ARTICLE IN PRESS

Acta Biomaterialia xxx (2015) xxx-xxx

Contents lists available at ScienceDirect

Acta Biomaterialia



journal homepage: www.elsevier.com/locate/actabiomat

In vivo study of magnesium plate and screw degradation and bone fracture healing

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ARTICLE INFO

18 Article history:

- 19 Received 18 August 2014
- 20 Received in revised form 10 February 2015
- 21 Accepted 13 February 2015
- 22 Available online xxxx
- 23 Keywords:
- 24 Magnesium
- 25 Fixation devices
- 26 Fracture fixation MicroCT
- 27 28

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ABSTRACT

Each year, millions of Americans suffer bone fractures, often requiring internal fixation. Current devices, like plates and screws, are made with permanent metals or resorbable polymers. Permanent metals provide strength and biocompatibility, but cause long-term complications and may require removal. Resorbable polymers reduce long-term complications, but are unsuitable for many load-bearing applications. To mitigate complications, degradable magnesium (Mg) alloys are being developed for craniofacial and orthopedic applications. Their combination of strength and degradation make them ideal for bone fixation. Previously, we conducted a pilot study comparing Mg and titanium devices with a rabbit ulna fracture model. We observed Mg device degradation, with uninhibited healing. Interestingly, we observed bone formation around degrading Mg, but not titanium, devices. These results highlighted the potential for these fixation devices. To better assess their efficacy, we conducted a more thorough study assessing 99.9% Mg devices in a similar rabbit ulna fracture model. Device degradation, fracture healing, and bone formation were evaluated using microcomputed tomography, histology and biomechanical tests. We observed device degradation throughout, and calculated a corrosion rate of 0.40 ± 0.04 mm/year after 8 weeks. In addition, we observed fracture healing by 8 weeks, and maturation after 16 weeks. In accordance with our pilot study, we observed bone formation surrounding Mg devices, with complete overgrowth by 16 weeks. Bend tests revealed no difference in flexural load of healed ulnae with Mg devices compared to intact ulnae. These data suggest that Mg devices provide stabilization to facilitate healing, while degrading and stimulating new bone formation.

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52 1. Introduction

Each year there are over 6 million bone fractures reported in the U.S. [1], approximately one third of which require internal fixation devices to help facilitate healing [2]. Currently, permanent and inert metals like titanium (Ti) alloys and stainless steel remain the gold standard for internal fixation devices; however, these materials are associated with various long-term complications such as interference with skeletal growth (particularly for pedi-60 atrics), tissue irritation, infection, interference with radiological imaging, and unfavorable esthetics (primarily for craniofacial

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http://dx.doi.org/10.1016/j.actbio.2015.02.010

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implants) [3–7]. For these reasons, permanent fixation devices may necessitate invasive removal surgeries, increasing patient burden and risk, and draining valuable hospital resources [8,9]. To mitigate these concerns, resorbable polymer devices have been developed; however their mechanical properties often limit them as viable options for load-bearing applications [10]. Furthermore, studies have reported long-term foreign body reactions associated with polymeric device degradation, likely due to their acidic degradation products [3,11,12]. For these reasons, there remains a need to develop novel fracture fixation devices which mitigate longterm complications and eliminate the need for removal surgeries.

Unlike permanent metals and resorbable polymers, degradable magnesium (Mg) alloys provide a unique combination of strength and degradation. For these reasons, Mg alloys are being explored for various craniofacial and orthopedic applications. Interestingly,

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Please cite this article in press as: Chaya A et al. In vivo study of magnesium plate and screw degradation and bone fracture healing. Acta Biomater (2015), http://dx.doi.org/10.1016/j.actbio.2015.02.010

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77 Mg alloys were first attempted as orthopedic devices over a centu-78 ry ago. Early Mg-based devices proved to be biocompatible, with 79 low rates of infection; however, rapid degradation of Mg that is 80 characteristic and to be expected with the current metallurgical 81 knowledge known to date caused excessive hydrogen gas forma-82 tion which ultimately prevented their clinical success [13,14]. 83 Since these initial investigations, numerous advancements in 84 alloying and corrosion control have been achieved. These advancements allow Mg and its alloys to be tailored to accommodate the 85 86 desired mechanical properties and degradation behavior.

87 Numerous in vitro and in vivo studies have demonstrated the 88 biocompatibility and osteoconductivity of these materials. Indirect assays, in which cells are exposed to media treated with Mg corro-89 90 sion products, have shown cell viability with low concentrations of 91 degradation product [3,13,15]. Similarly, direct assays, in which 92 cells are cultured directly on Mg alloys, have shown cytocom-93 patibility in the presence of ongoing Mg degradation [3,13,15]. 94 Importantly, studies assessing Mg implants in endosseous sites, such as guinea pig [16], rat [17], and rabbit femora [18] have 95 shown biocompatibility and normal foreign body response for var-96 97 ious Mg alloys. In addition, several studies have shown high min-98 eral apposition rates and increased bone mass and mineral 99 density surrounding Mg implants in bone [10,16,19,20].

