



A study on prediction of ship maneuvering in regular waves



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ABSTRACT

A simulation method is developed for predicting ship maneuvering in regular waves. Based on a two-time scale model, the total ship motion is divided into the low frequency maneuvering motion and the high frequency wave-induced motion. The maneuvering analysis is based on a MMG model which takes the mean second-order wave loads into account. In order to evaluate the second-order wave loads, a velocity potential is introduced and decomposed into a basic part and a perturbation part, which are related to the maneuvering motion and the wave-induced motion, respectively. The basic part is evaluated based on the double-body model with a trailing vortex sheet, while the perturbation part is solved via a time domain Rankine panel method. The effects of maneuvering motion on the wave forces are considered through the m-terms as well as the leading-order terms kept in the boundary conditions on the free surface. By using the proposed method, turning and zig-zag maneuvers of the S-175 container ship in regular waves are simulated. The predicted turning trajectories and 10°/10° and 20°/20° zig-zag maneuvers are compared with the experimental data, which show fairly good agreements. The drift forces and moment on the ship turning in waves are also discussed.

1. Introduction

Prediction of ship maneuverability is typically carried out under calm water condition. This provides valuable information at the ship design stage. However, an actual seagoing ship usually maneuvers in the presence of waves. From the viewpoint of ship navigation safety, it is meaningful to understand the maneuvering behavior of a ship in waves. According to the report of ITTC Maneuvering Committee (2011) and the literature review given by Tello Ruiz et al. (2012), the existing methods for investigating ship maneuvering in waves can be generally classified as experimental methods, simulation methods based on two-time scale models, simulation methods based on hybrid approach, and simulation methods using CFD.

Experiment methods are supposed to be the most reliable method to investigate ship maneuvering in waves. Several experimental investigations have been published. For example, Ueno et al. (2003) carried out turning, zig-zag and stopping tests in regular waves using a VLCC model, and discussed the effects of wave length and encounter angle to waves as well as the effect of loading condition on maneuvering motion based on the experimental data. Lee et al. (2009) investigated the effects of the wave amplitude and wave length on the maneuverability of a ship, with tests on a KVLCC model. The results showed that second-order wave force has a dominant influence on the trajectory for

turning and zig-zag maneuvers. Yasukawa (2006, 2008) conducted turning tests as well as zig-zag and stopping maneuvers with the SR108 ship model, and compared the model test results with their numerical results.

CFD methods in principle provide an adequate description of all physics. However, this approach is still considered as a subject of the state-of-the-art research rather than application in engineering practice. On one hand, these methods require large computational resources and long CPU time. On the other hand, according to Skejic (2013), a lot of technical difficulties concerning the analysis of ship maneuvering in waves are still unsolved, such as the adequacy of the selected turbulence models, the adequacy of the propeller and rudder models under large angle of attack, the appearance of the crossflow shed vortices and so forth.

Compared with CFD methods, the hybrid methods and the two-time scale methods are much more widely applied in numerical simulation of ship maneuvering in waves. Both of these two methods are based on the potential flow theory but they are different in specific treatments:

The hybrid approach integrates maneuvering motion and wave-induced motion into a generic set of rigid body motion equations to describe the ship maneuvering in waves. Several works falling into this category can be found in the literature, for instance, Bailey et al.

