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Oxygen-selective membranes integrated with oxy-fuel combustion

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ABSTRACT

The perovskite-type oxide $\text{SrCo}_{0.8}\text{Fe}_{0.2}\text{O}_{3-\delta}$ (SCF), a highly oxygen-permeable material, is restricted for application in the membrane-integrated oxy-fuel combustion process by its low tolerance to $CO₂$. In the present work, we found that the $CO₂$ tolerance of SCF is improved by increasing the oxygen partial pressure in the CO₂-containing gas. Long term oxygen permeation experiments, at 950 °C, show that mixing 5% of oxygen into the $CO₂$ sweep gas effectively prevents degradation of the SCF membrane. X-ray photoelectron spectroscopy indicates that the increase in $CO₂$ tolerance of SCF is caused by a decrease in basicity of the material with increasing oxygen partial pressure. Based on these experimental results, a modified oxy-fuel combustion process is proposed. Calculation of the required membrane area for operating a 50 MW coal-fired power plant showed that the modified process comprises a viable option. \odot 2014 Elsevier B.V. All rights reserved.

1. Introduction

Oxy-fuel combustion is a promising technique for $CO₂$ capture in a fossil fuel-fired power plant. In a typical oxy-fuel combustion process, pure oxygen instead of air is used for fuel combustion, resulting in a concentrated $CO₂$ gas stream, thus enabling efficient $CO₂$ capture. In most cases pure oxygen is separated from air via the cryogenic distillation or the pressure swing adsorption (PSA) process. Both processes are energy intensive, which limits further development of the oxy-fuel combustion technique $[1,2]$. It is proposed that oxygen can be produced by using mixed ionicelectronic conducting (MIEC) ceramic membranes, through which (neutral) oxygen transport at elevated temperatures (usually higher than 700 °C) [\[3,4\].](#page--1-0) A general scheme of this process is given in [Fig. 1.](#page-1-0) The oxygen, as separated from air by the membrane, is carried by the sweep gas $CO₂$, while the $CO₂/O₂$ gas mixture is used to combust the fossil fuel. After combustion and purification, the exhaust gas mainly consists of $CO₂$ ($>95%$). Part of the $CO₂$ is recycled as sweep gas and the rest is compressed for delivery and storage.

Most MIEC materials have the perovskite crystal structure and contain alkaline-earth elements like Ca, Sr or Ba. Due to the presence of these elements, a carbonation reaction tends to occur when these

membranes are exposed to a $CO₂$ -containing atmosphere. This reaction results in the formation of an alkaline-earth carbonate layer on the membrane surface, which is impermeable for oxygen, resulting in a decline in oxygen flux or even to a non-permeating membrane. For example, $\text{SrCo}_{0.8}\text{Fe}_{0.2}\text{O}_{3-\delta}$ (SCF), a highly oxygen-permeable material, shows a decrease in oxygen flux to almost zero within 100 h when using $CO₂$ as sweep gas [\[5\].](#page--1-0) In order to increase the $CO₂$ tolerance of SCF membranes, Sr^{2+} was partially substituted with La³⁺ [\[6\]](#page--1-0), or Co/Fe with Ti^{4+} , Zr^{4+} , Ta^{5+} or Nb^{5+} [\[7,8\].](#page--1-0) However, this improvement in $CO₂$ tolerance was at the expense of a decrease in oxygen flux [\[9\].](#page--1-0)

Besides partial substitution, there are other parameters that affect the $CO₂$ tolerance of SCF, for example, temperature and $CO₂$ partial pressure ($pCO₂$). Yi et al. [\[10\]](#page--1-0) found that SCF is more stable at higher temperature and lower $pCO₂$ (balanced with helium), and suggested SCF membranes should be operated above 900 \degree C. In the present study we examined another possible parameter: the oxygen partial pressure $(pO₂)$, which has not been reported before to the best of our knowledge, as a way to improve the $CO₂$ tolerance of alkaline-earth containing perovskite materials. In this study thermal-gravimetric analysis (TGA) was used to investigate the effect of $pO₂$ on the stability of the SCF perovskite system in a $CO₂$ -containing atmosphere. X-ray photoelectron spectroscopy (XPS) was used to examine the oxygen bonding energy of SCF at different oxygen partial pressures. Oxygen permeation experiments were performed to test the $CO₂$ tolerance of SCF membranes under operating conditions by adding 0% or 5% of oxygen to the sweep

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Fig. 1. Scheme for the membrane integrated oxy-fuel combustion process.

gas $(CO₂)$. Finally, we propose a modified oxy-fuel combustion process and estimated the SCF membrane area needed in a combustion process for a 50 MW coal-fired power plant.

