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## Research papers

# On the suspension of graded sediment by waves above ripples: Inferences of convective and diffusive processes

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## ARTICLE INFO

## Article history:

Received 11 December 2014

Received in revised form

2 October 2015

Accepted 9 October 2015

Available online 22 October 2015

## Keywords:

Sediment transport

Waves

Graded sediment

Sand ripples

Reference concentration

Suspended concentration profiles

## ABSTRACT

The relationship between the grain size distribution of the sediment on the bed and that found in suspension due to wave action above ripples is assessed here using detailed, pumped sample, measurements obtained at full-scale and also at laboratory scale. The waves were regular and weakly asymmetrical in most tests, and irregular in a minority of tests. The beds comprised fine and medium sand and were rippled in all tests. The cycle-mean sediment concentrations ( $C$ ) from the pumped samples were split into multiple grain size fractions and then represented by exponential C-profile shapes. The analysis of these profiles was carried out in two stages to determine: (i) the relationship between the size distribution of the sediment on the bed and that found in the reference concentration, and (ii) the behaviour of the exponential decay scale of the C-profiles. From this analysis inferences are made about the relative roles of diffusion and convection in the upward sediment flux linked to the process of vortex shedding from the ripple crests. The Transfer function ( $Tr$ ) defined to relate the bed sediment size distribution to that of the reference concentration indicates that, while finer fractions are relatively easily entrained, the suspension of some coarser fractions is caused by an additional convective effect that supplements diffusion. The evidence for this becomes pronounced above steep ripples, and the Transfer function suggests further that irregular waves increase the occurrence of coarser fractions in suspension. A functional form for  $Tr$  is suggested incorporating these principles. The exponential decay scale  $L_S$  arising from the fractional C-profiles is also examined to assess the mechanisms responsible for the upward transfer of grains and a parameterisation of  $L_S$  related to ripple size is suggested. The separate findings for  $Tr$  and  $L_S$  present supporting evidence of diffusion affecting the finer fractions in suspension and combined diffusion + convection affecting the coarser fractions. The methodology developed allows the vertical profile of suspended median grain size to be predicted given knowledge of both the bed grain size distribution and also the flow conditions.

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## 1. Introduction

Although the seabed sediment typically comprises a broad size distribution surprisingly little account is taken of this in many of the methods used in sediment transport estimation. A single representative grain size is generally used to characterise the sediment even though the seabed includes both fine grain fractions that can readily be entrained into suspension, for example by waves, and also coarse fractions that only ever form part of the bed load. The resulting grain size distribution in suspension can be significantly different from that of the seabed. Further, due to the larger settling velocities of the coarser fractions, the suspended

sediment size distribution becomes progressively dominated by finer grains as height above the bed increases. This has significant implications, for example in relation to sediment sorting across beach profiles and to water quality where contaminants are attached to finer or coarser particles. If the vertical sorting of sediment grains between the bed surface material and the suspension, and hence the relative movement of finer and coarser particles, is not taken into account, this may lead to bias and inaccuracy in predicting net sediment transport rates. In a series of laboratory experiments involving different sand mixtures beneath asymmetric waves, O'Donoghue and Wright (2004) showed that the relative contributions to the net transport, in suspension and in the near-bed sheet flow layer, varied significantly depending upon the sand size and grading.

Detailed procedures for modelling grain mixtures have remained rather *ad hoc*, with observations suggesting that some grain size fractions in suspension can be far coarser than

