ELSEVIER

Contents lists available at SciVerse ScienceDirect

Applied Thermal Engineering

journal homepage: www.elsevier.com/locate/apthermeng



New solid desiccant solar air conditioning unit in Tunisia: Design and simulation study



Zied Guidara a, Mounir Elleuch a, Habib Ben Bacha a,b,*

^a Laboratoire des Systems Electo-Mécaniques (LASEM), National Engineering School of Sfax University of Sfax, B.P W 3038 Sfax, Tunisia ^b College of Engineering at Alkhari, Mechanical Engineering Department, Salman bin Abdelaziz University, B.P. 655, 11942 Alkhari, Saudi Arabia

HIGHLIGHTS

- A new design of solid desiccant solar air conditioning unit is presented.
- Three modes of the functioning for this unit are developed.
- The modelling study is based on thermal and mass balances.
- A simulation study of the functioning of the unit is presented.

ARTICLE INFO

Article history: Received 15 August 2012 Accepted 5 May 2013 Available online 13 May 2013

Keywords:
Air conditioning
Desiccant cooling
Solar energy
Design
Modelling
Simulation

ABSTRACT

Solar air conditioning units present a promising solution for air conditioning, especially desiccant units, in terms of environmental protection and energy saving. In this context, the aim of this paper is a presentation of a new solid desiccant solar air conditioning unit for office spaces in Tunisia and a simulation study of its functioning. Thus, mathematical models for each component are developed which are based mainly on thermal and mass balances. Three mode of functioning are simulated for three climate cases: relatively cold and humid for Bizerte, hot and dry for Remada and finally moderate for Djerba. The results show that the conditioned air obtained in each mode of functioning can ensure comfortable conditions for the office space occupants.

 $\ensuremath{\texttt{©}}$ 2013 Elsevier Ltd. All rights reserved.

1. Introduction

Conditioned air becomes a vital necessity at office spaces. However conventional units of air conditioning have some environmental problems. In addition, conventional units consume a large quantity of electricity [1,2] which is an expensive energy obtained often by means of oil resources [3]. So more and more CO₂ emissions. Furthermore, with conventional units of air conditioning, the dehumidification of the air is done through a cooling operation under dew point temperature [4]. Thus, the air is very cold to be pulsed in the conditioned space. This operation can be characterized as an energy consuming procedure [5] and in some cases it cannot ensure the achievement of temperature and humidity levels required by the user [6].

E-mail address: habibbenbacha@yahoo.fr (H. Ben Bacha).

So due to the lack of oil resources in the planet and the pollution of the environment, many countries are encouraging the use of renewable energies [3] for air conditioning.

In Tunisia, the sector of energy confronts many problems owed essentially to the exhaustion of the reserves of hydrocarbons, and also to the steady increase of the rhythm of the consumption. Consequently the replacement of the conventional electric air conditioning by another alternative becomes a necessity. So limiting the need of the electrical energy for the air conditioning and satisfying needs in air conditioning are the main objectives to be achieved in our country. These objectives should be realized without breaking the international commitments relative to the environmental protection. Indeed, these commitments mainly intend to reduce CO_2 emissions, avoid the use of harmful gases to the ozone layer and to the greenhouse effect used in the conventional air conditioners.

Given the drawbacks mentioned above, many researches many investigations have been performed to solve these problems especially on the design of solar air conditioning unit.

^{*} Corresponding author. College of Engineering at Alkharj, Mechanical Engineering Department, Salman bin Abdelaziz University, B.P. 655, 11942 Alkharj, Saudi Arabia. Tel.: +966 506678408; fax: +966 (0)15453964.

