Contents lists available at ScienceDirect

Computers and Chemical Engineering

journal homepage: www.elsevier.com/locate/compchemeng

Process plant layout optimization with uncertainty and considering risk

Seyyed Ebrahim Latifi^a, Emran Mohammadi^{a,*}, Nima Khakzad^b

^a School of Industrial Engineering, Iran University of Science & Technology, Tehran, Iran
^b Safety and Security Science Group, Delft University of Technology, The Netherlands

ARTICLE INFO

Article history: Received 11 February 2017 Received in revised form 10 May 2017 Accepted 21 May 2017 Available online 3 June 2017

Keywords: Process plant layout Toxic release Fire and explosion scenarios Domino effect Risk assessment

ABSTRACT

Facility layout is an important factor in designing of process plants such as petrochemical units and refineries. An appropriate design of layout ensures proper performance of corresponding departments as well as providing an equilibrium between large number and sometimes inconsistent structural design constraints. In this research, a mixed integer non-linear programming (MINLP) formulation is proposed for process plant layout problem, considering the toxic release risk and possible scenarios of fire, explosion and the domino effects of them. Then the Bat metaheuristic algorithm was employed to solve it. Finally, the model was implemented on 6th refinery, unit 101 of Iran's South Pars gas field, and the results showed the effectiveness of the model, in costs reduction and safety improvement.

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1. Introduction

Process industries are chemical production units in which the final products are continuously generated through chemical and biological processes or separating out from raw materials. Engineering studies in order to set the placement ordering and the layout of the units and equipment, is one of the main factors for a process plant, playing a fundamental role in raising safety levels of these sites, providing economic conditions in the context of costs, and optimizing the utilization of these facilities.

From an economic perspective, some believe that piping costs may include up to 80% of total installation costs, in case of inappropriate layout of a unit (Peters et al., 1968). Also, it can be concluded that 15% to 70% of total operation costs in a process unit depends on the way of facilities layout together (Tompkins et al., 1996). In terms of safety, the role of incident prevention seems to be much more significant comparing with reaction to accidents, as almost all of the processing units deal with extremely dangerous materials such as toxic and high potential for fire or explosion substances (Finch and Lees, 1997). A proper layout can prevent occurrence of these incidents to a large extent.

* Corresponding author.

E-mail addresses: EbrahimLatifi@engineer.com (S.E. Latifi),

E.Mohammadi@iust.ac.ir (E. Mohammadi), N.KhakzadRostami-1@tudelft.nl (N. Khakzad).

http://dx.doi.org/10.1016/j.compchemeng.2017.05.022 0098-1354/© 2017 Elsevier Ltd. All rights reserved. Ideally, plant locating and layout placement should establish a balance between risks and costs (Grossel, 2004). Most previous researches in the field of plant layout design were generally based on personal experiences (Anderson, 1982; Arinze and Banerjee, 1992; House, 1969; Kern, 1977, 1978; Mecklenburgh, 1982a, 1982b, 1985). However, in the last three decades, articles also were published which attempted to do this through mathematical programming and applying optimization techniques. In the way that firstly a few researchers developed some procedures based on fundamental location model and methods (and common heuristic algorithms) (Mannan and Lees, 2005; Mecklenburgh, 1973) and other researches provided models that mainly focused on economic aspects of layout (Georgiadis and Macchietto, 1997; Jayakumar and Reklaitis, 1994, 1996).

In the following years, financial risk (Penteado and Ciric, 1996) and total exceeding amount of safety distance described by Mond (Castell et al., 1998) has been added to these models alongside the other objective functions such as total length of pipes connecting units, total costs of land required for layout, in order to achieve a more prominent role of security in layout problems. Later, some indexes were joined including risk measure index like human risks (Han et al., 2013), and Dow fire and explosion index (AIChE, 1994; Patsiatzis et al., 2004).

