



Review

Modelling approaches in membrane distillation: A critical review

I. Hitsov ^{a,b,*}, T. Maere ^a, K. De Sitter ^b, C. Dotremont ^b, I. Nopens ^a^a BIOMATH, Department of Mathematical Modelling, Statistics and Bioinformatics, Faculty of Bioscience Engineering, Ghent University, Coupure Links 653, 9000 Ghent, Belgium^b VITO – Flemish Institute for Technological Research, Boeretang 200, 2400 Mol, Belgium

ARTICLE INFO

Article history:

Received 27 August 2014

Received in revised form 22 December 2014

Accepted 24 December 2014

Available online 31 December 2014

Keywords:

Heat transfer

Mass transfer

Membranes

Simulation

Membrane distillation

ABSTRACT

Membrane distillation is a technique aimed at separating non-volatile components such as salts from aqueous feed streams. Mathematical modelling of a complex process like membrane distillation allows building further insight needed for effective analysis and optimization of the system, possibly leading to a breakthrough of the technology. Several models have been proposed in the literature for the heat and mass transport in the water channels of the module as well as inside the porous membranes. This article provides a critical review of these models and discusses the pros and cons of the different models to guide the reader into selecting the most suitable simulation approach. Moreover, research gaps in the literature are listed to indicate what is currently missing from a modelling as well as experimental data collection perspective. Areas for further research are suggested.

© 2015 Elsevier B.V. All rights reserved.

Contents

1. Introduction	49
2. State of the art in membrane distillation modelling	51
2.1. Heat transfer models.....	51
2.1.1. General Nusselt number-based approach	51
2.1.2. Considerations and extensions of Nusselt equations HT models	52
2.1.3. Calculation of membrane thermal conductivity	52
2.1.4. Experimental validation of Nusselt equations HT model.....	53
2.2. Mass transfer (concentration polarization) inside the feed channel	53
2.2.1. Concentration polarization estimation based on the Sherwood number	53
2.2.2. Calculation of water partial pressure and activity	53
2.3. Models for mass transfer inside the membrane	54
2.3.1. Fick's law model.....	54
2.3.2. Dusty gas model.....	54
2.3.3. Simplifications of the DGM – Ordinary, Knudsen and Transition regions.....	55
2.3.4. Gas permeation test for evaluation of DGM membrane parameters.....	55
2.3.5. Limitations of the dusty gas model.....	56
2.3.6. Pore size distribution models	56
2.3.7. Schofield's model	57
2.3.8. Structural network models (Monte Carlo)	57
2.3.9. Ballistic transport model	57

* Corresponding author at: BIOMATH, Department of Mathematical Modelling, Statistics and Bioinformatics, Faculty of Bioscience Engineering, Ghent University, Coupure Links 653, 9000 Ghent, Belgium.

E-mail addresses: Ivaylo.Hitsov@ugent.be (I. Hitsov), Thomas.Maere@ugent.be (T. Maere), Kristien.DeSitter@vito.be (K. De Sitter), Chris.Dotremont@vito.be (C. Dotremont), Ingmar.Nopens@ugent.be (I. Nopens).

2.4.	Empirical models.....	57
2.4.1.	Artificial neural network (ANN) models	58
2.4.2.	Empirical models based on tools from Design of Experiments (DoE).....	58
2.5.	Computational Fluid Dynamics (CFD) models.....	58
2.5.1.	CFD models for heat transfer optimization in the channels	59
2.5.2.	CFD models for heat and mass transfer optimization in the channels	59
2.5.3.	CFD system models including the mass transfer inside the membrane	59
3.	Discussion and research gaps	60
3.1.	Discussion	61
3.2.	Research gaps	61
4.	Conclusions.....	62
	References	62

Nomenclature

\bar{P}	average pressure (Pa)	DCMD	Direct Contact Membrane Distillation
δ	membrane thickness (m)	DGM	Dusty Gas Model
ϵ	porosity (-)	DoE	design of experiments
γ	activity coefficient (-)	EE	Energy Efficiency (%)
κ	thermal conductivity (W/m K)	h	heat transfer coefficient (W/m ² K)
λ_i	mean free path of a the molecule (m)	H_v	specific heat of evaporation (J/mol K)
$ p_a _{ln}$	logarithmic mean pressure of air across the membrane (Pa)	HT	Heat Transfer
μ	dynamic viscosity (Pa s)	K	mass transfer coefficient (m/s)
v	mean molecular speed ($\sqrt{\frac{8RT}{\pi M}}$, m/s)	K_B	Boltzmann constant (m ² kg/s ²)
ρ	density (kg/m ³)	KTG	Kinetic Theory of Gasses
σ_i	water vapour collision diameter (Å)	m	molality (mol/kg)
τ	tortuosity (-)	MT	mass transfer
D	diffusive (superscript)	Mw	molar weight (kg/mol)
V	viscous (superscript)	N	flux (mol/m ² s)
a	air (subscript)	P	pressure (Pa)
b	bulk (subscript)	P_a	partial pressure (Pa)
f	feed (subscript, superscript)	Pr	average pressure of air inside the membrane (Pa)
g	gas (subscript)	Pr_{wall}	Prandtl number (-)
m	membrane (subscript)	q	Prandtl number at the membrane interface (-)
p	permeate (subscript, superscript)	R	heat flux (W/m ²)
s	solid (subscript)	r	universal gas constant (J/mol K)
w	water (subscript)	Re	pore radius (m)
ANN	artificial neural network	RSM	Reynolds Number (-)
c	concentration (mol/m ³)	SNM	response surface methodology
C_p	specific heat capacity (J/kg K)	T	Structural Network Model
CFD	Computational Fluid Dynamics	U	temperature (K)
D	diffusion coefficient (m ² /s)	v	overall heat transfer coefficient (W/m ² K)
d	characteristic size of channel (m)	VMD	velocity (m/s)
$D_{ij,e}^m$	effective molecular diffusion coefficient (m ² /s)	x	Vacuum Membrane Distillation
D_{ij}^K	effective Knudsen diffusion coefficient (m/s)		molar fraction (-)

1. Introduction

Membrane distillation (MD) was first developed in 1963 by Bodel when he patented the vapour diffusion through silicone rubber for saline water distillation [1]. The most used and studied MD configuration is the direct contact membrane distillation where the hot feed and the cold permeate solutions are separated by a hydrophobic membrane. The feed solution comes into contact with the membrane and evaporates, the vapour travels through the pores and condenses on the cold permeate membrane interface (Fig. 1).

The temperature difference across the membrane between the feed side (T_{mf}) and the permeate side (T_{mp}) as indicated in Fig. 1 results in different partial pressures of water vapour at the feed (P_{mf}) and the permeate side (P_{mp}). It is noteworthy that the actual driving force for the flux through the membrane is the vapour

pressure difference and only the evaporated phase is transported across the membrane. The use of thin membranes creates large vapour pressure gradients, therefore allowing MD to be operated at relatively low feed temperatures, potentially allowing to reuse waste heat from other processes.

The heat and mass transfer in MD are interconnected and lead to a complex relationship. When water is evaporated on the feed side it takes away part of the energy of the feed, which is carried away by the water vapour flux. This energy is transferred to the permeate during the condensation. Moreover, some of the energy is transferred through the membrane matrix itself via conduction in the form of sensible heat. The combined effect of the sensible heat and the heat due to evaporation creates thermal boundary layers near the interface of the membrane, leading to reduction of the intermembrane flux.

Download English Version:

<https://daneshyari.com/en/article/640792>

Download Persian Version:

<https://daneshyari.com/article/640792>

Daneshyari.com