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# Reaction mechanism of direct  $H_2O_2$  synthesis from  $H_2$  and  $O_2$  over Pd/C catalyst in water with  $H^+$  and  $Br^-$  ions

# Takashi Deguchi, Masakazu Iwamoto  $*$

Chemical Resources Laboratory, Tokyo Institute of Technology, 4259-R1-5 Nagatsuta, Midori-ku, Yokohama 226-8503, Japan

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#### 1. Introduction

Many efforts have been devoted to catalytic synthesis of  $H_2O_2$  in water from  $H_2$  and  $O_2$  since it is a clean oxidizing agent and will lead a simple manufacturing process. Most of studies were carried out on Pd catalysts, and Au was also investigated in the form of alloy with Pd as reviewed in literatures [\[1–3\]](#page--1-0). Recently, Pd or Au–Pd nano-particle catalysts were intensively studied by several research groups [\[4–10\]](#page--1-0). The Pd catalyst was usually combined with proton and halide ions such as  $Cl^-$  or  $Br^-$ .

The synthesis reaction is widely recognized to consist of  $H_2O_2$ formation, direct  $H_2O$  formation, and subsequent decomposition and hydrogenation of  $H_2O_2$  produced as shown in [Scheme 1,](#page-1-0) in which  $r_f$ ,  $r_c$ ,  $r_{d1}$ , and  $r_{d2}$  represent the respective reaction rates. However, the detailed reaction mechanisms including the intermediates and the role of each component were still under debate [\[1–3,11–25\]](#page--1-0). It is widely accepted that proton and halide ions accelerate the  $H_2O_2$  formation and depress the unfavorable side reactions. Liu and Lunsford claimed that H<sup>+</sup> possessed two roles that it reacted with an active form of oxygen to produce  $H_2O_2$ and changed the electronic state of Pd surface to facilitate  $H_2O_2$ formation  $[11]$ . The similar interaction between  $H^+$  and adsorbed

#### **ABSTRACT**

Kinetic analyses including mass transfer processes were applied for the title reaction and the  $H_2O_2$ decomposition. Adsorption of Br<sup>-</sup> ion on the catalyst was also measured. A hydride-hydroperoxy species H-M-OOH (M, the metal surface) was proposed as the key intermediate in the  $H_2O_2$  formation, the direct  $H_2O$  formation, and the  $H_2O_2$  decomposition. The H<sup>+</sup> added would accelerate Br<sup>-</sup> adsorption, reductive elimination and  $\beta$ -elimination of the H-M-OOH species, and desorption of surface H<sub>2</sub>O<sub>2</sub> species. Two types of metal surface sites were suggested, one of which had a high degree of coordinative unsaturation and catalyzed the direct  $H_2O$  formation and the  $H_2O_2$  decomposition. Both reactions would be inhibited by adsorption of the  $Br^-$  and  $H^+$  pairs. Another had a low degree of unsaturation and was active for the H<sub>2</sub>O<sub>2</sub> formation. Sulfur poisoning study revealed that several surface Pd atoms were inactivated at once by adsorption of a sulfur atom for  $H_2-O_2$  reaction.

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 $O<sub>2</sub>$  was suggested by the others [\[12\]](#page--1-0). The adsorption of Cl<sup>-</sup> or Br<sup>-</sup> on Pd was confirmed by EDAX and XPS after the  $H_2-O_2$  reaction and was suggested to inhibit homolytic cleavage of  $O$ —O bond of  $O<sub>2</sub>$  and  $H<sub>2</sub>O<sub>2</sub>$  through blocking catalytic sites [\[13–15\]](#page--1-0). The H<sup>+</sup> was reported to enhance the adsorption of halide ions by lowering the pH below the isoelectric point of support and to inhibit the  $H<sub>2</sub>O<sub>2</sub>$  adsorption on the catalyst [\[13\]](#page--1-0). On the other hand, the dissociative adsorption of  $O_2$  and  $H_2O_2$  was suggested to proceed on more energetic Pd sites (defects, edges, corners, etc.), and they would be blocked by Br<sup>-</sup> to result in improved selectivity [\[16\].](#page--1-0) Br<sup>-</sup> was also proposed to act as an electron scavenger and inhibit radical-type decomposition [\[16\].](#page--1-0)

