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## A new approach to the dynamics of oxygen capture by the human lung



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#### ABSTRACT

Oxygen capture in the lung results from the intimate dynamic interaction *between* the space- and time-dependent oxygen partial pressure that results from convection-diffusion and oxygen extraction from the alveolar gas *and* the space and time dependence of oxygen trapping by the red blood cells flowing in the capillaries. The complexity of the problem can, however, be reduced due to the fact that the systems obey different time scales: seconds for the gas phase transport and tenths of seconds for oxygen trapping by blood. This results first from a dynamical study of gas transport in a moving acinus and second from a new theory of dynamic oxygen trapping in the capillaries. The global solution can be found only through a self-consistent iterative approach linking the two systems. This has been accomplished and used to quantify oxygen capture in various situations: at rest, during exercise, ventilation–perfusion mismatching, high altitude and pulmonary edema.

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#### 1. Introduction

The scientific understanding of oxygen capture has changed over time based on the conceptual and experimental tools that were available (West, 2004). Now, numerical tools exist that allow us to investigate the dynamic nature of oxygen capture in an unsteady realistic environment and complex geometry. Thus, herein a theory is presented that takes into account the complexity of the lung morphology, and the dynamics of respiration and oxygen trapping. It will be shown that because of the different characteristic time scales of oxygen transport in gas and blood, it is possible to study both separately although oxygen capture finally depends on their complex interaction.

In earlier studies, the possible non-uniformity of the oxygen concentration (also called incomplete gas mixing or stratification, Scheid and Piiper, 1980) was related to the finite diffusivity of oxygen (Dutrieue et al., 2000; Felici et al., 2003, 2005; Grebenkov et al., 2005; Hou et al., 2010; Mayo et al., 2012; Paiva and Engel, 1985, 1987; Sapoval et al., 2002a, b; Swan and Tawhai, 2011; Tawhai and Hunter, 2001; Weibel et al., 1981, 2005). To study the system from the gas point of view, we developed the concept of a "machine acinus" (Foucquier et al., 2013). This machine

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has realistic morphology and dynamics (Haefeli-Bleuer and Weibel, 1988; Weibel, 1984) but with an unknown permeability  $\Omega$ , hereafter called the "integrative permeability". We suppose that in the artificial machine, blood acts as a *perfect sink*. The development determines the  $\Omega$  values that give the same oxygen capture as the real acinus does under an oxygen partial pressure of approximately 100 mmHg.

Of course, saturation does really intervene and we show, by studying the *blood* point of view, how saturation evolves in time allowing us to determine the value of  $\Omega$ . Our results are different from those derived from the conventional approach which uses, for oxygen, the formalism introduced by Roughton and Forster (1957) for the carbon monoxide case. This difference comes from the previous misinterpretation of the time scales involved in the establishment of dissolution.

Respiration results from the complex interaction between gas dynamics and blood saturation depending on the distribution of oxygen partial pressure. It is then only by combining the gas and blood approaches in a self-consistent manner that we are able to build a quantitative theory of oxygen capture with no adjustable parameters. This general approach can be applied to the quantification of many situations such as ventilation–perfusion heterogeneity, respiratory response to altitude, the existence of a respiratory reserve and a decrease of arterial oxygen partial pressure in pulmonary edema.

The theory for oxygen capture by blood can be also applied to other gases. Herein we consider the diagnostic and