Some scholars suggested dividing manufacturing process of chemical products into sub processes (modules) and performing facility siting in each module at first. Then locating these arranged modules in the factory land. Both the equipment layout inside the







| 2 | 5 | |
|---|---|---|
| 2 | 2 | 3 |

| Nomenclature | | | |
|--|---|--|--|
| Parameters | | | |
| A;, B;, C; | Dimensions for the facility <i>i</i> | | |
| Area: | Cross-sectional area of the facility <i>i</i> | | |
| CALI | Direct asset loss cost for the failure of the facility <i>i</i> | | |
| C_{FCC} | Environmental cleanup cost for the failure of the | | |
| €CC,I | facility i | | |
| Стина | Human health loss cost for the failure of the facility | | |
| <i>сппL,i</i> | i | | |
| Cf | Compensation cost to pay per fatality | | |
| $C^{Sa} C^{Sb}$ | Cost unit factors for the height support of the facility | | |
| c_i, c_i | <i>i</i> | | |
| C^{P} | Cost per length unit for the pipe k | | |
| C_k | Cost per square meter of land | | |
| D_{ii}^{HO} | Minimum horizontal distance between facilities <i>i</i> | | |
| ŋ | and <i>i</i> | | |
| DVE | Minimum vertical distance between facilities <i>i</i> and | | |
| 2 ij | i | | |
| Fe | J Minimum elevation of facility i | | |
| E _i En | Explosion energy for the facility <i>i</i> | | |
| $F_{x}^{x} F_{y}^{y} F_{z}^{z}$ | Z Relative positions of the nozzle <i>n</i> | | |
| $K^{d}(\nu)$ | Nozzle destination for the nine k | | |
| $K^{0}(k)$ | Nozzle origin for the nine k | | |
| N ^{Fa} | Number of facilities | | |
| NNZ | Number of nozzles | | |
| N ^{Pipe} | Number of pipes | | |
| FS | Facility state | | |
| N ^{int} | Number of total element | | |
| Pa | Barometric pressure | | |
| Poi | Expected population in the facility <i>i</i> | | |
| $Q_r^x, Q_r^y, 0$ | Q_r^z Relative positions of the releaser point r | | |
| $S_{\alpha}^{\Delta x}, S_{\alpha}^{\Delta y}$ | N ^{int} - vectors to define quadrant position | | |
| U ^{FS} | Safety distance due to the facility state | | |
| a° , b° , c° | Parameters for exponential decay | | |
| a ¹ , b ¹ | Constant and variable costs for placement of each | | |
| 2 2 | square meter of facility per height | | |
| a_{FS}^2, b_{FS}^2 | Constant of the probit function based on facility | | |
| 1 ch | state | | |
| df _i " | Flame envelope produced by the primary unit <i>i</i> in | | |
| c | the scenario <i>n</i> | | |
| Jr m | Nevinum slope in element or | | |
| m_{α} | Fundational life time of the plant | | |
| ι _[τ | Capital recovery factor for period t, and interest rate | | |
| $v_{t_l,IR}$ | IR | | |
| IR | Interest rate | | |
| M | a large number | | |
| X | Something factor | | |
| ν | Annual probability of domino event occurrence | | |
| i(p) | the facility on which the nozzle <i>p</i> is located | | |
| (1) | | | |
| Binary V | ariables | | |
| $B_{ij}^{n,G}$ | the binary variable related to position of the facili- | | |
| | ties <i>i</i> and <i>j</i> in situation G under scenario h | | |
| $S_{i,r,\alpha}$ | the binary variables related to positioning of the | | |
| | facility <i>i</i> in element α with respect to the release | | |
| | point r | | |
| w_{ij}^x, w_{ij}^y, T | w_{ij}^{z} the binary variables for the relative position | | |
| - | between facilities <i>i</i> and <i>j</i> | | |
| <i>w</i> _{it} | the binary variable for rotation of the facility <i>i</i> in the | | |
| | manner <i>t</i> | | |