Many kinds of reaction mechanisms and the roles of additives were suggested as described above. To reach more clear understanding of them, sufficient kinetic studies should be carried out. One of the reasons for difficulties of the kinetic analyses of  $H<sub>2</sub>O<sub>2</sub>$  synthesis was the transportation limitation of the reaction gases in water [\[1\]](#page--1-0). Liu and Lunsford therefore carried out the kinetic studies in ethanol which shows higher solubility of the gasses [\[11\]](#page--1-0). Voloshin et al. studied them by using a micro-reactor since the reaction in the reactor was generally unrestricted from mass transfer limitation [\[17,18\].](#page--1-0) In spite of these previous studies, it would be desirable to establish a method of kinetic analysis that was applicable to batch-wise reactions with less assumption. Another reason for the difficulties of kinetic studies was the

<sup>⇑</sup> Corresponding author. Fax: +81 45 924 5228.

E-mail address: [Iwamoto@res.titech.ac.jp](mailto:Iwamoto@res.titech.ac.jp) (M. Iwamoto).

<span id="page-1-0"></span>

**Scheme 1.** Suggested reaction routes in the direct  $H_2O_2$  synthesis.

complicated reaction routes as shown in Scheme 1. It was not easy to determine the individual reaction rates on the basis of kinetics measurements [\[3\].](#page--1-0)

We reported a systematic rate analysis method that included the mass transfer processes of gasses and distinguished the respective rates of concurrent and consecutive reactions [\[26\]](#page--1-0). This method could be successfully applied to the  $H_2O_2$  synthesis from  $H_2$  and  $O_2$  in water on Pd/C catalyst with H<sup>+</sup> and Br<sup>-</sup> ions. Reaction rate of  $H_2(r_0)$  and  $H_2O_2$  accumulation rate were expressed by Eqs. (1) and (2). Assuming that  $r_{d1}$  and  $r_{d2}$  were expressed by Eqs. (3) and (4), in which  $k_{d1}$  and  $k_{d2}$  were the rate constants, and that  $H_2O_2$  formation selectivity ( $S_f$ , defined by Eq. (5)) and overall  $H_2O_2$  destruction rate constant ( $k_d$ , defined by Eq. (6)) were constant, Eq. (7) was derived. Here,  $[H_2O_2]$  and [Cat] were the concentrations of  $H_2O_2$  and catalyst, and  $k_{d1}$  and  $k_{d2}$  included the terms of partial pressures of  $H_2$  $(p_{H2})$  and  $O_2$  ( $p_{O2}$ ). S<sub>f</sub> and  $k_d$  could be determined from the time course of  $[H_2O_2]$  based on Eq. (7). The detailed calculation method was described in the previous paper [\[26\]](#page--1-0).

$$
r_0 = r_f + r_c + r_{d2} \tag{1}
$$

$$
d[H_2O_2]/dt = r_f - r_{d1} - r_{d2}
$$
 (2)

$$
r_{d1} = k_{d1} [H_2 O_2] [Cat]
$$
 (3)

$$
r_{d2} = k_{d2} [H_2 O_2] [Cat]
$$
 (4)

$$
S_f = r_f/(r_f + r_c) \tag{5}
$$

$$
k_d = k_{d1} + (1 + S_f)k_{d2}
$$
 (6)

$$
d[H_2O_2]/dt = r_0S_f - k_d[H_2O_2][Cat]
$$
 (7)

On the other hand, defining an apparent rate constant  $(k_{0a})$  as Eq. (8), the relation of  $k_{0a}$  with the overall mass transfer coefficient  $(k<sub>L</sub>a)$  was expressed by Eq. (9), in which  $k<sub>0</sub>$  and H were the intrinsic rate constant independent of mass transfer rate of  $H_2$  and the Henry's law constant of  $H_2$ , respectively [\[26\].](#page--1-0) Mass transfer rate of  $O<sub>2</sub>$  was regarded as sufficiently large because of much higher  $p_{O2}$  than  $p_{H2}$ . When the value of  $k<sub>L</sub>a$  of the reaction system is known, one can calculate  $k_0$  from  $k_{0a}$  by Eq. (9). In the previous study,  $k_0$  depended on  $p_{H2}$  and was not a constant in a strict sense, but it is useful as the index in the comparison of the catalytic activities [\[26\].](#page--1-0)

$$
r_0 = k_{0a} p_{H2} [\text{Cat}] \tag{8}
$$

$$
1/k_{0a} = 1/k_0 + [Cat]/(k_{L}a/H)
$$
\n(9)

In the previous paper [\[26\]](#page--1-0), the  $H_2$  and  $O_2$  partial pressure dependencies were analyzed by the above method, and also the progress in reaction was simulated based on them. In this study, we investigated the influence of H<sup>+</sup> and Br<sup>-</sup> ions, the kinetics of  $H_2O_2$  decomposition, and the adsorption behaviors of Br<sup>-</sup> on Pd to discuss the whole catalytic reaction mechanism.