2. Experimental procedure and methodology

2.1. Sample preparation

 $SrCo_{0.8}Fe_{0.2}O_{3-\delta}$ (SCF) was synthesized using an EDTA complexation/pyrolysis process. Metal nitrates were dissolved at a stoichiometric ratio in demineralized water under stirring. EDTA, dissolved in ammonium hydroxide, was added for chelating and after several minutes citric acid was added as well. The molar ratio of total metal ions:citric acid:EDTA was 1.0:1.5:1.0. The pH of the solution was adjusted to 6 by adding ammonium hydroxide. Subsequently $NH₄NO₃$ was added as an ignition aid at an amount of 100 g NH₄NO₃ per 0.1 mol of metal ions. The final solution was heated at $120-150$ °C under stirring to evaporate water until the system changed into a viscous gel, which was transferred to a stainless steel vessel and heated on a hot plate at a temperature of around 500 \degree C, while a vigorous combustion took place, resulting in a fluffy powder. The powder was collected and calcined at 950 °C for 5 h at a heating and cooling rate of 3 °C/min. The calcined powders were uniaxially pressed at 4 MPa into diskshaped membranes, subsequently cold isostatically pressed at 400 MPa for 6 min, and sintered in ambient air at 1200 \degree C for 10 h at a heating rate of 3 \degree C/min and a cooling rate of 2 \degree C/min.

2.2. Thermal-gravimetric analysis (TGA)

Isothermal gravimetric analyses were carried out on a Netzsch TG 449 F3 Jupiter[®]. About 45 mg of SCF powder was weighed in an alumina crucible and placed in the TGA setup. The system was heated (10 \degree C/min) to the desired temperature, in the range 900–1000 °C, in a flowing (120 ml/min) O_2/N_2 mixture at four different oxygen partial pressures $(pO₂)$, namely 10⁻⁴, 0,05, 0.1 and 0.2 bar. The system was held at this temperature for 1 h to attain equilibrium. Next, the purge gas was switched to a mixture of $O_2/N_2/67\%$ CO₂ (flow rate 120 ml/min), keeping the oxygen partial pressure (and thus the oxygen flow rate) in the gas mixture identical as before switching (so respectively 10^{-4} , 0,05, 0.1 and 0.2 bar), After 5 h, the system was cooled down at 20 $°C/$ min in the same purge gas. All TGA data were processed with a correction file of a blank crucible using the same temperature program, to exclude background data of the equipment.

Fig. 2. Schematic diagram of the high temperature permeation setup.

2.3. X-ray photoelectron spectroscopy analysis

For X-ray photoelectron spectroscopy (XPS: ESCALAB MK II, VG equipment) analysis SCF bars (8 mm \times 4 mm \times 3 mm) were prepared using the same procedure as for the disk-shaped membranes. After sintering and polishing to the desired dimensions, the samples were annealed in nitrogen (pO_2 = 10⁻⁴ bar) or oxygen (pO_2 = 1.0 bar) at 950 \degree C for 20 h and quenched to room temperature within a few seconds. Afterwards, the bars were fractured and only the center part of the cross section was analyzed by XPS using an X-ray beam size of 250 μm and a step size of 0.05 eV.

2.4. Oxygen permeation measurements

The experimental setup for oxygen permeation measurements is schematically shown in Fig. 2. Disk-shaped membranes with a diameter of 15 mm and a relative density $> 90\%$ were polished to a thickness of 1 mm and ultrasonically cleaned in ethanol. The membranes were sealed to one end of a quartz tube (diameter 12 mm) using gold paste and a sealing temperature of 1000 \degree C. After sealing, the temperature was lowered to 950 \degree C, and air was Download English Version:

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