FISEVIER

Contents lists available at ScienceDirect

Mechanical Systems and Signal Processing

journal homepage: www.elsevier.com/locate/ymssp



Review

Non-linearities in the vibrations of elastic structures with a closing crack: A state of the art review



A. Bovsunovsky a, C. Surace b,*

- ^a Department of Mechanical Engineering, Standardization and Certification of Equipment, National University of Food Technologies, 68 Vladimirska Str., 03033 Kiev, Ukraine
- ^b Department of Structural Geotechnical and Building Engineering, Politecnico di Torino, corso Duca degli Abruzzi 24, 10129 Torino, Italy

ARTICLE INFO

Article history: Received 11 September 2014 Received in revised form 12 December 2014 Accepted 22 January 2015 Available online 12 March 2015

Keywords:
Closing crack
Non-linearities
Cracked beams
Cracked shafts
Cracked plates
Crack detection techniques

ABSTRACT

The main purpose of the present review paper is to illustrate the principal achievements of numerous researchers who have studied the non-linear effects caused by a closing crack in the most common types of structural elements such as beams, shafts and plates, the aim being to assess the potential and future prospects of using non-linear behaviour to detect damage. Indeed, for a wide range of practical applications, in order to avoid catastrophic failure, the development of diagnostics techniques which are sufficiently sensitive to incipient cracks in structures and machines is a crucial issue. The main potential advantage of using vibration diagnostics based on the use of non-linear effects is the relatively high sensitivity to the damage of the closing crack type, especially for application to beam-like structures and rotating shafts; instead the potential for application to plate-like structures has been found to be limited.

After analysing the state-of-art on this subject in detail, a discussion of the respective merits, drawbacks and prospects of a range of non-linear vibration methods for structural damage detection is presented. The general conclusion which can be drawn from the highly encouraging results of recent research is that further development of these techniques for non-destructive testing of structures with closing cracks would be highly worthwhile.

© 2015 Elsevier Ltd. All rights reserved.

Contents

1.	Introd	luction	130
2.	Single	-degree-of-freedom (SDOF) oscillators simulating elastic bodies with a closing crack	132
	2.1.	Models of a cracked body	132
	2.2.	Free vibrations	132
	2.3.	Forced vibration	132
3.	Vibrat	ion of cracked beams	133
	3.1.	Simulation of a crack	133
	3.2.	Models of cracked beams	134
	3.3.	Free and resonant vibrations.	135

^{*}Corresponding author: Tel.: +39 110904904; fax: +39 110904899.

E-mail addresses: apbovsunovsky@gmail.com (A. Bovsunovsky), cecilia.surace@polito.it (C. Surace).

	3.4.	Sub- and superharmonic resonance vibrations	136
	3.5.	Forced oscillations far from resonance	137
	3.6.	Phase plots (trajectory)	138
	3.7.	Special methods for increasing the sensitivity of crack detection.	138
4.	Vibrat	ions of cracked shafts (rotors).	138
	4.1.	Features of vibrations of the rotating shaft with a closing crack	138
	4.2.	Crack models	139
	4.3.	Coupled vibration of a rotating shafts	140
	4.4.	Additional (non-linear) resonances.	140
	4.5.	Spectrum of vibration	141
		4.5.1. Transverse crack	141
		4.5.2. Slant crack	142
	4.6.	Phase plane plots	142
	4.7.	Additional excitation of a cracked rotor	142
	4.8.	Methods for increasing the sensitivity of vibration diagnostics	143
	4.9.	Direct experiments on non-linear vibrations of rotors	144
5.	Vibrat	ions of cracked plates (composite plates with closing delamination)	144
6.		isions: Advantages, drawbacks and future prospects of non-linear vibration methods for damage detection	
	Refere	nces	146

Nomenclature			critical backward whirl speed
		$arOlema_f$	critical forward whirl speed
а	crack depth	$arOlimits_{tr}$	frequency of torsional vibration
h	cross-section height	$\eta = \Omega/\mathcal{G}$	Ω_{cr} relative speed of rotation
$\gamma = a/h$	relative crack depth	φ	angular position of imbalance
İ	second moment of cross section area	θ	angle of crack opening
I_c	second moment of cracked cross section area	h_{sh}	thickness of a shell
H	Heaviside function	f_{exc}	frequency of excitation
L	length of beam or plate	f_{rel}	relative frequency of driving force
L_d	delamination length	R	restoring force
L_C	crack location	LP	low pressure
L_p	driving force application point	3D	three-dimensional
M_{S}	bending moment	FEM	finite element model
r	shaft radius	FRF	frequency response function
$\mu = a/r$	shaft relative crack depth	DOF	degrees-of-freedom
Ω	speed of rotation	SIF	stress intensity factor
Ω_0	shaft eigenfrequency	WT	wavelet transform
Ω_{cr}	critical speed of rotation	δ	logarithmic decrement of vibration

1. Introduction

The first works on the impact of local defects on the vibration characteristics of structural elements were performed by Kirmsher [1] in 1944 and Thomson [2] in 1949. In these studies approaches were proposed to the modelling of damage of a fatigue crack type, as well as the methods of determining the natural frequencies of vibrations of beams with a crack. As numerous studies have demonstrated [3], the change of natural frequencies and mode shapes seem insufficient to detect small cracks. A search for vibration characteristics that are more sensitive to the presence of damage and easy to apply still continue today. These characteristics include: the change of damping, the sub- and superharmonic vibrations, non-linear distortion of vibration at the principal resonance, the change of transfer function, the distortion of phase trajectories, antiresonance frequencies, mechanical impedance and static and dynamic compliance [4].

In many studies the slot type model of a crack was used. The crack is supposed to be constantly open regardless of the stress sign (the so called open crack). In this case the characteristic of the restoring force remains linear (Fig. 1a). However, such a simplification of the problem leads to the over estimation of changes in natural frequencies and mode shapes, as compared with the effect of the real crack [5,6]. Moreover, the models with an open crack are not suitable to describe the non-linear behaviour of structures with closing cracks and so are unable to identify the sub- and superharmonic resonances.

Real cracks usually are formed as a result of fatigue and corrosion and have the possibility of opening during the stretching cycle and closing during the compression cycle, thereby changing the stiffness of a body in the process of its cyclic deformation. That is why these cracks are referred to as closing or breathing (Fig. 2). It is assumed that the stiffness of the

Download English Version:

https://daneshyari.com/en/article/560142

Download Persian Version:

https://daneshyari.com/article/560142

<u>Daneshyari.com</u>