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Q1 **Achieving partial nitrification by inhibiting the activity of**  
 2 **Nitrospira-like bacteria under high-DO conditions in an**  
 3 **intermittent aeration reactor**

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**ABSTRACT**

It is generally accepted that a low dissolved oxygen (DO) concentration is more beneficial 16  
 for achieving partial nitrification than high-DO. In this study, partial nitrification was not 17  
 established under low-DO conditions in an intermittent aeration reactor for treating 18  
 domestic wastewater. During the operational period of low-DO conditions (DO:  $0.3 \pm 19$   
 $0.14$  mg/L), stable complete nitrification was observed. The abundance of Nitrospira-like 20  
 bacteria, which were the major nitrite-oxidizing bacteria, increased from  $1.03 \times 10^6$  to 21  
 $2.64 \times 10^6$  cells/mL. At the end of the low-DO period, the batch tests showed that high-DO 22  
 concentration ( $1.5, 2.0$  mg/L) could inhibit nitrite oxidation, and enhance ammonia 23  
 oxidation. After switching to the high-DO period ( $1.8 \pm 0.32$  mg/L), partial nitrification was 24  
 gradually achieved. Nitrospira decreased from  $2.64 \times 10^6$  to  $8.85 \times 10^5$  cells/mL. It was found 25  
 that suddenly switching to a high-DO condition could inhibit the activity and abundance of 26  
 Nitrospira-like bacteria, resulting in partial nitrification. 27

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40 **Introduction**

42 Partial nitrification, which avoids the oxidation of nitrite to  
 43 nitrate, is a critical step in some biological nutrient removal  
 44 processes (e.g. SHARON-ANAMMOX, CANON, OLAND) (Van  
 45 Hulle et al., 2010; Regmi et al., 2014). Compared to traditional  
 46 nitrification–denitrification nitrogen removal processes, pro-  
 47 cesses with partial nitrification are less expensive since they  
 48 consume less oxygen and less carbon-source (Ahn, 2006). The  
 49 establishment of partial nitrification is always the key to the  
 50 implementation of these processes, but it is difficult to  
 51 achieve. At present, several effective methods have been  
 52 developed to achieve partial nitrification, which are mainly  
 53 based on high temperature (Ge et al., 2015), high free  
 54 ammonia concentrations (FA) (Zhang et al., 2014), high free

nitrous acid (FNA) (Ge et al., 2015), aeration duration control 55  
 (Ma et al., 2016), inhibitors and low dissolved oxygen (DO) 56  
 concentration (Peng and Zhu, 2006). 57

Among these factors, low-DO concentration has been 58  
 widely reported to successfully achieve partial nitrification 59  
 in wastewater treatment systems (Peng and Zhu, 2006; Ma 60  
 et al., 2009, 2011). It is commonly recognized that the activity 61  
 of ammonium-oxidizing bacteria (AOB) is higher than that of 62  
 nitrite-oxidizing bacteria (NOB) under low-DO conditions. 63  
 This is because the oxygen half-saturation constant ( $K_o$ ) 64  
 of AOB is lower (Hanaki et al., 1990; Manser et al., 2005; 65  
 Stenstrom, 1990), resulting in NOB being gradually selected Q3  
 out due to the stronger inhibition by low-DO conditions. 67  
 However, Liu and Wang (2013) recently found their reactors 68  
 performed complete nitrification during long-term operation 69

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under low-DO conditions. Similarly, Park and Nogura (2004) suggested that complete and stable nitrification could be maintained even at a low-DO level (0.12 mg/L). Moreover, Regmi et al. (2014) found that the  $K_o$  of AOB (1.16 mg- $O_2$ /L) was significantly higher than that of NOB (0.16 mg- $O_2$ /L) in their reactor. These contradictory findings suggest that there is a high probability of not achieving partial nitrification in some low-DO reactors, which can adversely affect processes based on partial nitrification. However, there has been limited understanding of how to start-up or recover partial nitrification in a low-DO reactor performing complete nitrification.

In our study, an intriguing phenomenon was observed in an intermittent aeration nitrifying reactor treating organic-removed domestic wastewater. Complete nitrification was maintained under the low-DO concentration, but partial nitrification was started up under the high-DO concentration. In order to determine the mechanism of the start-up of partial nitrification, the nitrogen removal performance of the sequencing batch reactor (SBR) was monitored, and the activity and community of nitrifying bacteria were detected by batch experiments and biological methods.

