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Comparison study of phosphorus adsorption on different waste solids: Fly ash, red mud and ferric–alum water treatment residues

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ABSTRACT

The adsorption of phosphorus (P) onto three industrial solid wastes (fly ash, red mud and ferric-alum water treatment residual (FAR)) and their modified materials was studied systematically via batch experiments. Compared with two natural adsorbents (zeolite and diatomite), three solid wastes possessed a higher adsorption capacity for P because of the higher Fe, Al and Ca contents. After modification (i.e., the fly ash and red mud modified by FeCl₃ and FARs modified by HCl), the adsorption capacity increased, especially for the modified red mud, where more Fe bonded P was observed. The P adsorption kinetics can be satisfactorily fitted using the pseudo-second-order model. The Langmuir model can describe well the P adsorption on all of the samples in our study. pH and dissolved organic matter (DOM) are two important factors for P adsorption. Under neutral conditions, the maximum adsorption amount on the modified materials was observed. With the deviation from pH 7, the adsorption amount decreased, which resulted from the change of P species in water and surface charges of the adsorbents. The DOM in water can promote P adsorption, which may be due to the promotion effects of humic-Fe(Al) complexes and the pH buffer function exceeds the depression of competitive adsorption.

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45 Introduction

Excess phosphorus (P) in a water body can cause eutrophication 46 47 and significant environmental problems to water resources (Lürling et al., 2014; Paerl et al., 2011). The enhancement of P 48 removal in waste effluents before their discharge into the 49environment is thus of considerable significance. Presently, 50various techniques have been successfully applied for P remov-51al, such as physical (e.g., adsorption, and filtration), chemical 52(e.g., chemical precipitation and ion exchange), and biological 53(e.g., plant uptake and microbial degradation) techniques. 54

Among these techniques, adsorption is one of the most 55 attractive approaches, with the advantages of operation sim- 56 plicity, low operation cost and ability to provide effective 57 removal without yielding harmful by-products. 58

Many types of adsorbents for phosphate removal have 59 been investigated that are mainly divided into two types: 60 industrial solid wastes (Cao et al., 2013; Castaldi et al., 2010; 61 Liu et al., 2007; Wang et al., 2011) (fly ash, red mud, ferric–alum 62 residuals, etc.) and natural/synthetic mineral materials 63 (Borggaard et al., 2005; Huang et al., 2009; Wang and Peng, 64 2010; Xiong and Peng, 2008) (zeolites, diatomite, aluminum 65

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oxides, iron, iron oxides, etc.). Every year, the enormous 66 quantity of industrial solid wastes generated from power 67 plants, mineral extraction, and so on contributes to very 68 serious and alarming environmental problems. Some of these 69 solid wastes (such as fly ash, red mud, slag, and Fe/Al 70residual) have been demonstrated to have a remarkable 71 72 adsorption capacity for phosphate because these materials are enriched with oxides of aluminum, iron and calcium (Liu 73 74 et al., 2007; Wang et al., 2011). Therefore, even though some 75 natural/synthetic materials possess good P adsorption capacity (Huang et al., 2009; Liu et al., 2013; Xiong and Peng, 2008), 76 the use of the solid wastes for P adsorption is a more 77 promising suitable way for waste utilization. 78

The P adsorption capacities of solid wastes depend on both 79their properties (e.g., particles size, component and surface 80 characteristic) and the experimental conditions (e.g., tempera-81 ture, initial P concentration and pH) (Özacar, 2003; Wang et al., 82 2011). Some researchers found that solid wastes modified by 83 simple methods (such as thermal treatment, inorganic salt 84 treatment, and inorganic acid or alkali treatment) showed 85 higher P adsorption capacity. For example, fly ash was modified 86 by NaOH or HCl to change the surface characteristics. The P 87 adsorption capacity was found to decrease in the following 88 89 order: NaOH-fly ash > fly ash > HCl-fly ash (Pengthamkeerati 90 et al., 2008). In addition, the experimental conditions exhibited 91 an obvious influence on P adsorption. Earlier works demon-92strated that pH is the most important factor (Yan et al., 2010). In 93 addition, these earlier works demonstrated that Fe-Al residual has a high P adsorption capacity in the pH range of 3.6 to 5.6 94 (Wang et al., 2011). Also, natural organic matters in water bodies 95have an influence on the P adsorption (Lürling et al., 2014). 96 Those studies revealed that dissolved organic matter (DOM) can 03 compete with P for the adsorption sites and thus decrease the P 98 adsorption (Lürling et al., 2014; Weng et al., 2012). 99

The objective of this study was to investigate the P adsorption characteristics on three industrial solid wastes (fly ash, red mud and ferric-alum water treatment residuals (FARs)) and their modified materials. Their capacity was also compared to two typical natural materials (i.e., zeolite and diatomite). The effects of pH and DOM on the P adsorption were also elucidated.