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Nomenclature

A	Amplitude of the incident wave	v'	Non-dimensional transverse speed
a_H	Rudder force increase factor	w_{P0}	Wake fraction in straight moving
C_f	Frictional resistance coefficient	w_P	Wake fraction
C_r	Residuary resistance coefficient	\vec{W}	Velocity vector due to the low frequency motion
$C_{Rr}, C_{Rrrr}, C_{Rrrv}$	Experimental constants for expressing the inflow velocity to rudder	x_G	x-coordinate of the center of gravity
$[C_{ij}]$	Matrix of hydrostatic restoring coefficients	x'_P	Non-dimensional longitudinal coordinate of propeller
D_p	Propeller diameter	x_R	Longitudinal coordinate of the rudder
F_i	High frequency hydrodynamic components	x_H	Longitudinal coordinate of acting point of the additional lateral force induced by steering
$\vec{F}^{(2)}$	Generalized second-order wave force vector	X_H, Y_H, N_H	Low frequency hydrodynamic surge force, lateral force, yaw moment acting on ship hull except added mass components
F_N	Normal rudder force	X_P	Surge force due to propeller
G	Rankine source	X_R, Y_R, N_R	Surge force, lateral force, yaw moment by rudder
I_{zz}	Moment of inertia about z axis	X_W, Y_W, N_W	Wave drift forces and moment
J_p	Propeller advance ratio	α_R	Relative inflow angle to rudder
J_{zz}	Added moment of inertia about z axis	β_P	Geometrical inflow angle to the propeller
k_f	Form factor	χ	Incident angle of wave defined in the global frame
k	Wave number of the incident wave	δ	Rudder angle
K_T	Thrust coefficient	$\varepsilon, \kappa, \tau, \gamma$	Coefficients representing the interaction among the hull, propeller and rudder
L	Ship length	$\phi(\vec{x}, t)$	Perturbation potential
m	Ship mass	$\Phi(\vec{x}, t)$	Basic potential
m_x, m_y	Added masses in x-axis direction and y-axis direction, respectively	η	Wave elevation
m_i	m-terms	λ	Wave length
$[M_{ij}]$	Inertial matrix for the hull	$\varphi_I(\vec{x}, t)$	Incident wave potential
n	Propeller revolution	$\varphi(\vec{x}, t)$	Perturbation potential except incident wave potential
$\vec{n}^{(0)}, \vec{n}^{(1)}, \vec{n}^{(2)}$	Zero-, first- and second-order components of the normal vector on the hull surface, respectively	$\varphi_I(\vec{x}, t)$	Incident wave potential
n_i	Component of the generalized normal vector	Λ	Rudder aspect ratio
N_i	Ratio of τ_L to τ_H	ρ	Water density
$o - xyz$	Reference frame with the origin at midship	τ_L	Time step for the maneuvering computation
$O - XYZ$	Global frame fixed in space	τ_H	Time step for the seakeeping computation
$p^{(1)}$	First-order hydrodynamic pressure	ν	Damping strength of the numerical damping beach
r	Yaw rate of the low frequency motion	ω	Frequency of the incident wave
r'	Non-dimensional yaw rate of the low frequency motion	ω_e	'Local' encounter frequency during maneuvering process
$R(u)$	Ship resistance	$\vec{\xi}_T$	Translational displacements due to high frequency motion
S	Wetted hull surface	$\vec{\xi}_R$	Rotational displacements due to high frequency motion
\bar{S}_B	Mean wetted hull surface	ψ	Ship heading angle
t	Time	$\Psi(\vec{x}, t)$	Total velocity potential
t_p	Thrust deduction fraction	$\zeta(x, y, t)$	Wave elevation except incident wave elevation $\zeta_I(x, y, t)$
t_R	Steering thrust deduction factor	$\zeta_I(x, y, t)$	Incident wave elevation
u	Forward speed of the low frequency motion	ξ_z	Vertical displacement of point (x, y) due to high frequency motion
U_R	Relative inflow velocity to rudder		
v	Transverse speed of the low frequency motion		

(1997), Fang et al. (2005), Sutulo and Guedes Soares (2006), and Lin et al. (2006). A defect common to all these works is that none of them incorporated the effects of second-order wave forces. The omission of the steady components of the second-order wave forces will heavily decrease the accuracy of the maneuvering predictions. Recently, Subramanian and Beck (2015) developed a body-exact strip theory based model to simulate maneuvering of a ship in a seaway. In their methodology, the second-order wave effects are considered approximately via the square of the velocity potential's gradient.

Different from the hybrid approach, the two-time scale methods separate the total ship motion into two parts: the one for high frequency wave-induced motion and the other for the low frequency maneuvering motion, based on the fact that the wave-induced motions are generally much faster than the maneuvering motion. The motion separation brings in a favorable merit that the second-order wave forces can be evaluated in a more accurate manner. Within the framework of the two-time scale model, Skejic and Faltinsen (2008) carried out a unified seakeeping and maneuvering analysis of ships in

regular waves and compared the wave drift forces obtained by using four different approaches based on strip theory. Yasukawa and Nakayama (2009) conducted the 6-DOF motion simulations of a turning ship in regular waves. The high-frequency wave forces in their study were estimated based on the strip theory, while the wave drift forces were evaluated by Maruo's method. It should be noted that the seakeeping analysis in these two works was carried out based on the quasi-steady assumption, which means the memory effects due to the ship motion were not considered. Seo and Kim (2011) conducted the numerical analysis of the coupled maneuvering and seakeeping problem. In their study, two different time scales were used in solving the maneuvering and seakeeping problems, respectively; while the wave forces were solved directly in time domain by a 3D Rankine panel method.

In this paper, a numerical model for investigating ship maneuvering in waves is developed. The simulation method is based on the procedure suggested by Seo and Kim (2011), i.e. the maneuvering motion is predicted using MMG model, whereas the wave effects are

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