100 These data support the use of Mg implants as orthopedic 101 devices; however there remains a lack of in vivo data assessing the-102 se materials as actual fixation plates and screws. For these reasons, we previously conducted a pilot study to evaluate Mg fixation 103 plates and screws using a rabbit ulna fracture model [21]. In the 104 105 pilot study, we compared 99.9% Mg plates and screws to clinical-106 ly-used Ti devices, studying the effect of Mg degradation on 107 fracture healing. Our pilot study results showed no significant 108 difference in healing of fractures fixed with Mg or Ti devices. Inter-109 estingly, we also observed bone formation above the Mg, but not 110 Ti, plates and screws.

111 In order to validate this pilot study data, we have conducted a 112 more thorough follow-up assessment presented herein. In the pre-113 sent study, we aim to test our hypothesis that ongoing Mg device 114 degradation will continue to stimulate osteogenic differentiation 115 of local cell populations such as human bone marrow stromal cells 116 (hBMSCs) and/or periosteal cells. In turn, this differentiation will result in local bone formation, providing additional fracture stabi-117 lization. Through this process, it is anticipated that Mg devices will 118 be gradually replaced by bone growth, mitigating risk of long-term 119 120 complications and device removal surgeries. To test this hypothesis, we have performed a thorough assessment of the degradation 121 122 behavior and biological effect of Mg fixation devices. Specifically, 123 we have designed and tested Mg fixation plates and screws in a 124 rabbit ulna fracture model. Our results have confirmed our pilot 125 study observations of new bone formation around Mg devices, 126 especially above the devices where the periosteum and muscle tis-127 sue was present. In addition, we observed no inhibition of fracture healing. Mechanical testing demonstrated that healed fractures 128 fixed with Mg devices responded similarly to healthy controls 129 when subjected to three point bending. Taken together, these data 130 131 demonstrate the efficacy of Mg fixation devices in a load bearing fracture site. 132

133 2. Materials and methods

134 *2.1. Device design and development*

Fixation devices (Fig. 1) were machined with 99.9% pure Mg (Goodfellow, Coraopolis, PA). All devices were designed to accommodate rabbit ulnar geometry. Plates were 20×4.5 mm with a thickness of 1–1.5 mm. Screws were 7 mm in length, with a shaft

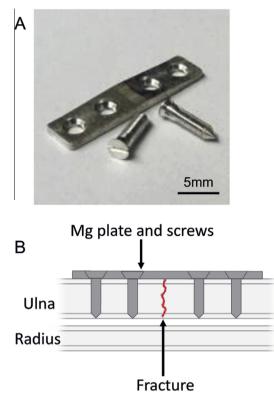


Fig. 1. Magnesium fixation plate and screws. Digital image showing devices prior to implantation (A). Schematic showing device placement with fractured ulna (B).

outer diameter of 1.75 mm and shaft inner diameter of 1 mm. Prior139to implantation, devices were cleaned by sonicated washes in pure140acetone and ethanol, followed by sterilization with gamma radia-141tion $(2 \times 10^6 \text{ cGy}, 23.5 \text{ Gy/min}, \text{ cesium 137 source, Mark I 68, JL142Shepherd and Associates, San Fernando, CA).143$

2.2. In vivo implantation

All animal experiments were approved by the University of 145 Pittsburgh's Institutional Animal Care and Use Committee. 12 146 New Zealand White rabbits (19 weeks of age, 3.5 ± 0.2 kg) were 147 used in this study. Both ulnae (right and left) of all animals were 148 used, providing a total of 24 surgical sites. Each time point consist-149 ed of 6 rabbits (12 surgical sites). Prior to surgery, animals were 150 anesthetized and forearms were shaved and disinfected. A 2 cm 151 incision was made over the ulna. Overlying skin and muscle was 152 carefully retracted to expose the ulna. A complete ulnar osteotomy 153 (0.5–1 mm thick) was created using a hand held drill. A fixation 154 device consisting of one plate and four screws was then placed 155 to stabilize the fracture. The incision was closed in layers with 156 sutures and left un-casted. Animals were monitored daily for gen-157 eral behavior, movement, and food and water intake. In addition, 158 forearms were checked thoroughly by visual inspection and gentle 159 palpation for signs of infection or subcutaneous gas pocket forma-160 tion. Based on consultation with the University of Pittsburgh's 161 Division of Laboratory Animal Resources, observable gas pockets 162 were removed with a sterile syringe. All gas pocket formations 163 and removals were documented throughout the study. 164

2.3. X-ray imaging

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X-ray imaging was used to monitor device placement and fracture healing throughout the study. All animals received X-rays immediately following surgery and every 2 weeks thereafter.

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