Nomei	Nomenclature		global exchange coefficient between absorber/external environment (W/(m²°C))
A	cross section of the air flow for one channel of the	V	velocity of the air flow (m/s)
71	hygroscopic wheel (m ²)	ν	water velocity (m/s)
A _{1.2}	areas of the coils in the storage tank (m ²)	W	water content in the desiccant (kg _{water} /kg _{desiccant})
A_{lat}	lateral area of one channel of the hygroscopic wheel	x	axial direction (m)
7 Idl	(m^2)	Y	specific humidity (kg _{water} /kg _{dry air})
$A_{ m d}$	desiccant cross section for one channel of the	•	specific framercy (ngwater/ngury air)
2 1 u	hygroscopic wheel (m ²)	Greek letter	
$C_{\rm p}$	specific heat (J/(kg K))	β	optical coefficient
$C_{\rm c}$	specific heat of the absorber J/(kg°C))	α	absorption coefficient of the absorber
$C_{\rm f}$	specific heat of water (J/(kg°C))	τ	transmission coefficient of the glass
f	specific function (°C)	η	water—air heat exchanger efficiency
у Н	enthalpy (kJ/kg _{dry air})	ε	efficiency
h	convective heat transfer coefficient between absorber/	ρ	density (kg/m³)
	water (W/(m^2 °C))	ω	specific humidity of the air (kg _{water} /kg _{dry air})
$h_{ m wh}$	heat transfer coefficient between desiccant/air (W/	ω_{p}	specific humidity of the air at the desiccant coating
	m ² K)	p	(kg _{water} /kg _{dry air})
h_{m}	mass transfer coefficient between desiccant/air (kg/m²s)	$\varphi_{ m p}$	relative humidity of the air at the desiccant coating
I	solar radiation (W/m ²)	Subscripts	
$L_{\rm wh}$	length of the hygroscopic wheel (m)	a	air
L_{ab}	length of the absorber (m)	acc	accumulation
L	mass flow of distributed water per unit of area (kg/	atm	atmospheric
	m^2 s)	С	cold
Μ	mass of the water in the storage tank (kg)	catu	cold air to use
$M_{\rm c}$	mass of the absorber (kg)	CV	convection
$M_{ m f}$	mass of the water (kg)	d	desiccant
$m_{ m f}$	mass flow of the water produced by solar collector (kg/	Ech	air—air heat exchanger
	s)	h	hot
ṁ	mass flow (kg/s)	hatc	hot air to cool
p	pressure (Pa)	Hum	humidifier
Q_{ad}	adsorption heat (J/kg)	in	inlet
S	area of the flat plate solar collector (m ²)	out	outlet
T	temperature (°C, K)	p	desiccant coating
T_{a}	ambient air temperature (°C)	t	treated
$T_{\rm c}$	absorber temperature (°C)	tc	to cool
$T_{ m f}$	water temperature (°C)	tca	treated cold air
$T_{\rm s}$	temperature of the water in the storage tank (K)	tu	to use
$T_{\rm f2/1}$	inlet/outlet water temperature, feeding side (K)	u	used
$T_{11,2}$	inlet/outlet water temperature, distribution side (K)	uha	used hot air
t	time (s)	W	water
$U_{1,2}$	overall heat transfer coefficient of the coil in the	W	wet
	storage tank (W/m ² K)	WS	saturation

In this context, solid desiccant units present a promising solution for air conditioning, in terms of environmental protection and energy saves. Indeed, desiccant units do not use harmful refrigerants to the environment. In addition, desiccant dehumidification is advantageous in handling latent heat, easy to be regenerated using low-grade energy, such as solar energy [7].

The standard desiccant unit which is mostly applied today uses standard components which have been used in air conditioning applications for buildings or factories since many years. These components are (i) a desiccant wheel to dehumidify the air, (ii) a heat exchanger to cool the supply air and to heat the return air, (iii) a humidifier to treat the supply air, (iv) a humidifier to cool the return air using evaporative cooling close to the saturation line and (v) a solar thermal collector system to produce hot air for the regeneration of the desiccant wheel [8].

H.M. Henning et al. [8] presented the results of the desiccant cooling cycle for climatic conditions with high ambient air humidity values. In this case, there is an enthalpy exchanger wheel in

addition to the components used in standards configurations. Thus, the air is pre-cooled and pre-dehumidified before it's entering the standard desiccant cycle using the return air from the conditioned space. However, high regeneration temperature (100 $^{\circ}$ C) is needed to ensure the regeneration of the desiccant wheel.

Furthermore, H.M. Henning et al. [8] presented also a desiccant cycle combined with two cooling coils. Thus, the air is pre-cooled under its dew point temperature by passing through the first cooling coil. This operation ensures the pre-dehumidification of the pre-cooled air. Furthermore, the air is finally cooled to the desired temperature before it's entering the conditioned space by use of the second cooling coil. However, if a compression machine is used for providing cold water, the unit will be more complex and more expensive. Not only this, but it is possible to front the risk of going back to the disadvantages of conventional machines already quoted. On the other hand, if an absorption or adsorption machine is used to produce cold water, the unit will be more complex and more expensive.

Download English Version:

https://daneshyari.com/en/article/646849

Download Persian Version:

https://daneshyari.com/article/646849

<u>Daneshyari.com</u>