic  $CO_2$  sequestration (GCS) is an effective option for reducing  $CO_2$  in the atmosphere. Among various reservoir types for storing  $CO_2$ , deep saline formations have the largest  $CO_2$  storage capacity (Metz et al., 2005). For GCS,  $CO_2$  is injected into a saline aquifer (i.e., permeable rock) with an impermeable caprock (e.g., shale) serving as a seal for permanently storing  $CO_2$ . During  $CO_2$  storage,  $CO_2$  can be dissolved and mineralized into stable form (e.g., carbonate minerals) within several thousand years (Lindeberg and Bergmo, 2003; Metz et al., 2005).

Natural hydrocarbon reservoirs are commonly sealed with caprocks having very low permeability, such as shales and evaporates. These rocks are considered potential caprocks for geological storage of sequestered CO<sub>2</sub>. Shales are generally composed of fine-grained quartz, feldspar, carbonates, and clay minerals (e.g., illite, kaolinite, chlorite, and smectite) (Gueguen and Palciauskas, 1994). The mechanical and transport properties and sealing capacity of shales can be affected by the content of high swelling clays (Mitchell and Soga, 2005; Kaya and Fang, 2005; Espinoza and Santamarina, 2012).

As liquid  $CO_2$  is injected into deep saline formations with overlying caprock, it becomes supercritical (SC)  $CO_2$  in the reservoir. The SC  $CO_2$  exhibits intermediate behavior between liquid and gas, and has a high

density, close to the liquid state, and lower viscosity, similar to the gas state (Lozowski, 2010). The interactions between SC CO<sub>2</sub>, water, and caprock in the CO<sub>2</sub> storage area can potentially occur as three reaction systems: a SC CO<sub>2</sub>/caprock reaction system in the immediate vicinity of the injection well; SC CO<sub>2</sub>/water/caprock reaction system in the aquifer around the CO<sub>2</sub> injection well, where dissolved CO<sub>2</sub> can exist; and water/caprock reaction system far away from the CO<sub>2</sub> injection well.

The interactions between SC CO<sub>2</sub> and caprock, which are characterized by slow reaction rates, can affect the properties of the aluminosilicate minerals contained in the caprock. The interactions between SC CO<sub>2</sub> and potential caprock clay have been primarily studied using numerical modeling because of their very slow reaction rates and difficulties in experimentally simulating a deep geological environment (Botan et al., 2010; Romanov et al., 2010; Yang and Yang, 2010; Cygan et al., 2012; Rother et al., 2012; Krishnan et al., 2015; Leng and Rao, 2016). For example, Botan et al. (2010) reported that the CO<sub>2</sub> interlayer in Na-montmorillonite inhibits the diffusion of exchangeable cations. In addition, Yang and Yang (2010) conducted Gibbs Ensemble Monte Carlo simulations to investigate the swelling behavior and interlayer structure of Na-montmorillonite in SC CO<sub>2</sub> fluid. They showed that the interlayer spacing of Na-montmorillonite in the presence of SC CO<sub>2</sub> was larger than that of Na-montmorillonite in the absence of SC CO<sub>2</sub>.

Many experimental studies have been conducted to investigate the

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interactions between SC CO2 and potential caprock clay (Naveau et al., 2011; Shao et al., 2011; Espinoza and Santamarina, 2012; Giesting et al., 2012; Rother et al., 2012; Jong et al., 2014; Loring et al., 2014). These studies have suggested that the shrinkage or expansion of montmorillonite depends on the initial hydration state and relative humidity of SC CO<sub>2</sub>. The types of cations in the montmorillonite interlayer also affect their swelling or shrinkage behavior. For example, Shao et al. (2011) conducted experimental tests to investigate the effect of salinity and water availability on the interactions between SC CO<sub>2</sub> and phlogopite, which is considered a potential clay mineral in caprock at GCS sites. Two reaction systems, SC CO<sub>2</sub>/H<sub>2</sub>O(liq)/phlogopite and SC CO<sub>2</sub>/  $H_2O(g)$  /phlogopite, were evaluated in their study. They suggested that a thin water film adsorbed on the phlogopite surface formed dissolution pits and secondary mineral surface coatings that could change the caprock properties. In addition, Espinoza and Santamarina (2012) evaluated porosity changes and crack formation in Ca-montmorillonite in contact with 2 M NaCl solution and SC CO2. They reported that the porosity of Ca-montmorillonite decreased more in SC CO2 than in 2 M NaCl solution. Cracks formed in the Ca-montmorillonite in contact with SC CO<sub>2</sub> for 73.5 h due to changes in electrical and capillary forces in the Ca-montmorillonite particles caused by the SC CO<sub>2</sub>.