## 1. Materials and methods

### 1.1. Experimental bioreactor set-up and operating conditions

An SBR with a working volume of 10 L was used which included two operational stages: low-DO stage (DO:  $0.3 \pm 0.14$  mg/L) and high-DO stage (DO:  $1.8 \pm 0.32$  mg/L). The SBR was operated at a fixed temperature of 25°C using an electric heater. The oxygen required for the nitrification process was supplied by an air pump through a flow meter. A mechanical stirrer was used to ensure a completely mixed status during the nitrification process. The pH, DO and temperature in the reactor were monitored using an on-line multi-parameter sensor (WTW 3420, Germany). The pH was not controlled in the reactor. The operational stage in each cycle included four periods, namely 10 min feeding period, variable-length intermittent aeration (10 min aeration/10 min anoxic) period, 30 min settling period, and 15 min discharging of 5 L supernatant period. The terminal point of nitrification was judged by the real-time control of DO concentration. The endpoint values were 0.7 mg/L in the low-DO stage and 3 mg/L in the high-DO stage. The SRT was maintained at 30 days by withdrawing the activated sludge regularly. The mixed liquor suspended solids (MLSS) was maintained at  $1500 \pm 134$  mg/L, and the effluent suspended solids (SS) was  $24 \pm 8$  mg/L.

The influent to the nitrifying SBR was domestic wastewater from which the organics had been removed in an activated sludge bioreactor by direct aeration for a short time (35 min). The characteristics of the influent were as follows: COD: 40–55 mg/L,  $NH_4^+$ -N: 50.2–80.4 mg/L,  $NO_2^-$ -N: 0.1–5.4 mg/L,  $NO_3^-$ -N

0.04–1.24 mg/L, and pH 7.2–7.8. Activated sludge taken from a pilot-scale SBR (volume: 7000 L) was used as the inoculum.

### 1.2. Batch experiments

Batch experiments were carried out to investigate the effect of DO fluctuation on the nitrifying performance of the activated sludge acclimated to the stable DO concentration. The experiments were conducted in a lab-scale SBR with a working volume of 2.5 L at the end of the low-DO stage and the high-DO stage, separately. The sludge was taken from the operating SBR (10 L) and washed three times with deionized water before being transferred to the 2.5 L SBR. The synthetic wastewater was prepared from a solution of  $NH_4Cl$  and  $NaNO_2$ . The initial  $NH_4^+$ -N and  $NO_2^-$ -N concentrations were 40 mg/L and 20 mg/L, respectively. Different DO concentrations (0.3, 0.5, 1.0, 1.5 and 2.0 mg/L) were applied in the batch experiment. A variable frequency air pump was used to adjust air flow automatically according to the DO probes, in order to ensure a stable DO concentration. The initial MLSS in each 2.5 L SBR was kept at 2000 mg/L. The temperature was maintained at 24°C and the pH was kept at 7.2 by adding  $NaHCO_3$  solution. The batch experiments were operated in triplicate for each DO concentration.

### 1.3. Analytical methods

$NH_4^+$ -N,  $NO_2^-$ -N and  $NO_3^-$ -N concentrations were measured using a Quickchem® 8500 system (Hach Company, Lachat Instruments, USA), while the chemical oxygen demand (COD), SS and MLSS, MLVSS were analyzed using standard methods (American Public Health Association, 1998).

### 1.4. DNA extraction and quantitative PCR assay

Total DNA was extracted from 0.1 g of lyophilized sludge using a Fast DNA Spin Kit for Soil (QBIogen Inc., Carlsbad, CA, USA), following the manufacturer's instructions. The DNA samples were stored at -20°C. The concentration of DNA was measured using a Nanodrop ND-1000 UV-Vis Spectrophotometer (NanoDrop Technologies, Wilmington, DE, USA).

Quantitative PCR was performed with a Stratagene Mx3000P QPCR System (Agilent Technologies, USA), using the fluorescent dye SYBR-Green approach (TAKARA, Dalian, China). Three coupled primers (Table 1) were used to amplify the AOB and NOB (*Nitrobacter*, *Nitrospira*), namely amoA-1f/amoA-2f, FGPS872f/FGPS1269r and NSR1113f/NSR1264r (Park et al., 2010; Degrange and Bardin, 1995; Geets et al., 2007). Each PCR amplification mixture (20  $\mu$ L) consisted of 10  $\mu$ L SYBR® Premix Ex Taq™ (Takara, Dalian, China), 0.4  $\mu$ L ROX Reference Dye50, 1  $\mu$ L bovine serum albumin (25 mg/mL), 0.2  $\mu$ L of each primer (10  $\mu$ mol/L) and a 2  $\mu$ L template of DNA (1–10 ng). The PCR amplification program performed denaturation for 3 min at 96°C followed by 40 cycles of

**Table 1 – List of primers.**

Target	Primer name	Sequence (5'-3')	Temp. (°C)
AOB	amoA-1f/amoA-2r	gggtttctactggtggt/ccctckgsgaaagccttcttc	53
<i>Nitrobacter</i>	FGPS872f/FGPS1269r	ctaaaactcaaaggaattga/tttttgagattgctag	56
<i>Nitrospira</i>	NSR1113f/NSR1264r	cctgcttcagttgctaccg/gtttgacgagcgtttgaccg	53
	EUB338f/Ntspa0685M	actcctacgggagcagc/cggaattcccgcgctc	53

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