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# Modelling the response of laboratory horizontal flow constructed wetlands to unsteady organic loads with HYDRUS-CWM1



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#### a r t i c l e i n f o

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## A B S T R A C T

Although horizontal flow constructed wetlands (HF CWs) are usually subjected to unsteady loads in real application,the modelling of HF CWresponse to time-variable loads has been scarcely studied in literature yet. The aim of this study is to test the capability of HYDRUS-CWM1 to simulate the behavior of HF CWs subjected to unsteady loads. Hence, we applied HYDRUS-CWM1 to simulate laboratory results of HF CWs subjected to variable COD inflows. The modelling results adequately fit the experimental data, with an almost perfect agreement in global COD removal efficiencies (67 and 68% from laboratory experiments and simulations, respectively), and mean percent error equal to 20 and 31% for effluent COD and NH $^+_4$ concentrations, respectively. The obtained results suggest that HYDRUS-CWM1 can be a powerful tool to simulate the response of HF CWs under time-variable loads. Additionally, more detailed data are shown to be crucial in order to better exploit process-based model tools.

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# **1. Introduction**

Constructed wetlands (CWs) are a wastewater treatment technology that exploits the physical, chemical, and biological processes occurring in soils to improve water quality [\(Kadlec](#page--1-0) [and](#page--1-0) [Wallace,](#page--1-0) [2009\).](#page--1-0) The low operation and maintenance costs allow for a widespread use of CWs, especially for treating wastewater from small communities [\(Haberl](#page--1-0) et [al.,](#page--1-0) [2003;](#page--1-0) [Kadlec](#page--1-0) [and](#page--1-0) [Wallace,](#page--1-0) [2009\).](#page--1-0)

Horizontal subsurface flow (HF) is a common CW type to treat organic loads [\(Kadlec](#page--1-0) [and](#page--1-0) [Wallace,](#page--1-0) [2009;](#page--1-0) [Abou-Elela](#page--1-0) et [al.,](#page--1-0) [2013\).](#page--1-0) In HF CWs, wastewater flows horizontally beneath the soil surface and from the inlet to the outlet of a gravel bed planted with wet-land vegetation ([Haberl](#page--1-0) et [al.,](#page--1-0) [2003;](#page--1-0) [Kadlec](#page--1-0) and Wallace, [2009\).](#page--1-0) Due to the reductive state developed, HF CWs are usually preferred to other CW types when anaerobic processes for treating wastewater are sufficient ([Kadlec](#page--1-0) [and](#page--1-0) [Wallace,](#page--1-0) [2009\).](#page--1-0) Moreover, HF CWs are also preferred to surface flow CWs for concerns about human contact with untreated wastewater, mosquito and odor control, and

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Process-based models are powerful tool to investigate the behavior of HF CWs, since they are able to separately simulate the effect of the different organic removal processes [\(Langergraber,](#page--1-0) [2008\).](#page--1-0) However, process-based models were typically used to investigate HF CWs subjected to steady state loads (e.g., [Llorens](#page--1-0) et [al.,](#page--1-0) [2011;](#page--1-0) [Samso](#page--1-0) [and](#page--1-0) [Garcia,](#page--1-0) [2013a\)](#page--1-0) and only recently they were started to be used for unsteady long-term simulations (e.g., [Samso](#page--1-0) [and](#page--1-0) [Garcia,](#page--1-0) [2013b\).](#page--1-0) Generally, little is known about the ability of process-based model to simulate the performance of HF CWs under unsteady loads.