108 1. Materials and methods

109 **1.1. Materials**

Samples of fly ash, red mud, and FARs were provided by
Beijing Shougang Iron Works, Aluminum Corporation of
China Limited Shandong branch, and the 9th Water Supply
Plant of Beijing, China, respectively. Zeolite and diatomite
were purchased from Sinopharm, China. All of the chemical
reagents used were analytically pure.

A total of 5 g of the sample of FARs were placed into HCl solution of 2 mol/L. After being shaken for 12 hr, the mixture was centrifuged to obtain the precipitate. Next, the solution was washed using deionized water many times until the solution was neutral. The sample was then dried at 105°C for 3 hr.

Five-gram samples of fly ash or red mud were placed into 500 mL of deionized water, and then, the pH value was adjusted to 13. Subsequently, a 0.5 mol/L of FeCl₃ solution was dropped 123 into the mixture slowly with continual stirring until the solution 124 pH decreased to 5. After precipitating for 24 hr, the residue 125 remaining after centrifuging was dried at 105°C for 3 hr. Next, 126 the residue was grinded and passed through a 100-mesh sieve. 127

1.2. Methods

1.2.1. Adsorption capacity for phosphorus

All of the adsorptive tests in this work were performed in a 130 shaker at $30 \pm 1^{\circ}$ C. Two drops of 0.1% chloroform were added 131 to inhibit the bacterial activity. 132

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The characteristics of the adsorption kinetics of P were 133 obtained by mixing 0.20 g samples (red mud, fly ash, zeolite 134 and diatomite) and 25 mL of solution with an initial phos-135 phate ion concentration of 100 mg/L. Because the P adsorp-136 tion capacity of the other materials was considerably higher, 137 the P solution volume was increased to achieve equilibrium. 138 For FARs, modified FARs (m-FARs), modified fly ash (m-fly 139 ash) and modified red mud (m-red mud), the P solution 140 volume was 100 mL. The samples were collected at different 141 time intervals and at different concentrations.

Three kinetic models were used to analyze the experimen-143tal data: pseudo-first-order (Eq. (1)), pseudo-second-order (Eq. 144144(2)), and a double-constant rate equation (Eq. (3)).145

$$\ln(Q_e - Q_t) = \ln Q_e - k_1 t \tag{1}$$

$$\frac{t}{Q_t} = \frac{1}{k_2 Q_e^2} + \frac{t}{Q_e}$$
(2)

$$\ln Q_t = a + b \ln t \tag{3}$$

where, Q_e (mg/g) is the P adsorption capacity at equilibrium; Q_t 150 (mg/g) is the P adsorption capacity at time t; k_1 and k_2 (hr⁻¹ and 152 kg/(kg·hr)) are the rate constants of Eqs. (1) and (2), respectively; 153 t (hr) is the reaction time; and *a* and *b* are the kinetic constants. 154

To study adsorption equilibrium, adsorption isotherms were 155 obtained as follows. Briefly ash, 0.20 g of each of the samples (red 156 mud, fly ash, zeolite and diatomite) was added in a series of 157 25 mL solutions with initial phosphate ion concentrations of 0, 158 30, 60, 100, 120, 150 and 300 mg/L. Because the phosphate 159 adsorption capacity of the other materials was considerably 160 higher, the initial phosphate ion concentration was increased to 161 reach saturation, and then, the maximum adsorption capacity 162 was calculated. For FARs, the initial phosphate ion concentra- 163 tions were 100, 150, 300, 450, 600, 750 and 1000 mg/L. For the 164 three modified materials, the initial phosphate ion concentra- 165 tions were 100, 300, 600, 750, 1500 and 3000 mg/L. After achieving 166 equilibrium via 48 hr of processing in a shaker, the solutions 167 were centrifuged at 5000 r/min for 20 min, and then, the 168 supernatants were used for phosphate analysis. The phosphate 169 adsorbed on the samples was calculated using the difference 170 between the initial and the equilibrium concentrations. 171

The results were fitted to Langmuir (Eq. (4)) and Freundlich 172 (Eq. (5)) isotherm models. Where Q_m (mg/g) is the monolayer 173 capacity of the sorbent and K, K_F and n are constants. 174

$$Q_e = \frac{KQ_mC_e}{1 + KC_e^n}$$

(4)

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