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Power balance control of micro gas turbine generation system based on supercapacitor energy storage



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ABSTRACT

In view of the impact load problems in the traditional micro gas turbine (MT) power generation system, this paper analyzes its working mechanism and finds the reason lies in the slow response of the micro turbine output power adjustment. In order to make up for the shortage of the instantaneous output power of micro turbine, the method of instantaneous power fast control is proposed. Control algorithm of instantaneous compensation power is raised by power response prediction of MT. The high power dynamic response of super-capacitor energy storage can compensate low dynamic response problem of MT output power, so the instantaneous power of the system is real balance to ensure that the DC bus voltage is smooth and adaptability of MT power generation system is enhanced for impact load. Finally, the correctness and feasibility of the proposed control strategy are verified by simulation results.

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1. Introduction

With the rapid development of human society, the demand for energy power is increasing, and it is very important to improve the performance and energy efficiency of the power system. MT has the characteristics of high power density [1], high reliability, high efficiency [2], low maintenance and low emissions [3]. It can use natural gas, diesel, oil field associated gas and other fuels that does not rely on a single energy form [4]. In the aerospace, defense and other industries, such as ships, oil and gas production and other fields it has a wide range of applications, highly valued in recent years.

The impact load is generally present in distributed generation systems, which are related to the finite energy of distributed or independent generation system. For example, impact load cycling has been identified as being one of the main causes of fuel cell inefficiencies as a consequence of compressor inertia and gas manifolding effects [5]. For a constant speed wind turbine in an electrical network torque impact can lead to various active power quality, reactive power and r.m.s. phase to phase voltage problems [6]. Another example is solar energy source claimed as a clean and noise free source of electricity. Even so, a reliable energy storage

* Corresponding author. E-mail address: duanjiandong@hit.edu.cn (J. Duan). system is required as an energy buffer to bridge the mismatch between available and required energy [7]. In order to meet the impact load, the MT generation system must have the ability of fast adjustment of output power. However, the response of output mechanical power is slow because of slow MT combustion mechanism. This slow response characteristic cannot suit to the application object with impact load. Therefore, the development and popularization of MT generation system is restricted [8]. In order to solve this problem, it is needed to analyze the variation of MT output power in theory, and to further study and propose the solution based on instantaneous power balance.

An effective method to solve the impact load problem is to compensate for the slow response of the original motive output power by using the fast charge and discharge energy storage device. Supercapacitor has the advantages of long service life [9], high charge and discharge efficiency [10], short charge and discharge time and so on [11], which has been widely used in many applications such as wind generation system [12], fuel cell [5], electric vehicle [13] and battery energy storage system [14] mainly to solve the dynamic response problem. The corresponding coordinated control strategy can be divided into two types, one is based on the accurate information of the output power, and the other is not to need the exact information. Because of the easy to implement and no need to know detailed output characteristic, the methods of PI control [15], droop control, low pass filter [16], high pass filter and so on are widely used for smoothing the output power of the



