### Chemical Engineering Science 173 (2017) 303-334

Contents lists available at ScienceDirect

# **Chemical Engineering Science**

journal homepage: www.elsevier.com/locate/ces

# Electrostatics in gas-solid fluidized beds: A review

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### HIGHLIGHTS

• The characterization methods of electrostatics in fluidized beds are outlined.

• Charge generation and distribution phenomena in fluidized beds and the underlying mechanisms are discussed.

• The interplay between electrostatics and hydrodynamics in fluidized beds is reviewed.

• Practical applications of tribocharging fluidized beds are presented.

• The CFD simulations of fluidized bed systems including electrostatic charges are compared.

#### ARTICLE INFO

Article history: Received 3 May 2017 Received in revised form 29 June 2017 Accepted 2 August 2017 Available online 3 August 2017

Keywords: Fluidization Electrostatics Hydrodynamics Triboelectric charging Application Simulation

# ABSTRACT

Gas-solid fluidized beds, by their nature, are associated with intense and frequent collisions of solid particles with each other and with the vessel wall, causing tribo-electrification. Accumulation of electrostatic charges in fluidized bed reactors can result in severe problems such as agglomeration, wall fouling, nuisance and hazardous discharge, all reducing the process performance and raising significant safety concerns. Tribo-charging of particles in fluidized beds has also been exploited in a number of useful applications. In this review, the characterization methods of electrostatics and the mechanisms of charge generation and distribution in fluidized beds are presented, followed by an account of the interplay between the hydrodynamics and electrostatic phenomena. Furthermore, techniques of electrostatic charge control in fluidized beds are reviewed, and applications of tribo-electrostatic fluidization systems are summarized. Finally, computational fluid dynamics simulations of the electrostatic effects on the hydrodynamic characteristics of fluidized beds are outlined.

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#### Nomenclature

Symbol	S	Ζ	dis
Ap	probe tip surface area, m <sup>2</sup>		
d	particle diameter, m	Greek letters	
D	fluidized bed diameter, m	$\alpha_i$	fitt
$D_{\rm b}$	bubble size/diameter, m	βi	fitt
$d_p$	particle diameter, m	γ <sub>i</sub>	fitt
$E_{d}$	breakdown potential in air $(3 \times 10^6 \text{ V/m})$	$\Delta t$	tim
F <sub>d</sub>	drag force, kg m/s <sup>2</sup>	$\Delta \tau$	tim
Fe	electrostatic force, kg m/s <sup>2</sup>		pea
$F_{g}$	gravity force, kg m/s <sup>2</sup>	3	voi
Ι	total current, A	ε <sub>0</sub>	vac
q	particle electrostatic charge, C	$ ho_{ m b}$	flui
$q_{\rm m}$	charge density or specific charge on particles, C/kg	$ ho_{ m p}$	par
t	time, s		
Ub	bubble velocity, m/s	Subscripts	
Ug	superficial gas velocity, m/s	1	up
U <sub>jet</sub>	jet velocity, m/s	2	low
$U_{\rm mf}$	minimum fluidization velocity, m/s	max	ma
Ut	terminal settling velocity of particles, m/s	min	mii
VV <sub>s</sub>	entrainment flux of solid particles, kg/m <sup>2</sup> s	mf	miı
Xi	weight fraction of fine particles having $a_i$ as average		
	alameter, amensiomess		

### tance between tips of a dual-tip probe, m

- ed parameter in Eq. (5), kg/m
- ed parameter in Eq. (5), C s<sup>2</sup>/kg m<sup>2</sup>
- ed parameter in Eq. (5), C/kg
- e lag between peaks from two tips, s
- e difference between maximum and minimum aks from one tip. s
- dage, dimensionless
- cuum permittivity (8.854  $\times$  10<sup>-12</sup> F/m)
- idized bed density, kg/m<sup>3</sup>
- ticle density, kg/m<sup>3</sup>
- per probe tip
- ver probe tip
- ximum
- nimum
- nimum fluidization

# 1. Introduction

Fluidization is associated with solid particles being transformed into a fluid-like state by a flowing fluid. It arrived on the industrial scene in a major way in the early 1940s with Fluid Catalytic Cracking (FCC) (Jahnig et al., 1980) and has since been implemented in many other industrial applications, including solid-catalyzed gasphase reactions, non-catalytic reactions and physical processes. Advantageous features of gas-solid fluidized beds such as excellent gas-solid contacting, efficient and uniform heat transfer, temperature uniformity, and suitability for processing a wide range of feedstocks, have led to widespread industrial applications including coal/biomass combustion/gasification/pyrolysis, drying, coating, ore roasting, catalytic processes such as acrylonitrile, aniline and Fischer-Tropsch synthesis, and gas-phase polyolefin production (Grace et al., 2006; Kunii and Levenspiel, 1991).

Electrostatic charging of particles in gas-solid fluidized beds was first reported about 60 years ago in connection with anomalous behavior encountered in experiments on subjects as diverse as heat transfer (Miller and Logwinuk, 1951), elutriation (Osberg and Charlesworth, 1951), and characteristics of fluidized particles (Lewis et al., 1949). Problems associated with fluidized bed electrification include particle-wall adhesion, inter-particle cohesion and electrostatic discharges. The charged particles can coat vessel walls, requiring frequent cleaning. The electrostatic charges on particles and vessel walls, as well as the high-voltage electrical fields arising from them, can affect hydrodynamics and cause the formation of undesired byproducts (Cheng et al., 2012a). They can also interfere with sensors and bed internals, leading to malfunction of measurement instruments and operation (Zhang et al., 2013). For instance, when electrical capacitance tomography (ECT) is applied in a particulate process, electrification can result in measurement errors and even malfunction of some ECT systems (Gao et al., 2012; Zhang et al., 2014). Electrostatic charges are also responsible for potentially severe problems in commercial gassolid fluidized bed facilities due to agglomeration (Ciborowski and Wlodarski, 1962), sheeting (Hendrickson, 2006), shank (fusion of solid particles into solid shapes resulting from overheating particles residing on the reactor wall in a reactive environment) (Moughrabiah, 2009), nuisance discharges and product handling (Chen et al., 2003a, 2003b). All of the obstacles owing to electrostatics, especially sheeting in fluidized bed polymerization reacDownload English Version:

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