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### Reuse of Fenton sludge as an iron source for NiFe<sub>2</sub>O<sub>4</sub> synthesis and its application in the Fenton-based process

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#### Introduction 48

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49 The Fenton process, which is based on the generation of hydroxyl radicals (HO.) from hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) in the 50presence of Fe<sup>2+</sup>, has been extensively studied and successfully 51applied for the effective treatment of various industrial waste-52waters (Bautista et al., 2008; Pignatello et al., 2006). However, 53 despite its simplicity, the main weakness of the Fenton process 54is the formation of sludge during neutralization after Fenton 55

oxidation (Ma and Xia, 2009). The yield of Fenton sludge is 56 dependent upon the ratio and volume of the added reagents. 57 Due to the residual of toxic organics or heavy metals in it, sludge 58 from the Fenton process treating recalcitrant industrial waste- 59 water is often disposed as hazardous solid waste, which leads to 60 high sludge disposal cost and the risk of secondary pollution. 61 Therefore, Fenton sludge is the main obstacle preventing full 62 scale application of the Fenton process in the field of industrial 63 wastewater treatment (Bautista et al., 2008). 64

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# ABSTRACT

The potentially hazardous iron-containing sludge from the Fenton process requires proper treatment and disposal, which often results in high treatment cost. In this study, a novel method for the reuse of Fenton sludge as an iron source for the synthesis of nickel ferrite particles (NiFe<sub>2</sub>O<sub>4</sub>) is proposed. Through a co-precipitation method followed by sintering at 800°C, magnetic NiFe<sub>2</sub>O<sub>4</sub> particles were successfully synthesized, which was confirmed by powder X-ray diffraction (XRD), scanning electronic microscopy (SEM), energy dispersive spectroscopy (EDS), Fourier transform infrared spectroscopy (FT-IR) and Raman spectroscopy. The synthesized NiFe<sub>2</sub>O<sub>4</sub> could be used as an efficient catalyst in the heterogeneous Fenton process. In phenol degradation with H<sub>2</sub>O<sub>2</sub> or NiFe<sub>2</sub>O<sub>4</sub> alone, the phenol removal efficiencies within the reaction time of 330 min were as low as  $5.9\% \pm 0.1\%$  and  $13.5\% \pm$ 0.4%, respectively. However, in the presence of both  $NiFe_2O_4$  and  $H_2O_2$ , phenol removal efficiency as high as 95% ± 3.4% could be achieved, indicating the excellent catalytic performance of NiFe<sub>2</sub>O<sub>4</sub> in the heterogeneous Fenton process. Notably, a rapid electron exchange between =Ni<sup>II</sup> and =Fe<sup>III</sup> ions in the NiFe<sub>2</sub>O<sub>4</sub> structure could be beneficial for the Fenton reaction. In addition, the magnetic catalyst was relatively stable, highly active and recoverable, and has potential applications in the Fenton process for organic pollutant removal

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To minimize the production of Fenton sludge, two approaches 65 have been suggested, i.e., development of heterogeneous 66 catalysts and reuse of iron in the sludge. Various heterogeneous 67 catalysts have been developed, such as natural minerals 68 (Garrido-Ramirez et al., 2010), iron-containing clays (Navalon 69 et al., 2010), iron immobilized on solid support (Aleksić et al., 70 71 2010) and zero-valent iron (Shen et al., 2013; Liu et al., 2015). Heterogeneous catalysts are superior to the traditional homo-72 geneous catalyst, i.e., Fe<sup>2+</sup>, due to the easy separation of the 73 catalysts from the treated wastewater by sedimentation or an 74 external magnetic field (Liu et al., 2012). Therefore, generation 75of Fenton sludge in a heterogeneous Fenton system can be 76 reduced to some extent. However, the catalytic activity is 77 usually deteriorated after repetitive use due to the leaching of 78 active iron (Ji et al., 2011) or the decay of active catalytic sites 79 80 (Takbas et al., 2008). Recently, reuse of iron-containing Fenton sludge has been drawing increasing interest from researchers 81 world-wide. Yoo et al. (2001) suggested the recycling of sludge 82 generated from Fenton oxidation in a coagulation process. With 83 the recycling of Fenton sludge, the sludge to be disposed could 84 be reduced up to 50% and the coagulant could be reduced by 85 50%. Sheu and Weng (2001) developed a recycling system based 86 on the reduction of Fe<sup>3+</sup> by H<sub>2</sub>O<sub>2</sub> to produce Fe<sup>2+</sup>, which could be 87 used as a Fenton reagent. Bolobajev et al. (2014) developed a 88 89 sequential Fenton/Fenton-based system for the treatment of 90 landfill leachate. Iron-containing sludge produced from the 91 Fenton process could be reused as an iron source in the 92following Fenton-based system, thus production of hazardous ferric waste could be minimized. Cao et al. (2009) presented a 93 simple method for recovering the iron catalyst from the iron 9495 hydroxide sludge for oxidative treatment of industrial wastewaters. The sludge was dewatered, dried and baked at 350-96 400°C, and then the residual solids were dissolved in sulfuric 97 acid to form a reusable catalyst for Fenton and Fenton-like 98 reactions. The reuse routines mentioned above are beneficial 99 for the reduction and minimization of iron-containing sludge 100 compared with traditional treatment processes. However, they 101 increase the overall cost and operational difficulty because of 102 the low utilization efficiency or additional sludge regeneration 103 step. In addition, a feasible method for final and thorough 104 disposal of Fenton sludge has not been suggested so far. 105106 Resourcization of Fenton sludge in order to achieve final and 107 thorough disposal merits investigation.