Nomenclature		<i>K</i> _{SCp}	supercapacitor energy storage unit power loop
<i>m</i>	compution efficiency	V	proportional gain
η _B	efficiency of compressor	K _{vfi}	inverter voltage loop propertional gain
η _c	MT efficiency	κ _{vfp}	inverter voltage loop proportional gain
⁷ /MT	officiency of turbing	L_{dc}	supercapacitor energy storage unit output filter
η _t	MT closed loop poles		inductance
^k1,k2,k3	NIT closed loop poles	$L_{\rm f}$	inverter output filter inductance
$\omega_{\rm dc}$	PWM rectifier voltage loop corner frequency	Lg	synchronous inductance of permanent magnet
ω_{i}	inverter current loop cut-off frequency		synchronous motor
$\omega_{ m p}$	PWM rectifier power loop cut-off frequency	n	speed
ω_{SCc}	supercapacitor energy storage unit open loop cut-off	P_1	Inlet total pressure of compressor
	frequency	P_2	outlet total pressure of compressor
$\omega_{\rm V}$	inverter voltage loop cut-off frequency	P_3	input pressure of turbine
π_{c}	pressure ratio of compressor	P_4	output pressure of turbine
π_{t}	expansion ratio of turbine	Pc	consumption power of compressor
Α	MT system matrix	P _{ESSdc}	DC side power of supercapacitor energy storage unit
$a_{i,j}i,j=1$	1, 2, 3 MT system matrix coefficients	$P_{\rm f}$	input power of MT
В	MT input matrix	P _{Ldc}	DC side power of load
$b_i i = 1, 2$	2,3 MT input matrix coefficients	$P_{\rm L}$	load active power
С	DC bus capacitor	Pm	output power of MT
$C_{\rm f}$	inverter output filter capacitor	Prec	output power of PWM rectifier
$C_{\rm MT}$	MT output matrix	P_{SC}	supercapacitor output power
Gc	mass flow of compressor	P_{t}	output power of turbine
G_{f}	mass flow of fuel	$Q_{\rm L}$	load inactive power
$G_{inv}(s)$	inverter Transfer function	$Q_{\rm u}$	low heat value of fuel
$G_{\rm MT}(s)$	microturbine Transfer function	R _{dc}	supercapacitor energy storage unit output filter
$G_{\rm rec}(s)$	PWM rectifier Transfer function		resistance
Gt	mass flow of turbine	$R_{\rm f}$	inverter output filter resistance
$i_{\mathrm{f}lpha}, i_{\mathrm{f}eta}$	inverter output current in two phase stationary	Rg	stator winding resistance of permanent magnet
	coordinate		synchronous motor
$i_{\mathrm{fa}}, i_{\mathrm{fb}}$	inverter output current in three phase stationary	S_a, S_b, S_c	supercapacitor converter ratio
	coordinate	T_1	inlet temperature of compressor
i _{fref}	inverter output current set value	T_2	output temperature of compressor
$i_{\rm f}$	inverter output current	T'_2	temperature of cold outlet end
i _L	load current	T_3	input temperature of turbine
i _{SC}	supercapacitor current	T_4	output temperature of turbine
Κ	MT feedback matrix	T'_{A}	temperature of hot outlet end
$k_i i = 1, 2$	2,3 MT feedback matrix coefficients	Tsc	supercapacitor energy storage unit power sampling
<i>K</i> _{dci}	PWM rectifier voltage loop integral gain	50	filter time constant
<i>K</i> _{dcp}	PWM rectifier voltage loop proportional gain	Vdcref	DC bus voltage set value
$K_{\rm dc}$	supercapacitor energy storage unit system gain	$v_{f\alpha}, v_{f\beta}$	inverter output voltage in two phase stationary
K _{ifi}	inverter current loop integral gain	iu, ib	coordinate
K _{ifp}	inverter current loop proportional gain	Vfa, Vfb	inverter output voltage in three phase stationary
K _{pi}	PWM rectifier power loop integral gain	' Ia / " ID	coordinate
K _{pp}	PWM rectifier power loop proportional gain	$v_{\rm fref}$	inverter out voltage set value
K _{SCi}	supercapacitor energy storage unit power loop integral	$v_{\rm f}$	inverter output voltage
	gain	v_{SC}	supercapacitor voltage
		*	refers to the stagnation parameter

generation system [17]. The difficulty of these methods lies in the choice of the control strategy and the design of the controller, which needs to achieve the maximum power output of the generation system and smooth the output power. These methods are passive response control strategies, so the control response is slow, and the power distribution between the prime generation equipment and the energy storage is not easy to achieve optimization.

In this paper, the supercapacitor energy storage is applied to the MT generation system, and for impact load compensation the instantaneous power fast control method is proposed. Control algorithm of instantaneous compensation power is raised by power response prediction of MT. The high power dynamic response of super-capacitor energy storage can compensate low dynamic

response problem of MT output power, so the instantaneous power of the system is real balance to ensure that the DC bus voltage is smooth and adaptability of MT power generation system is enhanced for impact load. The control strategy is proposed based on the characteristics of the MT output power, which has faster response, better power distribution between prime generation system and energy storage.

The remainder of this paper is organized as follows. In Section 2, the structure of MT generation system is analyzed. In Section 3, MT model is established and output characteristics is analyzed. In Section 4, instantaneous power compensation control is proposed, witch is validated in Section 5, and conclusions are drawn in Section 6.

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