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Heat transfer characteristics and energy-consumption benchmark state with varying operation boundaries for coal-fired power units: An exergy analytics approach



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HIGHLIGHTS

• The idea of 'energy-consumption benchmark state' was proposed.

• The parameters type includes controllable boundaries in operation and maintenance and uncontrollable boundaries.

- Models for benchmark state were built under varying boundaries involving load rate, coal quality and ambient temperature.
- The effect of boundary factors on the heat transfer coefficients of heat and mass transfer process has been illustrated.

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ABSTRACT

The energy-saving analytics of coal-fired power units in China is confronting new challenges especially under varying working conditions and operation boundaries, such as load rate, coal quality and ambient temperature. Compared with traditional optimization of specific operating parameters, the idea of energy-consumption benchmark state was proposed. The exergy analytics was introduced to determine the energy-consumption benchmark state, with the minimum exergy destruction under varying operation boundaries. The heat transfer coefficient and condenser vacuum were calculated by considering the influence of operation boundaries in different coal guality and ambient temperature. The coal rate was figured out for the coal fuel in different composition and calorific values, for the circulating water condition in different temperatures and cooling modes with different load rate. As a case study, the energy consumption model of a 1000 MW ultra supercritical power unit was built on the platform of Ebsilon and tested by practical operation data of power unit. The results show that the heat transfer coefficient and condenser vacuum change greatly with different coal composition and circulating water temperatures under different working conditions. The energy-consumption benchmark state of power unit is also operation condition and boundary-dependant. The coal rate of such benchmark state is considerably less than that of the actual state with the same operation boundaries. This makes great reference for the operation optimization of coal-fired power units.

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1. Introduction

Energy conservation in thermal power generation has been increasingly concerned in China for the last decades for several facts. The installed capacity of thermal power units has accounted for 71.5% of the total by the end of 2012 with the coal consumption for power generation shared a steady increase from 47.67% in 2005

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http://dx.doi.org/10.1016/j.applthermaleng.2014.12.020 1359-4311/© 2014 Elsevier Ltd. All rights reserved. to 52.67% in 2011 of the nation-wide coal consumption in overall industries; the coal rate of thermal power generation has reduced dramatically by 59 g/kWh from 385 g/kWh in 2001 to 326 g/kWh in 2012 [1]. It is of great significance for coal-fired power generation to reduce the coal consumption and pollutant emission in considerable extent.

The in-depth energy-saving analytics of coal-fired power units in China is confronting new challenges. Firstly, the coal-fired power units are complex systems with great number of subsystems, equipment and instruments, and there are high-dimension, nonlinear and strong coupling correlation between different