| Positive Variables | | | |
|--|--|--|--|
| X, Y, Z | Size of the box that encloses the plant layout | | |
| x_i, y_i, z_i | Position of the center of the facility <i>i</i> | | |
| x'_{i}, y'_{i}, z'_{i} | Auxiliary variables | | |
| $x^N y^N 7$ | ^N Position of the nozzle n | | |
| \sqrt{RP} \sqrt{RP} | z^{RP} Position of releaser point r | | |
| x_r, y_r, C^S | 2_r Position of releaser point <i>i</i> | | |
| | ⁷ Manhattan distance between the contour of facili | | |
| $d_{ij}^{*}, d_{ij}^{*}, d_{ij}^{*}$ Manhattan distance between the centers of facili- | | | |
| <i>c c</i> | ties <i>i</i> and <i>j</i> | | |
| xf _{ij} , yf _{ij} , 2 | zf_{ij} Variable for relative situation facilities <i>i</i> and <i>j</i> in | | |
| en en | each direction | | |
| $l_{k}^{x+}, l_{k}^{x-}, l_{k}^{x-}$ | $b_k^{p+}, b_k^{p-}, l_k^{2+}, l_k^{2-}$ Length of pipe k using manhattan distance | | |
| dr_{ir}^{x}, dr_{ir}^{y} | dr_{ir}^{z} Manhattan distance between the center of | | |
| | facility <i>i</i> and releaser point <i>r</i> | | |
| D_{ii}^{Min} | Minimum distance between surface of facilities <i>i</i> | | |
| ij | and <i>i</i> | | |
| DHS ^{h,G} | Domino hazard score between facilities i and j in | | |
| ij | scenario h and situation G | | |
| DHIii | Domino hazard index between facilities <i>i</i> and <i>j</i> | | |
| Ro | Characteristic distances between facilities <i>i</i> and <i>i</i> | | |
| ΔP_{ii} | Overpressure affected the facility <i>i</i> generated by the | | |
| —- y | facility i | | |
| Pr | Probit variable | | |
| P ^{BW} | Damage probability of the facility <i>i</i> caused by blast | | |
| - ij | wave of the facility i | | |
| (1) | Credit factor for domino escalation | | |
| w_{ij} | credit factor for domino escalation | | |
| Subscripts | | | |
| i, j | Indexes for facilities $(i = 1,, N^{Fa})$ | | |
| p, q | Indexes for nozzles $(p = 1,, N^{NZ})$ | | |
| k | Index for pipes $(k = 1,, N^{Pipe})$ | | |
| r | Index for facilities that with possible release point | | |
| | $(r \in R)$ | | |
| α | Index for direction slice ($\alpha = 1,, N^{int}$) | | |
| h | Index for fire and explosion scenarios $(h =$ | | |
| | $\{FF, FB, IF, PF, BW\}$ | | |
| t | Index for rotations $(t = 1,, 8)$ | | |
| | | | |

modules and the modules layout in the factory site are executed by a similar model (Guirardello and Swaney, 2005).

Since most of the large scale process plant layout problems can't be solved using the exact methods, there have been efforts to develop heuristic algorithms to solve them (Xu and Papageorgiou, 2007a, 2007b, 2009). These methods convert the layout problems to smaller sub-problems with a solvable complex integer programming format by using iterative algorithms, based on the described model of Papageorgiou and Rotstein (1998).

In last few years, the annual amount of damage and loss expected for each layout is calculated as the sum of expected values of probability for the amount of damage caused by incident in each unit (Caputo et al., 2015); and assumption of having the potential toxic release (Vázquez-Román et al., 2010) and various methods for calculating different scenarios of domino events in layout problem (de Lira-Flores et al., 2014; López-Molina et al., 2013) have been introduced, too. All of these studies used the restrictive assumptions (involving considering the layout in a two-dimensional form or considering pre-positioned facilities) to reduce the scale of the problems, and included just one of the incident modes. Thus, it seems necessary to provide a study in order to achieve a comprehensive model which contains methods for calculating the Download English Version:

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