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**Nomenclature**

$a$	coefficient in Eq. (A.2)	$L_{ST}$	total decay (or distribution) length scale for the aggregated C-profile
$a_1, a_2$	coefficients in ripple ‘flow contraction’ expression	$Re_s$	Reynolds number of a settling grain ( $=w_s d/\nu$ )
$A_1$	semi-orbital near-bed excursion amplitude based on the wave fundamental frequency	$RE$	wave Reynolds number ( $=U_1 A_1/\nu$ )
$A_*$	( $=D_*^3$ ) Archimedes Buoyancy Index	$s$	( $=\rho_s/\rho$ ) relative sediment density
$b$	coefficient in Eq. (A.2)	$T, T_p$	wave period, peak wave period
$b_1, b_2$	coefficients in Transfer function expression (Eq. (14))	$Tr$	‘Transfer function’ relating the reference concentration to the bed sediment
$B_1, B_2$	dimensional coefficients with numerical values depending upon $\nu$ , $s$ and $g$	$u_*$	friction (or shear) velocity (with prime $u_*'$ : skin friction component)
$c_1$ – $c_4$	empirical constants	$u_{*w}$	peak value of friction (or shear) velocity during the wave cycle (with prime $u_{*w}'$ : as above)
$C$	wave cycle-mean sediment concentration	$U_1, U_2$	first and second harmonics of the near-bed wave velocity amplitude
$C_0, C_a, C_r$	sediment volumetric reference concentration at height $z=0$ , $z=a$ and $z=z_r$ , respectively	$w$	upward fluid velocity (convective velocity in <a href="#">Fredsoe and Deigaard's (1992)</a> model)
$C_{bi}$	bed sediment volumetric concentration of the $i$ th grain fraction	$w_s$	sediment settling velocity
$C_{ri}$	volumetric reference concentration of the $i$ th grain fraction ( $\langle \dots \rangle$ denotes a wave cycle-mean)	$w_{sc}$	settling velocity corresponding to the critical grain size in suspension $d_c$
$C_{cb}$	cumulative %-distribution of bed sediment sizes	$X$	non-dimensionalisation of grain diameter, defined by Eq. (14)
$C_{cr}$	cumulative %-distribution of reference concentration particle sizes	$z$	height above the bed
$C_i(z_j)$	suspended concentration of the $i$ th grain fraction at the $j$ th height $z$ above the bed	$z_a$	reference height above the bed at which $C=C_a$
$C_{cum,i}(z_j)$	cumulative concentration based on $C_i(z_j)$	$z_r$	height of reference concentration $C_r$
$C_{sum}(z_j)$	total concentration summed over the $i$ grain fractions at the $j$ th height $z$ above the bed	$\beta$	( $=\epsilon_s/\epsilon_m$ ) quotient describing the local difference between the diffusion of a fluid ‘particle’ and a discrete sediment particle
$d$	sediment grain size; this includes sizes obtained by interpolating the discrete $d_m$ scale	$\delta_s$	near-bed layer thickness in which sediment diffusivity $\epsilon_s$ remains constant
$d_c$	maximum allowable or critical grain size in suspension	$\epsilon_e$	estimated sediment diffusivity in <a href="#">Fredsoe and Deigaard's (1992)</a> convective model
$d_s$	sieve size used in grain distribution analysis	$\epsilon_m$	eddy viscosity, or vertical diffusion coefficient for momentum, in a clear fluid
$d_m$	grain size corresponding to central diameter for each sieve interval determined at the respective mid-points on the $\phi$ scale	$\epsilon_s$	sediment vertical diffusivity
$d_{50}$	median grain diameter of the sediment	$\phi$	( $=-\log_2(d)$ with $d$ in mm) Krumbein phi scale
$d_{50b}$	median grain diameter of the bed material	$\eta$	ripple height
$d_{50s}$	median grain diameter of the sediment in suspension	$\lambda$	ripple wavelength
$d_i$	sediment grain diameter (bed or suspended material) for which $i\%$ of the grains are finer by volume (or weight)	$\nu$	kinematic viscosity of water
$d_0$	( $=2A_1$ ) near-bed orbital diameter	$\theta$	Shields parameter, peak value during wave cycle (Eq. (12)) (with prime $\theta'$ : skin friction component)
$D_*$	dimensionless grain size (defined by Eq. (10))	$\rho$	density of water
$f_w$	wave friction factor ( $f_{w,max}$ is maximum value according to <a href="#">Swart's (1976)</a> formula)	$\rho_s$	density of sediment
$g$	acceleration due to gravity	$\sigma_g$	( $= (d_{84}/d_{16})^{0.5}$ ) geometric standard deviation of the sediment
$H, H_s$	wave height, significant wave height	$\tau_b$	bed shear stress ( $\langle \dots \rangle$ denotes a wave cycle-mean)
$k_s$	equivalent bed roughness	$\tau_{crit,i}$	critical shear stress for the $i$ th grain fraction of the bed sediment in isolation
$L_s$	( $=\epsilon_s/w_s$ ) decay (or distribution) length scale of the exponential C-profile	$\tau_e$	time scale of exchange in <a href="#">Fredsoe and Deigaard's (1992)</a> convective model
		$\omega$	( $=2\pi/T$ ) wave angular frequency

accounted for by standard methodologies. For example, [Masselink et al. \(2007\)](#) estimated the sediment size in suspension above oscillatory ripples at a coarse-grained beach site to be 0.6 mm with settling velocity 80 mm/s; these values are far larger than would be predicted by the turbulent diffusion methodologies referred to later. This raises the interesting and important question: ‘are all grain fractions in suspension in a given flow influenced in the near-seabed layer by the same mixing mechanisms?’ The answer is implicit in some previous works (e.g. [Van Rijn, 1993](#)), but we return to the question here with the benefit of an extensive, detailed data set highlighting the suspension of graded sediments by waves above rippled beds. While arguing that the answer is ‘no’,

we infer from the experimental data that, while the finer fractions in suspension are influenced primarily by diffusion, the coarser fractions are progressively influenced also by convection. The present study is in two parts, each involving suspended sediment data obtained beneath waves in both a full-scale wave facility and also a laboratory flume. Initially we consider the relationship between the size distribution of the sediment on the bed and that in suspension, and then the nature and causes of the concentration profiles of the individual fractions in suspension. A similar study was carried out for steady flow by [Sengupta \(1979\)](#) who related the size distribution of the bed material to that obtained in suspension by pumped sampling at a fixed height above the bed.

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