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а	radius of a red blood cell
$C_{\rm E}$	oxygen concentration on the external surface of a
	red blood cell
$C_{ m g}$	local oxygen concentration in gas
$C_{\rm p}$	oxygen concentration in the internal fluid assimi-
	lated with plasma
$C_{\text{RBC}}$	oxygen concentration in a red blood cell
$C_{\rm S}$	oxygen concentration in air at sea level
Cv	oxygen concentration in mixed venous blood
D	diffusion coefficient of oxygen in air
$D_{\mathrm{O}_2}$	diffusion coefficient of oxygen in plasma
$D_{\text{CO}}$	diffusion coefficient of carbon monoxide in plasma
$D_{ m NO}$	diffusion coefficient of nitric oxide in plasma
$DL_{O_2}$	diffusing capacity of the lung for oxygen
$DL_{CO}$	diffusing capacity of the lung for carbon monoxide
DL <sub>NO</sub> Hb	diffusing capacity of the lung for nitric oxide
нь Hct	hemoglobin molecule hematocrit
ни k <sub>CO</sub>	rate constant for carbon monoxide uptake
$k_{\rm NO}$	rate constant for nitric oxide uptake
$N_{\rm ac}$	number of acini in the lung
N <sub>Hb</sub>	number of Hb molecules per red blood cell
$N_{\rm NO}$	number of nitric oxide molecules leaving the alveo-
1.110	lar volume
NRRCLung	number of red blood cells in the lung
n	exponent of the Hill equation
$P_{A}$	average alveolar oxygen partial pressure
$P_{a}$	oxygen partial pressure of the arterial blood
${P_{b}}^*$	barometric pressure
$P_{\mathrm{I}}$	inspired oxygen partial pressure
$P_{ m g}$	local alveolar oxygen partial pressure
$P_{p}$	oxygen partial pressure in plasma
$P_{V}$	oxygen partial pressure of the mixed venous blood
$P_{50}$	P <sub>p</sub> at 50% saturation
RBC	red blood cell
Q S	cardiac output gas exchange surface area
	total lung surface area
S <sub>Lung</sub> Sat	oxygen saturation fraction of hemoglobin molecules
STP	standard temperature and pressure
T	duration of a respiratory cycle
t	time coordinate for gas during the respiratory cycle
$t_{\mathrm{B}}$	time coordinate for oxygen trapping dynamics by
ъ	blood
$t_{\rm c}$	capillary transit time
$t_{\rm s}$	saturation time for blood
U	gas convection velocity in airways
V	volume of an acinar branch
$V_{A}$	alveolar volume
$V_{\rm ac}$	volume of an acinus
$V_{\rm c}$	pulmonary capillary volume
$V_{\mathrm{p}}$	plasma volume per red blood cell
$V_{ m RBC}$	volume of a red blood cell
V V	ventilation the amount of evergen untake of the lung
$\dot{V}_{\mathrm{O}_2}$	the amount of oxygen uptake of the lung position in airways
$\alpha$	liquid to gas partition ratio for oxygen
$\alpha_{\mathrm{CO}}$	liquid to gas partition ratio for carbon monoxide
$\alpha_{ m NO}$	liquid to gas partition ratio for nitric oxide
$\alpha'$	partition ratio of oxygen concentration between
	plasma and red blood cell
$lpha'_{CO}$	partition ratio of carbon monoxide concentration
20	hetween plasma and red blood cell

between plasma and red blood cell

partition ratio of nitric oxide concentration between
plasma and red blood cell
characteristic time for oxygen diffusion from alveo-
lar space to the red blood cell surface
characteristic time for carbon monoxide diffusion
from alveolar space to the red blood cell surface
characteristic time for nitric oxide diffusion from
alveolar space to the red blood cell surface
characteristic time for oxygen trapping by
hemoglobin molecules
characteristic time for carbon monoxide trapping by
hemoglobin molecules
characteristic time for nitric oxide trapping by
hemoglobin molecules
· · · · · · · · · · · · · · · · · · ·
equivalent diffusion barrier thickness
oxygen flux across the gas exchange surface
instantaneous oxygen flux per red blood cell
integrative permeability
integrative permeability in physiological units
$(ml_{STP} cm^{-2} min^{-1} mmHg^{-1})$

therapeutic gases carbon monoxide (CO) and nitric oxide (NO). Thus, we propose a quantitative approach to determine the diffusing capacity of the lung for these gases,  $DL_{CO}$  and  $DL_{NO}$ . It is found that oxygen capture, although controlled by the same type of equations, is fundamentally different from CO or NO capture.

#### 2. Methods

## 2.1. The gas phase transport: the machine acinus at rest and during exercise

If the oxygen  $(O_2)$  concentration is non-uniform, the differential oxygen flux across an element of the alveolar surface dS at position x and time t can be expressed by

$$d\Phi = \Omega \left( C_{\rm g}(x,t) - \frac{C_{\rm v}}{\alpha} \right) dS \tag{1}$$

where  $C_g(x,t)$  is the local  $O_2$  concentration,  $C_v$  is the mixed venous O2 concentration in blood plasma (assumed to be constant during a breathing cycle) and  $\alpha$  is the Ostwald partition ratio (dimensionless ratio of concentration in liquid to concentration in gas at equilibrium, 0.024 for oxygen in water and air). Units of flux are molecules/time and  $\Omega$  is expressed in units of length/time or velocity. Note that the usual physiological units in terms of partial pressures obscure the fact that the permeability really measures an average molecular velocity that is explicit in this formulation. Permeability is usually measured in standard physiological units such as volume per unit surface per unit time per partial pressure (for instance ml<sub>STP</sub> cm<sup>-2</sup> min<sup>-1</sup> mmHg<sup>-1</sup>; where STP refers to standard temperature and pressure). Here we use the equivalent physical units, length divided by time or velocity units, to emphasize that the permeability is a measure of average molecule velocity. The equivalence between the physical and the physiological units of permeability is then given by  $\Omega$  (cm s<sup>-1</sup>) = 12.7 ×  $\Omega$ <sub>physiol</sub>  $(ml_{STP} cm^{-2} min^{-1} mmHg^{-1}).$ 

The  $O_2$  concentration is space- and time-dependent because it is governed by convection, diffusion and permeation across the peripheral surface. Assuming that the transverse diffusion time across the acinar duct is negligible compared to the stream-wise transport during the respiratory cycle, the 1D convection-diffusion-permeation equation can be used to

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