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## Experimental research on the relationship between fit accuracy and fracture resistance of zirconia abutments

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## ABSTRACT

*Objective:* The purpose of the study was to investigate the correlation between fit accuracy and fracture resistance of zirconia abutments, as well as their feasibility for clinical applications.

Methods: Twenty self-made zirconia abutments were tested with 30 Osstem GSII implants. Firstly, 10 Osstem GSII implants were cut into two parts along the long axis and assembled with the zirconia abutments. The microgaps between the implants and the zirconia abutments were measured under scanning electron microscope. Secondly, the zirconia abutments were assembled with 20 un-cut implants and photographed before and after being fixed with a central screw of 30-N cm torque. The dental films were measured by Digora for windows 2.6 software. Then the fracture resistance of zirconia abutments were measured using the universal testing machine at 90°. All results were analyzed using SPSS 13.0 software.

Results: The average internal-hexagon microgaps between the implants and zirconia abutments were  $19.38 \pm 1.34 \mu m$ ; The average Morse taper microgap in the implant-abutment interface was  $17.55 \pm 1.68 \mu m$ ; The dental film showed that the Morse taper gap in the implant-abutment interface disappeared after being fixed with a central screw of 30-N cm torque and the average moving distance of the zirconia abutments to the implants was  $0.19 \pm 0.02 \text{ mm}$ ; The average fracture resistance of zirconia abutments was  $282.93 \pm 17.28 \text{ N}$ ; The internal-hexagon microgap between the implants and zirconia abutments was negatively related to the fracture resistance of the abutments ( $r_1 = -0.97$ , p < 0.01); The Morse taper microgap in the implant-abutment interface was negatively related to the fracture resistance of the abutments ( $r_2 = -0.84$ , p < 0.01).

Conclusion: The microgap between implant and abutment was negatively related to the fracture resistance of the abutment. While the internal-hexagon microgap has better correlation than the Morse taper microgap. The fracture resistance of zirconia abutments can satisfy the clinical application.

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#### 15 1. Introduction

17 With the increasing of living standards and aesthetic demand, the implant dentures in anterior area are more than a biological 18 19 requirement. The conventional and widely used titanium abutment shows undesirable metal colour through thin gingival 20 tissue. In recent years, due to its perfect aesthetic effect, 21 22 excellent biological and mechanical performance, zirconia 23 abutment has become a research focus. Our previous study 24 has found that zirconia abutments fabricated with injection 25 moulding technique showed sufficient resistance required for 26 the clinical application under loadings with different angles.<sup>1</sup> 27 The existence of microgap between implant and abutment has 28 been described in many studies. Microgap could be colonized by 29 bacteria, which may influence the remodelling of the periimplant bone and the long-term health of the peri-implant 30 tissues. In the present study, zirconia abutments were made 31 32 with injection moulding technique. The microgaps between the zirconia abutments and the titanium implants were measured 33 34 under scanning electron microscope. The changes of joint interface between the zirconia abutments and the implants 35 before and after the central screw fixation were observed with 36 37 dental film. The fracture resistance of the zirconia abutments 38 were measured with Universal Test Machine. The relationship between fit accuracy and fracture resistance of the zirconia 39 abutments was analyzed. 40

#### 2. Materials and methods

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#### 2.1. Materials and instruments

43 Zirconiapowder(TZ-3YB-E)waspurchasedfromTosohCompany (Japan). Thirty titanium implant were from Osstem Implant 45 Company (Osstem GS II system, 4.5 mm × 10 mm, Korea). Other equipments included laser three dimensional gage (LPX-250, 46 Japan), banbury mixer (XSN-15, Giding Co., Ltd., Taichung City, 48 Taiwan), injection shaper (XSN-15, Shapers' Deutschland GmbH, 49 Gladenbach, Germany), sintering apparatus (KSX-5-14, ChangZ-50 hou Xing Guang Kilns Co., Ltd., Jiangsu, China), mill (XSM-LC,

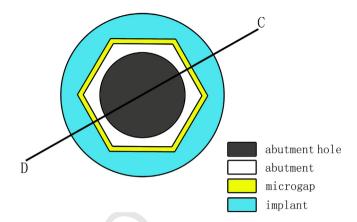


Fig. 2 - The cross section of internal-hexagon in abutmentimplant interface.

Beijing, China), universal test machine (AGS-J, Japan), and intraoral dental X-ray (FIN-00031 SOREDEX, Finland).

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#### 2.2. Zirconia abutment fabrication

The fabrication of zirconia abutment was described as in Yang et al. Briefly, three dimensional scanning on the titanium abutment and the connecting portion with the implant (the portion of hexagon and Morse taper) was measured by laser gauge. The zirconia abutment draft was drawn according to the liner shrinkage of zirconia materials. The abutments were fabricated following the procedures (including mixing, injection moulding, degreasing, sintering, and refinement, Fig. 1).

### 2.3. Analysis of adaptation at implant-abutment and interface

The interface adaptation was assessed by calculating the microgap between the zirconia abutment and the tititum implant, as shown in Figs. 2 and 3. Ten implants (Osstem-GS II) were randomly selected and fixed to the self-made zirconia abutments, which then were placed on a test stand of wire cut electrical discharge machining (Fig. 4). The cutting wires were



### Fig. 1 - The side view and bottom view of zirconia abutment.

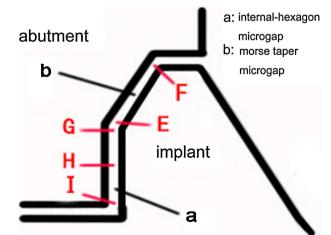


Fig. 3 – The diagram of microgap between zirconia abutment and tititum implant.

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