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# Fast real-time three-dimensional wind estimation for fixed-wing aircraft

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## ABSTRACT

This paper proposes a fast real-time estimation algorithm which is inspired by the philosophy of the generalized model predictive static programming and solves the three-dimensional wind estimation problem in an optimal control manner. The wind estimation problem is transformed into a static optimization problem featuring a highly efficient solving framework. The proposed algorithm estimates the three-dimensional wind components without considering any hypothesis on the structure of the wind, and without relying on airspeed measurements either. The measurement noise and the model uncertainties are applied. Simulations demonstrate the rapidity and accuracy of the proposed method.

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## 1. Introduction

The wind is a critical risk factor for the inflight safety, especially during the take-off and landing phases [1]. This paper was motivated by attempts to fast indicate the wind condition on-board to enhance the pilots' situational awareness in some emergency cases. Through the investigation and analysis of the reality and some accidents, we summarize three important factors that must be considered for an adequate wind estimation algorithm for emergency cases.

1. The estimation algorithm must be fast. The fastness is embodied in two aspects. The algorithm must be computationally efficient and it must be able to indicate the wind variation in a short time. Firstly, a successful implementation of the online estimation method is subject to the limited computing power on-board [2]. A traditional numerical method may not be efficient enough to be run onboard. Hence, the estimation algorithm must employ an advanced solution, preferably an explicit closed-form solution. Secondly, there is plenty of evidence to suggest that the quick changing wind structure played a hazardous role in some accidents. The Air France Airbus A340-313 crashed because of a sudden wind velocity variation [3]. If the estimation method produces estimates with

some time delay, it offers little help to the crew's judgment and behavior during emergency cases [4].

2. The wind estimation must be three-dimensional (3-D) and the algorithm must consider unknown wind structures. Firstly, in most passenger airplanes mainly the horizontal wind situation is displayed in strength and direction. However, the low-altitude vertical wind shear, one of the most dangerous atmospheric activities for civil aviation was considered as a major contributory factor in some severe accidents [5]. In March 2009, a McDonnell Douglas MD-11F cargo flight had a severe accident due to the vertical gusty wind [6]. The Boeing 737-236A of Bhoja crashed on approach in the extreme vertical wind shear condition [7]. Secondly, the unknown rapidly changing wind was often one of the major contributing factors in some tragic accidents. In June 2012, the severe wind disturbance was so strong that a Boeing 767 of All Nippon Airways seriously damaged [8]. Moreover, in modern manned flight, the constant wind usually poses minor impact on operation. Therefore, for emergency cases, the predefined wind structure should not be considered as an assumption that the algorithm is based on.
3. The algorithm may not rely on the airflow measurements. We suppose that in some extreme cases, the airspeed sensor failure can happen. In June 2009, the crash of the Airbus A332 of Air France may serve as an example [9]. We intend to use only non-airflow measurements, which can be more feasible and reliable.

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1 Wind estimation algorithms were broadly addressed in the liter-  
 2 ature. Conventionally, the wind models were subject to several  
 3 assumptions while the estimation algorithm was being developed,  
 4 e.g. the steady wind model. Petrich et al. estimated the quasi-  
 5 constant wind using Kalman filters [10], as they were interested  
 6 in estimating the steady state components of the wind instead of  
 7 gusts for emergency cases. The constant wind with random gusts  
 8 was estimated by Pachter et al. using an unscented Kalman filter  
 9 (UKF) [11]. It is reasonable to assume that the Micro Air Vehicles  
 10 (MAV) fly in a constant wind field during the short flight. However,  
 11 our efforts are made towards the gusty wind field.

12 Some of the existing approaches consider two-dimensional  
 13 (2-D) wind models. Based on the UKF, Palanhandalam-Madapusi  
 14 provided a 2-D wind field estimation scheme [12]. The effect of the  
 15 unknown wind disturbance to the MAV navigation concerned them  
 16 in the defined scenarios for planer flight. Assuming that the wind  
 17 existed in the horizontal plane, Kumon et al. proposed a wind es-  
 18 timation method using an unmanned air vehicle with delta wing  
 19 [13]. From the case reviews, we evidenced accidents caused by  
 20 vertical wind shear, so it stands to reason to incorporate the addi-  
 21 tional vertical components of wind.

22 The airflow measurements are widely required in prior wind  
 23 estimation methods (e.g. [10–12,14] and [15]). However, required  
 24 by our mission statement, these approaches are not available for  
 25 our problem without the presence of the airflow measurements.

26 Kalman Filter and its extensions are broadly employed by re-  
 27 searchers for wind estimation (e.g. [10–12,14] and [16]). However,  
 28 when we carefully studied the presented results, some potential  
 29 drawbacks including the converging speed, the higher order correla-  
 30 tion and the additional tuning effort concerned us for practical  
 31 reasons. For example, the changes of the wind speed is modeled  
 32 by using the first-order Gauss–Markov process which is frequently  
 33 utilized for estimating some slowly varying signals [16], which is  
 34 in contrast to our motivation to fast indicate the quickly changing  
 35 wind variations, such as the gusty wind and wind shear. An uncon-  
 36 ventional algorithm overcoming all the aforementioned drawbacks  
 37 is therefore developed and presented.

