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Invited review

The physics of wind-blown loess: Implications for grain size proxy interpretations in Quaternary paleoclimate studies



Gábor Újvári ^{a,b,*}, Jasper F. Kok ^c, György Varga ^d, János Kovács ^{e,f}

- a Institute for Geological and Geochemical Research, Research Centre for Astronomy and Earth Sciences, Hungarian Academy of Sciences, H-1112 Budapest, Budaörsi u. 45., Hungary
- ^b Geodetic and Geophysical Institute, Research Centre for Astronomy and Earth Sciences, Hungarian Academy of Sciences, H-9400 Sopron, Csatkai E. u. 6-8., Hungary
- ^c Department of Atmospheric and Oceanic Sciences, University of California, 405 Hilgard Ave, Los Angeles, 90095, CA, USA
- d Geographical Institute, Research Centre for Astronomy and Earth Sciences, Hungarian Academy of Sciences, H-1112 Budapest, Budaörsi út 45., Hungary
- ^e Department of Geology and Meteorology, University of Pécs, H-7624 Pécs, Ifjúság u. 6., Hungary
- f Environmental Analytical and Geoanalytical Laboratory, Szentágothai Research Centre, University of Pécs, H-7624 Pécs, Ifjúság u. 20., Hungary

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ABSTRACT

Loess deposits are recorders of aeolian activity during past glaciations. Since the size distribution of loess deposits depends on distance to the dust source, and environmental conditions at the source, during transport, and at deposition, loess particle size distributions and derived statistical measures are widely used proxies in Quaternary paleoenvironmental studies. However, the interpretation of these proxies often only considers dust transport processes. To move beyond such overly simplistic proxy interpretations, and toward proxy interpretations that consider the range of environmental processes that determine loess particle size distribution variations we provide a comprehensive review on the physics of dust particle mobilization and deposition. Furthermore, using high-resolution bulk loess and quartz grain size datasets from a last glacial/interglacial sequence, we show that, because grain size distributions are affected by multiple, often stochastic processes, changes in these distributions over time allow multiple interpretations for the driving processes. Consequently, simplistic interpretations of proxy variations in terms of only one factor (e.g. wind speed) are likely to be inaccurate. Nonetheless using loess proxies to understand temporal changes in the dust cycle and environmental parameters requires (i) a careful site selection, to minimize the effects of topography and source distance, and (ii) the joint use of bulk and quartz grain size proxies, together with high resolution mass accumulation rate calculations if possible.

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E-mail address: ujvari.gabor@csfk.mta.hu (G. Újvári).

^{*} Corresponding author.