However, experiments investigating the dehydration and shrinkage of clay materials in contact with SC CO<sub>2</sub> at various conditions (e.g., temperature, pressure, and water chemistry) have been rarely conducted. The objective of this study was to investigate the characteristics of bentonite when directly reacted with dry SC CO<sub>2</sub> and with SC CO<sub>2</sub> in the presence of salt solutions. Bentonite was used to simulate a caprock because bentonite is impermeable and primarily consists of clay minerals. Kinetic tests for SC CO<sub>2</sub>, bentonite, and water interactions were conducted in a stainless steel autoclave reactor with two reaction systems, SC CO<sub>2</sub> and bentonite and SC CO<sub>2</sub>, bentonite, and salt solutions, at 50 °C and 12 MPa to mimic the GCS environment. 1 N NaCl, 1 N CaCl<sub>2</sub>, and 1 N MgCl<sub>2</sub> solutions and seawater were used to evaluate the effect of salts on bentonite properties in the presence of SC CO<sub>2</sub>.

## 2. Materials and methods

#### 2.1. Bentonite

The bentonite used in this study was obtained from a Geosynthetic Clay liner (GCL), which is sold commercially under the trade name Bentofix<sup>®</sup>. The mineralogy of the bentonite was analyzed using X-ray diffractometer (XRD) methods at Mineralogy-Inc., USA. The unreacted bentonite contained 74% montmorillonite, 12% plagioclase feldspar, 6% quartz, 5% K-feldspar, 1% cristobalite, and traces of halite and pyrite. The specific gravity  $(G_s)$  of the bentonite was 2.7. The chemical properties of the experimental seawater are shown in Table 1.

#### 2.2. Vacuum-drying tests

The wet bentonite samples were prepared by mixing bentonite and 1 N NaCl, 1 N CaCl<sub>2</sub>, and 1 N MgCl<sub>2</sub> solutions in a 2:1 weight ratio, and then placed in a stainless steel cell. The cell was cylindrical shape, with a 27.2 mm outer diameter, 23.2 mm inner diameter, 15 mm height, and 2 mm thickness. Fig. 1 shows a schematic of the stainless steel cell with the wet bentonite specimen. Filters, with a pore size of  $0.45 \,\mu m$  from ADVENTEC®, were placed on the top and bottom of the wet bentonite

Table 1 d in this

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Chemistry	of seawater	used	in	this	study.

Material	Concentrat		pН			
	Na	K	Ca	Mg	Si	
Seawater	8719.0	291.9	323.2	983.0	0.3	8.0

Reaction of supercritical CO2 with bentonite without water



## Reaction of supercritical CO2 with bentonite in the presence of water

Fig. 1. Schematic of the experimental stainless steel container containing the bentonite mixture.

specimen in the stainless steel cell. Therefore, SC CO2 and water could penetrate into the bentonite, and the filter prevented the dispersion of bentonite particles. Before placing samples in the stainless steel cell, the mass of each stainless steel cell was measured to determine the subsequent changes in bentonite mass.

The cells containing the wet bentonite samples were placed in a vacuum desiccator. During testing, the diameter and height of the samples were measured using a vernier caliper at designated times (1, 3, 4, and 7 d). The volume and porosity of the bentonite samples were calculated using phase equations (Fredlund and Rahardjo, 1993). Reacted bentonite samples obtained from the vacuum drying tests were dried in an oven at 100 °C for 12 h. The oven dried bentonite samples were transferred right away from the oven to a 50 mL vial in the atmosphere condition. The 50 mL vial, which had the oven dried bentonite, was sealed and stored then in a vacuum desiccator for material characterization. All tests were conducted twice for replication under the same conditions.

## 2.3. SC CO<sub>2</sub> drying tests

A high-pressure environmental chamber (HPEC, 750 mL, Phosentech, Inc) was used to react the dry SC CO<sub>2</sub> with bentonite and investigate potential interactions in an aquifer saturated with CO<sub>2</sub> in deep geological CO<sub>2</sub> storage sites. Fig. 2 shows a schematic of the HPEC system. The bentonite specimen mixed with 1 N NaCl solution was placed in a stainless steel cell. The container with the wet bentonite specimen was placed in the HPECs for drying using SC CO<sub>2</sub> (i.e., SC CO<sub>2</sub> drying). The CO<sub>2</sub> was pressurized to 12 MPa using a syringe pump and introduced into the HPECs, which were controlled at 50 °C, right after the wet bentonite specimen was placed in the HPECs. The specific temperature and pressure were chosen to investigate interactions between SC CO2 and caprock appropriate for geological conditions (Suto et al., 2007).

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