# 2. Experimental

#### 2.1.  $H_2O_2$  synthesis

The  $H_2-O_2$  reaction was carried out in a 300-ml glass flask equipped with a magnetic stirrer, a gas baffle, a gas feeding nozzle, a liquid sampling nozzle, and a thermometer. A football-shaped stirring rotor of 20 mm in diameter and 45 mm in length was used to agitate the aqueous suspension and increase gas dispersion. To avoid ignition by static electricity, all apparatus except for the reactor was made of stainless steel tube of 1 mm inner diameter. The dead volume in the reactor was minimized, and the glass plug was put in the reactor as a safety valve. Pd/C catalyst with 5 wt.% Pd (AER type suitable to hydrogenation of nitro compounds, the average particle size of ca. 20  $\mu$ m) was provided by NE Chemcat Company, Japan and used for the experiments as received. All gases were of industrial grades, and respective flow rates were controlled by mass flow controllers. All experiments were carried out at an atmospheric pressure.

A selected amount of the Pd/C catalyst was introduced in a calculated amount of water in the flask and activated by supplying  $H_2$ (20 Ncm<sup>3</sup> min<sup>-1</sup>) in an aqueous suspension at 30 °C for 1 h. Subsequently,  $N_2$  gas was introduced to displace the  $H_2$  gas, and the additive(s) was supplied in the form of an aqueous solution. Unless otherwise stated,  $H_2SO_4$  was employed as the  $H^+$  source and NaBr as the Br<sup>-</sup> source. When the effects of  $H^+$  and Br<sup>-</sup> ions were studied, Na<sub>2</sub>SO<sub>4</sub> was added to regulate the concentration of  $[SO_4^{2-}]$  species to 0.01 N. Finally, the volume of solution was adjusted at 300 ml. After the sufficient displacement with  $N_2$ , the mixture of  $H_2$ , O<sub>2</sub>, and N<sub>2</sub> gases was flowed at a constant rate into the reactor through the nozzle. The composition of supplied gases was determined by gas chromatography in advance. The gas flow rate and the gas composition at the reactor outlet were measured every 30 min to determine the  $H_2$  consumption rate and the partial pressure of each gas. A small part of the suspension was picked out at the same time through the nozzle, and the  $H_2O_2$  concentration was analyzed by a UV–Vis absorption method using a titanium sulfate solution. It was confirmed in separated experiments that no further reaction proceeded in the collected solution after mixed with the titanium sulfate solution.

The reaction temperature was usually 30 $\degree$ C, and the agitation rate was 1355 rpm in the standard experiments. The  $k_{\text{L}}a$  value in the experiments was measured by the method described in the previous paper [\[26\]](#page--1-0) and was 560  $h^{-1}$ .

### 2.2.  $H<sub>2</sub>O<sub>2</sub>$  decomposition

The reaction was carried out in a 100-ml glass flask. The suspension containing catalyst was undergone the same pretreatment as the above, and finally, the volume of solution was adjusted at 98 ml. Then, 2 ml of a 17 wt.%  $H_2O_2$  solution was added, and the H<sub>2</sub>O<sub>2</sub> concentration was periodically followed.

## 2.3. Br<sup>-</sup> adsorption

The catalyst was activated in the same manner as the above.  $N<sub>2</sub>$ was then introduced to displace  $H_2$ , mixture of  $O_2$  and  $N_2$  (1:9) gases was flowed for 10 min in order to eliminate possibly adsorbed hydrogen atoms, and finally,  $N_2$  was again introduced. The  $H<sub>2</sub>SO<sub>4</sub>$ , NaBr, and Na<sub>2</sub>SO<sub>4</sub> solutions of desired concentrations were added. The mixture was agitated at 30  $\degree$ C for 1 h. After the settlement of catalysts, the  $Br^-$  concentration in the solution was measured by ion chromatography.

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