Recently, ferrites, such as NiFe<sub>2</sub>O<sub>4</sub>, CuFe<sub>2</sub>O<sub>4</sub> and ZnFe<sub>2</sub>O<sub>4</sub>, have 108 drawn much more attention due to their potential application in 109 the fields of catalysis (Rashad and Fouad, 2005), high sensitivity 110 gas sensors (Rezlescu et al., 2006), magnetic fluids (Hasmonay 111 112et al., 2000) and microwave devices (Giannakopoulou et al., 2002). Sugimoto et al. (1998) suggested that ferrites could be synthesized 03 by using ferric salts as raw material. Recently, ferrite has been 114 115used as the catalyst for heterogeneous photo-Fenton or Fentonlike processes (Liu et al., 2012; Marco et al., 2014). However, to the 116 best of our knowledge, preparation of ferrite using Fenton sludge 117 as an iron source and application of the obtained ferrite as a 118 119 Fenton catalyst have not yet been reported.

In this work, a new reuse method for Fenton sludge was investigated. The iron-containing Fenton sludge was used as an iron source for the synthesis of nickel ferrite (NiFe<sub>2</sub>O<sub>4</sub>), which was used as a catalyst in the Fenton process. Thus, the objectives of this study were: (1) to synthesize and to characterize NiFe<sub>2</sub>O<sub>4</sub>, (2) to evaluate the catalytic properties  $^{125}$  and stability of the synthesized NiFe<sub>2</sub>O<sub>4</sub>, and (3) to propose a  $^{126}$  possible catalytic mechanism for the Fenton process using  $^{127}$  NiFe<sub>2</sub>O<sub>4</sub> as catalyst.  $^{128}$ 

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### 1. Experimental

#### 1.1. Characterization of Fenton sludge

The iron-containing sludge derived from the Fenton process 132 was characterized as follows. The chemical oxygen demand 133 (COD) value was found to be  $6500 \pm 500$  mg/L. The total iron 134 content of the sludge was as high as  $7.67 \pm 1.87$  g/L, which 135 provided a rich iron source for the synthesis of NiFe<sub>2</sub>O<sub>4</sub>. The 136 ratio of volatile solids (VS) to total solids (TS) was 90.46%  $\pm$  137 2.43%, indicating the presence of abundant organics in the 138 sludge. In addition, the iron-containing sludge was fluidized, 139 with water content and total solid content of 89.65%  $\pm$  1.75%, respectively.

### 1.2. Synthesis of NiFe<sub>2</sub>O<sub>4</sub> from Fenton sludge

NiFe<sub>2</sub>O<sub>4</sub> particles were synthesized according to the controlled 143 co-precipitation method (Kulkarni et al., 2014). Before the Q4 synthesis process, the iron content in the Fenton sludge was 145 determined. Ni(NO<sub>3</sub>)<sub>2</sub> was dissolved into ultrapure water, and 146 then Ni(NO<sub>3</sub>)<sub>2</sub> solution was added and mixed into the Fenton 147 sludge at Fe/Ni mole ratio of 2:1. Then 4 mol/L sodium 148 hydroxide solution was added dropwise into the mixture of 149 Fenton sludge and Ni(NO<sub>3</sub>)<sub>2</sub> to adjust the pH value to 9.0-10.0. 150 During this procedure, the mixture was continuously stirred 151 using a magnetic agitator and kept at a temperature of 50°C. 152 Six hours later, the resultant precipitate was filtered and 153 washed with ultrapure water until the pH value of the filtrate 154 reached 7.0. The solid product was dried in a vacuum oven 155 at 100°C for 8 hr and then sintered at 800°C for 6 hr. The 156 obtained particles were ground and stored for further charac- 157 terization and application. 158

### 1.3. Application of NiFe<sub>2</sub>O<sub>4</sub> in heterogeneous Fenton process 159

The heterogeneous Fenton reaction for phenol degradation 160 was performed in 100 mL centrifuge tubes containing 50 mL 161 phenol solution. The initial phenol concentration and the 162 initial pH of the phenol solution were 250 mg/L and 3.0, 163 respectively. Then  $H_2O_2$  and the obtained NiFe<sub>2</sub>O<sub>4</sub> powder 164 were added at dosages of 120 mmol/L and 2.0 g/L to initiate 165 the Fenton reaction. The Fenton reaction was carried out on a 166 rotary shaker at 25°C and 200 r/min. After Fenton reaction, 167 NiFe<sub>2</sub>O<sub>4</sub> was collected by magnetic separation for possible reuse. 168 The control reactions carried out with NiFe<sub>2</sub>O<sub>4</sub> but without  $H_2O_2$  169 or with  $H_2O_2$  but without NiFe<sub>2</sub>O<sub>4</sub> were performed in the same 170 manner. 171

### **1.4.** The role of the leached iron ions in Fenton process

To evaluate the contribution of homogeneous Fenton oxidation 173 catalyzed by the leached iron ions in the phenol degradation 174 process, the role of the leached iron ions was investigated. After 175

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