The aim of the work is to test the capability of HYDRUS-CWM1 ([Langergraber](#page--1-0) [and](#page--1-0) Šimůnek, [20012\)](#page--1-0) to model the HF CW response to time-varying loads simulating the laboratory data collected by [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\).](#page--1-0)

# **2. Methods**

In this section the main features of experimental dataset and of the used process-based model are briefly exposed. For more details about data from laboratory HF CWs see [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\),](#page--1-0) while about HYDRUS-CWM1 see [Langergraber](#page--1-0) et [al.\(2009\),](#page--1-0) Simůnek et [al.](#page--1-0) [\(2011a\),](#page--1-0) and [Langergraber](#page--1-0) [and](#page--1-0) Šimůnek [\(2012\).](#page--1-0)





**Fig. 1.** Unsteady COD inflow concentrations. The squares and circles represent the measured data from [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)](#page--1-0) for group A and B, respectively. The continuous and dashed lines figure the inflow trend assumed in simulations for A and B, respectively.

#### 2.1. Experimental data

The data used to test the HYDRUS-CWM1 model were collected from laboratory experiments on six HF CWs set up at the Technical University of Lisbon in 2010 ([Galvão](#page--1-0) [and](#page--1-0) [Matos,](#page--1-0) [2012\).](#page--1-0) Each HF CW consisted of a gravel bed with length 1.1 m, width 0.76 m, and height 0.3 m. HF CWs were fed with an average hydraulic load of 10 l/d as follows: from Tuesday to Thursday 10 l/d; on Mondays and Fridays 20 l/d, to mimic the weekends (no feeding during Saturday and Sunday). A concentrated synthetic wastewater (i.e., no bacteria and no solids) was used with theoretical concentrations of COD and total nitrogen (TN) equal to 39 and 6 g/l, respectively. The synthetic wasterwater was composed with a mixture of urea, acetate, peptone, starch, powdered milk, and soy oil (for concentrations see [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)\).](#page--1-0) This solution was diluted to obtain the desired concentration to feed each bed. After an inoculation period, the six beds were divided in two groups, A and B, fed for 127 days with higher (A) and lower (B) average COD concentrations, respectively, as shown in Fig. 1. Each group was composed of three beds with different vegetation configurations: no plants, P. australis, and Scirpus. Water level was constantly maintained 5 cm below the surface. Since the HF CWs were situated inside laboratory, the resulting evaporation rates were very low (see [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)\)](#page--1-0) and are neglected in the present analysis.

The results from [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)](#page--1-0) have shown no significant role of plants, therefore the data from the three different beds per group are averaged in the present work. In this way, we obtain a single effluent value of COD and NH $_4^+$  with corresponding standard deviation per group, which is compared with results from modelling simulations.

## 2.2. HYDRUS-CWM1

The HYDRUS Wetland Module is an extension of the HYDRUS family codes, which allows for a detailed simulation of subsur-face flow CWs ([Langergraber](#page--1-0) [and](#page--1-0) Šimůnek, [20012\).](#page--1-0) HYDRUS solves systems of partial differential equations in three dimensions in order to simulate (Šimůnek et [al.,](#page--1-0) [2011a\):](#page--1-0) (i) variably-saturated water flow (Richards' equation); (ii) transport of constituents (mass balance equations); (iii) influence of plants (water and nutrient uptake, radial oxygen loss) and (iv) water temperature (heat transport equation). On this framework, the HYDRUS Wetland Module adds two different biokinetic models: CW2D for aerobic and anoxic processes, and CWM1 for aerobic, anoxic, and anaerobic transformations. Since HF CWs are principally anaerobic systems ([Kadlec](#page--1-0) [and](#page--1-0) [Wallace,](#page--1-0) [2009\),](#page--1-0) CWM1 was adopted in our simulations. For sake of simplicity, we refer to this option of HYDRUS Wetland Module as HYDRUS-CWM1.

The biokinetic model CWM1 ([Langergraber](#page--1-0) et [al.,](#page--1-0) [2009\)](#page--1-0) simulates the transformation of organic matter (expressed as chemical oxygen demand – COD), nitrogen (N), and sulfur (S) via biochemical transformation under aerobic, anoxic, and anaerobic conditions. The organic matter is considered via both soluble and particulate COD fractions, while microorganisms are considered as fixed particulate components. The soluble and particulate groups are referred as  $S_x$  and  $X_x$ , respectively, where x states the component acronym. A list of the components included in CWM1 and of the seventeen biogeochemical transformations considered in CWM1 are reported in Supplementary online material.