Nomenclature		$(\overrightarrow{x},\overrightarrow{v})$	power unit state	
		$(\overrightarrow{x}, \overrightarrow{v})^b$	energy-consumption benchmark state	
		f(.)	function captures the mapping between (\vec{x}, \vec{v}) and y	
Abbreviation		\overrightarrow{s}	vector of boundary variables	
AH air pr	eheater	Sc	cth boundary variable	
AT spray	desuperheater	$\overrightarrow{\mathbf{s}}$	ith vector of boundary variable	
CAV cavity		$J_i \rightarrow h$		
HTC heat t	transfer coefficient	$(\vec{x}, \vec{v}) \frac{s}{s}$	energy-consumption benchmark state with boundary	
CON conde	enser		$\overrightarrow{S_i}$	
CI coolir	ng tower	$(\overrightarrow{x_i}, \overrightarrow{v_i}) =$	\rightarrow ith power unit state with boundary $\vec{s_i}$	
CWP circul	ating water pump	(j, j, s_i)	the heat transfer	
CWT circul	ating water temperature	V V	heat transfer coefficient	
DA decre	asing amplitude	Δ	the heat transfer area	
DEA deaer	ator	Λt	the temperature difference	
ECON econo	omizer	$\Delta \iota$	energy_consumption variable of <i>i</i> th power unit state	
ES extrac	ction steam	$y \xrightarrow{s_i} j$	\therefore $1 \rightarrow \rightarrow$	
ESFC energ	y specific fuel consumption	0	with boundary s _i	
FKH III III	reneater	$\Omega \rightarrow \gamma$	reasible space of boundaries	
FSH final S	superneater	$Q(\overline{x_j}, \overline{v_j})$	$\overrightarrow{s_i}$ the heat between boundary $\overrightarrow{s_i}$ and the	
FVVP leedw	ia concertor		corresponding power unit state $(\overrightarrow{x_i}, \overrightarrow{v_i})_{\overrightarrow{s}}$	
G electi	acal concumption rate	$k \rightarrow$	heat transfer coefficient with boundary $\vec{s_i}^{i}$	
GCCK gloss	rove grindability index	$\sigma()$	function captures the mapping between boundary \vec{s}	
Un the n	th feed water probater	8(•)	and k_{\rightarrow}	
HPRH horiz	ontal primary reheater	Enk	exergy destruction of device k	
HP bigb i	pressure turbine	E _E	exergy of the fuel	
IP interr	mediate pressure turbine	E	exergy loss	
IF lower	neurace pressure turbine	Ep	output exergy	
I HV lower	· heating value	b	energy specific fuel consumption	
IP low n	pressure turbine	b _{min}	theoretical minimum energy specific fuel consumption	
PR penda	ant-tube riser	$b_{D,k}$	energy specific fuel consumption of device k	
PRH plater	1-type reheater	b_L	energy specific fuel consumption loss	
PSH plater	n-type superheater	$b \rightarrow i$	energy specific fuel consumption of <i>j</i> th power unit	
SSH screen	n-type superheater	S _i J	state with boundary s	
ST the se	econdary turbine	Р	product	
UF upper	r part of the furnace		product	
VPRH vertic	a vertical primary reheater S		Superscripts	
WW water	wall	b	benchmark	
		w	number of controllable variables	
Symbols		т	number of noncontrollable variables	
y energ	y-consumption variable of a power unit state	n	number of boundary variables	
\overrightarrow{x} vector	r of controllable variables of a system		·	
x_a ath co	th controllable variable Subscripts			
$\overrightarrow{x_i}$ ith ve	ctor of controllable variable	1	index of variables	
\overrightarrow{v} Vecto	r of noncontrollable variables of a system	i	index of variables	
v_h bth co	ontrollable variable	j	index of variables	
$\overrightarrow{v_i}$ ith ve	ector of noncontrollable variable	р	index of variables	
tj jen ve				

sections. It is of more uncertainties, in this mean, to illustrate, evaluate and optimize the economic performance of coal-fired power units [2]; Secondly, the performance of unit proper tends to deteriorate in continuous operation. The heat transfer characteristics, for instance, would become worse by the contamination, ash deposition, erosion and slagging on heat exchanging surfaces [3], in addition to the increasing power consumption of fans and pumps, the decreasing cylinder efficiency resulted from the damaged glands and sealing [4]; Thirdly, the energy-consumption features are dynamically time-dependant especially under the off-designed working conditions and operation boundaries, such as load rate, coal quality and ambient temperature etc [5–7]. The coal-fired power units, even the large-scale power units, have to responsible for the peaking of power grid, partly due to the rapid

development of power generation from renewable energy in China [5]; the coal type and coal quality, terribly affected by the demandand-supply fluctuation of coal market, are quite different and deviated from the designed conditions during the practical operation [6]; in addition, the ambient conditions, such as the ambient temperature and humidity, influences the energy-consumption of coal-fired power units by changing power consumption of pumps and fans and introducing different cooling modes, particularly for the air-cooled coal-fired power units [7].

Т

Traditional energy analysis practices are mainly based on the first law and the second law of thermodynamics [8-10], the former of which focuses on the mass and energy balance, neglecting the properties of the system environment or the degradation of the energy quality through dissipative processes. For the latter,

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