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Abbreviations			collection/collision efficiency due to thermophoresis in below-cloud scavenging				
Appear	ring in the main text	F_d	dust emission rate/vertical dust flux of airborne dust $(\mu g m^{-2} s^{-1})$				
а	constant in mean charge calculations for raindrops and particles	$F_{d,a}$	dust emission rate due to direct aerodynamic lifting $(\mu g m^{-2} s^{-1})$				
A_2	coefficient including factors like particle shape, sorting, pack-	$F_{d,d}$	dust emission rate due to disaggregation/auto-abrasion				
4	ing and bed roughness	г	(μg m ⁻² s ⁻¹)				
A_B	dimensionless threshold friction velocity (Bagnold, 1941)	$F_{d,s}$	dust emission rate due to saltation bombardment/ sandblasting ($\mu g m^{-2} s^{-1}$)				
A_c	the contact area between adjacent grains	г					
A_{Co1}	model parameter associated aerodynamic forces (Cornelis	F_{dep}	dry deposition flux at a reference height z_r (g m ⁻² s ⁻¹)				
4	et al., 2004a,b) (N m ⁻¹)	F_D	aerodynamic drag force (N)				
A_{Co2}	model parameter associated inter-particle forces (Cornelis	F_G	gravity force (N)				
4	et al., 2004a,b) $(N m^{-1})$	F_C	inter-particle cohesive force (N)				
A_{Co3}	geometry factor (Cornelis et al., 2004a) (N ⁻¹ m ⁻¹)	F_L	aerodynamic lift force (N) acceleration due to gravity (m s^{-2})				
A_N	dimensionless threshold friction velocity (Shao and Lu, 2000)	g					
b_r	width of an individual roughness element (m) heat capacity of air ($\text{m}^2 \text{ s}^{-2} \text{ K}^{-1} / \text{J kg}^{-1} \text{ K}^{-1}$)	GS GSI	grain size				
C _a			grain size index, the ratio of 20–50 µm/<20 µm fractions				
C_1	coefficient in the Ferguson and Church (2004) model, a con-	h_r	height of a roughness element (m) rainfall intensity (mm h^{-1})				
C_2	stant for laminar settling for Re_{pt} < 1 coefficient in the Ferguson and Church (2004) model, a con-	J k _a	thermal conductivity of air ($J m^{-1} s^{-1} K^{-1}/W m^{-1} K^{-1}$)				
C ₂	stant C_d for $Re_{pt} > 10^3$		thermal conductivity of article (J m ⁻¹ s ⁻¹ K ⁻¹ /W m ⁻¹ K ⁻¹)				
C_B	constant for the saltation mass flux model of Bagnold (1941)	k_p	empirical coefficient in the Shao (2001) model				
C_c	Cunningham slip correction factor	k _s k	Boltzmann constant (1.3806488 \times 10 ⁻²³ J K ⁻¹ /				
C_c	drag coefficient	K	$m^2 \text{ kg s}^{-2} \text{ K}^{-1}$				
C_{DK}	parameter for the saltation mass flux model of Kok et al.	K	eddy (or turbulent) viscosity				
CDK	(2012)	K K _{ES}	constant in calculation of the electrostatic collection efficiency				
C_K	constant for the saltation mass flux model of Kawamura	K _{ES} Kn	Knudsen number				
CK	(1951)	LGM	Last Glacial Maximum				
C_p	local concentration of depositing particles (g m ⁻³)	m	surface shear stress inhomogeneity parameter				
C_p	roughness element drag coefficient	M_a	molecular weight of air (kg kmol ⁻¹)				
_	surface drag coefficient	MAR	mass accumulation rate				
C _S d	zero plane displacement height (m)	M_d	median (D_{50}) grain size (μm)				
D_B	Brownian diffusivity of particles (m^2 s ⁻¹)	MIS	Marine Isotope Stage				
D_p	particle diameter (m)	M_r	modulus of rupture (Pa)				
D_p	typical roughness element size (Nikuradse roughness)	M_s	mean grain size (µm)				
D_{rd}	raindrop diameter (m)	MS	magnetic susceptibility				
D _{ra} D _{rd-r}	representative raindrop diameter (m)	$M_{\rm w}$	molecular weight of water vapor (kg kmol ⁻¹)				
D_{ra-r} D_w	water vapour diffusivity in air $(m^2 s^{-1})$	n_r	number of roughness elements				
E_B	collection efficiency from Brownian diffusion	$n_{\rm S}$	empirical coefficient in the Shao (2001) model				
E_{Bw}	collection/collision efficiency from Brownian diffusion in	$N(D_p)$	particle number concentration with a diameter between D_p				
~BW	below-cloud scavenging	11(Dp)	and $D_p + dD_p$				
E_{DPw}	collection/collision efficiency due to diffusiophoresis in	$N(D_p)_t$	particle number concentration at time t with a diameter be-				
DFW	below-cloud scavenging	(p)(tween D_p and $D_p + dD_p$				

electrostatic collection/collision efficiency in below-cloud initial number concentration of particles with a diameter be- $N(D_p)_0$ E_{ESw} scavenging tween D_p and $D_p + dD_p$ E_{IM} collection efficiency from impaction $N(D_{rd})$ raindrop number size distribution collection/collision efficiency from inertial impaction in $N(D_{rd-r})$ number concentration of representative raindrop E_{Imw} $p_a^{\hat{o}}$ p_s^0 below-cloud scavenging vapour pressure of water at temperature T_a (Pa) E_{IN} collection efficiency from interception vapour pressure of water at temperature T_s (Pa) $p_s(D_p)$ E_{Inw} collection/collision efficiency from interception in belowsoil/sediment size distribution fully-disturbed particle size distribution of the parent soil cloud scavenging $p_f(D_p)$ EM end member $p_m(D_p)$ minimally-disturbed particle size distribution of the parent end member modeling algorithm **EMMA** soil

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