# 2.3. Model set-up

The HF CWs studied by [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)](#page--1-0) are modeled via a vertical 2D rectangular domain 1.1 m long, and 0.30 m high. In the soil hydraulic model, the van Genuchten–Mualem formulation is assumed for soil water retention and hydraulic conductivity  $(\check{\textrm{Sim}}$  [unek](#page--1-0) et [al.,](#page--1-0) [2011a\).](#page--1-0) For the solute transport model, the Millington and Quirck formulation is set for soil tortuosity, while a Langmuir law is considered for  $NH_4^+$  adsorption (Sim[unek](#page--1-0) et [al.,](#page--1-0) [2011a\).](#page--1-0)

Since the experiments of [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)](#page--1-0) did not show relevant difference between vegetated and unvegetated CWs, the plant effects (i.e. water and nutrient root uptake, radial oxygen loss) are not considered. The scarce role of plant can be explained in term of evapotraspiration rate. Differently from outdoor locations in which evapotranspiration plays an important role [\(Pedescoll](#page--1-0) et [al.,](#page--1-0) [2013\),](#page--1-0) very low evapotranspiration rates are reported for the indoor laboratory HF CWs studied by [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\).](#page--1-0) This confirms the scarce role of root water uptake in the hydrodynamics of [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)'s](#page--1-0) HF CWs. An additionally explanation can be related to root development. Indeed, [Galvão](#page--1-0) [and](#page--1-0) [Matos](#page--1-0) [\(2012\)](#page--1-0) have also mentioned no significant removal rates inside each group related to root compartment. This probably because the plants were very young, so the root system was not expected to be fully developed. For sake of simplicity, the influent  $O<sub>2</sub>$  is set equal to zero, in accordance with other studies dealing with modelling HF CWs (e.g., [Samso](#page--1-0) [and](#page--1-0) [Garcia,](#page--1-0) [2013a,b\).](#page--1-0) The sulfur cycle is not modelled for lack of measured data.

Since the influent wastewater is synthetic, typical COD fractionations for domestic wastewater proposed in literature (e.g., [Henze](#page--1-0) et [al.,](#page--1-0) [2000\)](#page--1-0) are not usable. Hence, the COD inflow concentration is fractionated in accordance with influent load composition as follows: 62% for S<sub>F</sub>, 10% for S<sub>A</sub>, 3% for S<sub>I</sub>, 20% for X<sub>S</sub>, and 5% for X<sub>I</sub>. Since  $NH<sub>4</sub><sup>+</sup>$  inflow was not monitored, an average ratio between  $\rm NH_4^+$  and COD inflow,  $\rm NH_4^+ / COD = 0.02$ , is used to estimate  $\rm NH_4^+$ inflow concentration.

Initial conditions are obtained simulating 10 days ofinoculation, with low initial component concentration and COD inflow concentrations equal to 1108 and 510 mg/l for group A and B, respectively.

The adopted boundary conditions have the following features: the inflow is modeled as distributed on the whole water depth; outflow is located in a single node at 1 cm from the bottom and set as constant pressure head in order to maintain the water table 5 cm below the top; the upper boundary is not covered, therefore the atmospheric  $O<sub>2</sub>$  is allowed to diffuse within CW; all other boundaries are assumed impermeable and with no solute fluxes. A graphical representation of boundary conditions is reported in Supplemental online material.

Only few parameters are modified from the default values reported in [Langergraber](#page--1-0) et [al.](#page--1-0) [\(2009\);](#page--1-0) their values are reported together with other set parameters in [Table](#page--1-0) 1. Note that the fractions of organic nitrogen are calibrated in order to guarantee the

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