38 This paper developed a 3-D wind estimation algorithm fea-  
 39 turing high computational efficiency and fast indication using the  
 40 non-airflow measurements. The generalized model predictive static  
 41 programming (G-MPSP) is a computationally efficient method de-  
 42 veloped for solving finite-horizon nonlinear optimal control prob-  
 43 lems [17]. The proposed real-time wind estimation method is in-  
 44 spired by the philosophy of the G-MPSP – the terminal error of  
 45 a finite time horizon between the predicted and actual outputs  
 46 can be minimized by updating control variables using an explicit  
 47 closed-form solution. The overall idea of the proposed algorithm  
 48 is that the wind components are considered as “virtual” inputs to  
 49 the model, and with the measured information during a previous  
 50 finite horizon, the predicted kinematic velocity states with the ve-  
 51 locity expressed as absolute value and direction with respect to  
 52 the ground are calculated. Then, based on the error between the  
 53 predicted and the measured states, the inputs, i.e. the wind vector  
 54 can be updated using the customized G-MPSP so that the terminal  
 55 errors are eliminated.

56 Four key points are addressed in the proposed algorithm.  
 57 Firstly, the main achievement of the paper is a new, non-standard  
 58 optimization method for wind estimation which does not involve  
 59 computationally intensive numerical procedures. This is the reason  
 60 why the scheme is not only computationally efficient but also  
 61 can be run onboard in real-time. We see this proposed scheme  
 62 (which is in contrast to standard numerical optimization proce-  
 63 dures) as a significant contribution, particularly for its potential  
 64 to be used in onboard applications. Secondly, as a supplement to  
 65 the main achievement, any observed terminal error will immedi-  
 66 ately lead to the indication of the wind variation. The situational

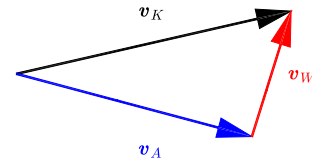


Fig. 1. Velocity triangle.

67 awareness in the emergency cases is only valid when the response  
 68 is fast enough. The proposed approach does not inherently feature  
 69 the low-pass characteristic, which is considered to be an important  
 70 aspect of the contribution to the proposed “fastness”. Thirdly, the  
 71 algorithm is not developed for any specific structure of the wind  
 72 model, as the non-constant wind variations, especially the vertical  
 73 wind changes, are the inevitable challenge to the inflight safety. As  
 74 an important feature, the 3-D non-constant wind components are  
 75 taken into consideration in the algorithm. Finally, only non-airflow  
 76 measurements are utilized by the estimation method. Therefore,  
 77 the proposed wind estimation algorithm fulfills the needs and con-  
 78 tributes to the prior art of the wind estimation.

79 This paper is presented as follows. The necessary mathematical  
 80 details of the nonlinear aircraft model using the 3-D wind vector  
 81 as the virtual input are covered in section 2. In section 3, the wind  
 82 estimation algorithm is introduced. The simulation results are pre-  
 83 sented in section 4. Finally, conclusions are drawn in section 5.

## 2. Aircraft model

84 For the proposed wind estimation algorithm, the 3-D wind  
 85 components are considered as “virtual” inputs to the model and  
 86 the expected response in translation is to be calculated with the  
 87 inputs and the measured variables.

88 This section details the 6 degrees of freedom (6-DoF) non-linear  
 89 model of a fixed-wing aircraft in the presence of a 3-D wind con-  
 90 dition. The definition of basic rotation matrices is given in the Ap-  
 91 pendix, while in this section, the subscripts denote the frames, in  
 92 which the components are notated. Vectors are associated with the  
 93 center of gravity. The inertial frame is earth-fixed with axes paral-  
 94 lel to the north east down (NED) frame  $O$ . The model is based on  
 95 the models presented in Refs. [18,19]. The overall idea of this sec-  
 96 tion is that we calculate the air data, i.e. the aerodynamic velocity,  
 97 angle of attack, angle of sideslip and aerodynamic bank angle us-  
 98 ing the information from non-airflow measurements and the wind  
 99 components provided by the algorithm to give the state prediction  
 100 in translation.

101 The 3-D wind vector  $\mathbf{v}_W$  in Fig. 1 is given in the  $O$ -Frame as

$$102 (\mathbf{v}_W)_O = \begin{pmatrix} u_W \\ v_W \\ w_W \end{pmatrix}_O. \quad (1)$$

103 The wind information in the system is provided by the wind  
 104 estimation algorithm.

105 Via the velocity triangle approach, the relation between the  
 106 aerodynamic velocity  $\mathbf{v}_A$ , the wind velocity  $\mathbf{v}_W$  and the kinematic  
 107 velocity  $\mathbf{v}_K$  is obtained as follows,

$$108 (\mathbf{v}_A)_O = (\mathbf{v}_K)_O - (\mathbf{v}_W)_O. \quad (2)$$

109 Furthermore, the aerodynamic velocity can be described with  
 110 3-D components in the  $O$ -frame as,

$$111 (\mathbf{v}_A)_O = \begin{pmatrix} u_A \\ v_A \\ w_A \end{pmatrix}_O = \begin{pmatrix} V_A \cos \chi_A \cos \gamma_A \\ V_A \sin \chi_A \cos \gamma_A \\ -V_A \sin \gamma_A \end{pmatrix}_O \quad (3)$$

112 where  $\chi_A$ ,  $\gamma_A$  and  $V_A$  are the aerodynamic flight-path course an-  
 113 gle, the aerodynamic flight-path climb angle and the aerodynamic  
 114 speed, respectively, which can be obtained as follows,

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