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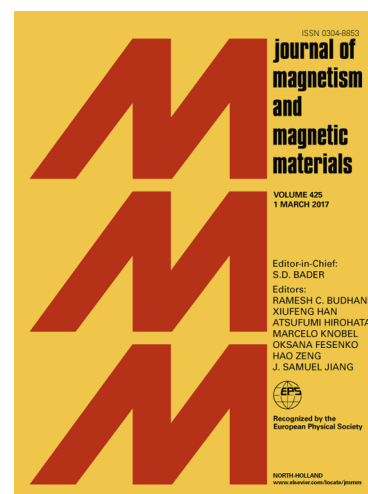
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# Magnetic and dielectric properties in the UHF frequency band of half-dense Ni-Zn-Co ferrites ceramics with Fe-excess and Fe-deficiency

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This work investigates electromagnetic properties of half-dense ceramics with compositions  $\text{Ni}_{0.5}\text{Zn}_{0.3}\text{Co}_{0.2}\text{Fe}_y\text{O}_{4-\delta}$  where  $y=1.98$  (Iron deficient, noted ID) or  $y=2.3$  (Iron in excess, noted IE). IE and ID materials are obtained by chemical coprecipitation route. The obtained nano-sized powders are pressed and annealed at two temperatures (800 °C, 900 °C), so has to obtain half-massive ceramics. Ferrous and ferric ions coexist in the crystalline structures, but the former in a less extend for ID ferrite. The concomitant influences of  $\text{Fe}^{2+}$  and  $\text{Fe}^{3+}$  on the dielectric and magnetic losses ( $\epsilon''/\epsilon'$  and  $\mu''/\mu'$ , respectively) are considered at frequency up to 6 GHz. The permeability dispersion changes from relaxation-like to resonance-like with the decrease in ferrous ions. In reason of the relaxing-like behavior of  $\text{Fe}^{2+}$ , and because of a relatively high amount in  $\text{Fe}^{2+}$ , IE sample shows lower total losses (magnetic and dielectric) than ID sample. These conclusions applied for  $T_A=900$  °C. At frequencies above 700 MHz, the total loss values (IE and ID samples) are prohibitive for antenna downsizing whatever is the firing temperature value (800 °C and 900 °C). Whereas at frequencies below 700 MHz  $\text{Ni}_{0.5}\text{Zn}_{0.3}\text{Co}_{0.2}\text{Fe}_{2.3}\text{O}_{4-\delta}$  may leads to better antenna performances than  $\text{Ni}_{0.5}\text{Zn}_{0.3}\text{Co}_{0.2}\text{Fe}_{1.98}\text{O}_{4-\delta}$ .

**Index Terms**— Iron-excess ferrites, magnetic permeability, Microwave frequencies.

## 1. Introduction

There is an increasing demand of antenna downsizing, which especially concerns the electronic devices for mobile communication and aerospace areas [1]. In this topic, size reduction is frequently reached using high-permittivity substrates. However a drawback is a considerable decrease in antenna efficiency and bandwidth [2,3]. It has been shown that the use of magneto-dielectric substrates for applications in the low-UHF frequency band (300-900 MHz) may get over these limitations. Actually, using such materials (with permeability  $\mu^* = \mu' + j\mu''$  and permittivity  $\epsilon^* = \epsilon' + j\epsilon''$ , where  $\mu' > 1$  and  $\epsilon' > 1$ ) led to larger bandwidths and improved efficiency for the antenna [4,5]. Indeed, the permeability ( $\mu'$ ) decreases the detrimental effects of losses, whereas the permittivity ( $\epsilon'$ ) -while increasing the stored energy- has the opposite effect. Then the permeability presents a positive impact on antennas' performances, which counterbalance the negative impact of permittivity. An example is provided by the antenna efficiency  $\eta$ . An ideal transmitting antenna

accepts power ( $P_{\text{input}}$ ) from a source and radiates the power ( $P_{\text{radiated}}$ ) into space. The ratio of  $P_{\text{radiated}}$  to  $P_{\text{input}}$  is the antenna efficiency  $\eta$  (Eq.1) [6], which affects the ability of an antenna to generate far field electromagnetic radiation. Let us consider a patch antenna of width  $W$  over a magneto-dielectric substrate ( $\mu$ ,  $\epsilon$ ) of thickness  $d$ . Eq.(1), illustrates the opposite roles taken by  $\mu'$  and  $\epsilon'$  on the antenna efficiency. Actually in this equation, where  $G_r$  is the radiation conductance of the antenna [7],  $L$  represents the sum of magnetic and dielectric losses (defined as  $\mu''/\mu'$  and  $\epsilon''/\epsilon'$ , respectively). It is clear from Eq.(1) that to use a substrate with  $\mu > 1$  would lead to compensate -at least partly- the undesirable effects coming from  $L$ .

$$\eta = \left(1 + \frac{L}{240 G_r d} \sqrt{\frac{\epsilon}{\mu}}\right)^{-1} \quad (1)$$

The materials intended to be used for antenna miniaturization should show  $\epsilon' > 1$  and  $\mu' > 1$ , together with low loss tangents (both dielectric and magnetic) [8,9]. Bulk spinel ferrites meet these requirements up to frequency values about 300 MHz, but show detrimental magnetic losses at higher frequencies. Elevated sintering temperatures are usually required (1100 °C-1200 °C) in order to obtain such dense ferrite substrates [9,10]. Actually this allows a large grain growth, and therefore a multi-domain magnetic grain structure by which high permeability values are ensured. As a counterpart, domain-wall bulging results in magnetic losses. These losses remain high from the quasistatic frequencies until several 100 MHz. There is an upper limit of frequency above which ferro-ferrimagnetic materials cannot be used for low-loss electromagnetic devices applications. This limit is fixed by the ferromagnetic resonance frequency  $f_R$  (The observed maximum of  $\mu''$  in the  $\mu''$ - $f$  curve obtained on polycrystalline materials, accords with the resonance frequency; this feature defined the ferro-ferrimagnetic resonance  $f_R$  [11]). Above this cut-off value of frequency there is a large increase in magnetic losses, which runs along with a decrease in permeability. This was recognized by Snoek [12], who stated first the following relationship that exists between the static permeability  $\mu_s$  and the spin resonance frequency  $f_R$ :  $(\mu_s - 1) \cdot f_R = 2/3 \bar{\gamma} M_s$ , where  $M_s$  is the magnetization at saturation and  $\bar{\gamma}$  is the gyromagnetic ratio ( $\bar{\gamma} = 35.185$  MHz/kA.m<sup>-1</sup>). For most bulk materials, Snoek's law applies [13]. More recently, the following

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