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On subsurface fracture opening and closure

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ABSTRACT

Understanding of subsurface fracture opening and closure is of great importance to oil/gas production, geothermal energy extraction, radioactive waste disposal, and carbon sequestration and storage. Fracture opening and closure involve a complex set of thermal, hydrologic, mechanical and chemical (THMC) processes. In this paper, a fully coupled THMC model for fracture opening and closure is formulated by explicitly accounting for the stress concentration on aperture surface, stress-activated mineral dissolution, pressure solution at contacting asperities, and channel flow dynamics. A model analysis, together with reported laboratory observations, shows that a tangential surface stress created by a far-field compressive normal stress may play an important role in controlling fracture aperture evolution in a stressed geologic medium, a mechanism that has not been considered in any existing models. Based on the model analysis, a necessary condition for aperture opening has been derived. The model provides a reasonable explanation for many salient features of fracture evolution in laboratory experiments, including a spontaneous switch from a permeability reduction to a permeability increase in a static limestone experiment. The work may also help develop a new method for estimating in-situ stress in a reservoir.

1. Introduction

Understanding of fracture opening and closure in geologic media is crucial for oil/gas production, geothermal energy extraction, radioactive waste disposal, and carbon sequestration and storage (e.g., [Yasuhara et al., 2006](#page--1-0); [Ellis et al., 2013](#page--1-1)). It has been observed that, under certain circumstances, a fracture can undergo either opening or closure or switch from one regime to another [\(Polak et al., 2004; Liu](#page--1-2) [et al., 2006; McGuire et al., 2013](#page--1-2)). Fracture evolution involves a complex set of coupled physical and chemical processes, including stress-mediated mineral dissolution/precipitation, fluid flow and transport, mechanical deformation, etc. Significant effort has been made to understand these processes in laboratories. For example, in a flowthrough experiment on a natural novaculite fracture under moderate effective stress (~14 bars), [Yasuhara et al. \(2006\)](#page--1-0) observed a reduction in fracture permeability for the first 1500 h followed by a significant increase in fracture aperture as the fluid flow rate and the temperature in the experiment were ramped up. In a similar experiment on a limestone fracture, [Polak et al. \(2004\)](#page--1-2) observed that, during the initial circulation of groundwater, the differential pressure increased about threefold as the contacting asperities across the fracture were removed. Interestingly, after switching to distilled water, they first observed another threefold reduction in permeability and then a spontaneous switch from a permeability reduction to a permeability increase without any change in experimental conditions. The underlying mechanism

for this switch is unknown. An increase in permeability usually involves preferential dissolution channeling ([Elkhoury et al., 2013](#page--1-3)).

Various models have been developed for fracture opening and closure, with various levels of complexity with respect to process couplings, ranging from a simple geometrical model to a coupled thermal-hydrologic-mechanical-chemical (THMC) model [\(Table 1\)](#page-1-0). However, those models are to a large extent empirical and thus not amenable for predictions. No existing model is able to provide a consistent explanation for some key features of fracture evolution often observed in laboratory experiments, for example, a spontaneous transition from a permeability reduction to a permeability increase ([Polak et al., 2004](#page--1-2)), an enhancement of fracture permeability by temperature ([Yasuhara et al., 2006](#page--1-4)), or a similar enhancement by a low-pH solution [\(McGuire et al., 2013](#page--1-5)). Questions, such as what role a normal stress would play in fracture evolution and under what conditions a fracture would tend to open or close, still remain open.

The objective of this paper is to lay a theoretical foundation for modeling subsurface fracture opening and closure. The model proposed below is a fully coupled THMC model that explicitly accounts for three key processes: (1) stress concentration around individual aperture channels, (2) stress-activated mineral dissolution on fracture surfaces, and (3) reactive infiltration instability of fluid flow in fracture aperture. This model is based on a recent observation in materials science that a tangential surface stress may enhance or inhibit mineral reaction on a stressed solid surface ([Aziz et al., 1991; Yu and Suo,](#page--1-6)

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Table 1

Type Model

[Szymczak and](#page--1-12) [Ladd \(2009,](#page--1-12) [2012\)](#page--1-12)

 HM Zhao et. (2014)

[Souley et al.](#page--1-14) [\(2015\)](#page--1-14)

[Memoto et al.](#page--1-15) [\(2009\)](#page--1-15)

[Min et al.](#page--1-16) [\(2004\)](#page--1-16)

[Pyrak-Nolte](#page--1-17) and [Morris](#page--1-17) [\(2000\)](#page--1-17)

MC [Beeler and](#page--1-18) [Hickman](#page--1-18) [\(2004\)](#page--1-18)

Survey of models for fract mechanical model; HC- hydrologic-chemical model; HM – hydrologic-chemical model; MC – mechanical-chemical model; HMC - hydrologic-mechanical-chemical model; THMC – thermal-hydrologic

a $\frac{b^2}{2} + \frac{(y'-h)^2}{b'^2} = 1$ (1) $\frac{1}{2}$

$$
\frac{x'^2}{a'^2} + \frac{(y' + h)^2}{b'^2} = 1\tag{2}
$$

where x' and y' are the local coordinates; and a' and b' are the major and minor semi-axes of the two intersecting ellipses respectively. Parameters a' and b' are related to the semi-axes of the truncated ellipse (a, b) by [\(Fig. 2\)](#page--1-8):

Crack stiffness; Water saturation degree w/r prop

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