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## Original Research Article

# A two dimensional approach for modelling of pennate muscle behaviour

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## 1. Introduction

The human movement system consists of striated skeletal muscles that have different architectures. Among these muscles are fusiform muscles and pennate muscles (unipennate muscles, bipennate muscles and multipennate muscles) [1]. The fusiform muscle fibres run generally parallel to the muscle axis (it is line connecting the origin tendon and the insertion tendon). The unipennate muscle fibres run parallel to each other but at the pennation angle to the muscle axis [2]. The bipennate muscle consists of two unipennate muscles that run in two distinct directions (i.e. different pennation angles). The multipennate muscle is composed of a few bundles of fibres that run in distinct directions.

Q2 From the physiology point of view, the unipennate muscle consists of three parts: the muscle insertion (insertion tendon), the belly (muscle fibres), and the muscle origin (origin tendon). It is assumed that during contraction the belly maintains the isovolume, each tendon moves only along its axis and muscle fibres become more pennated, i.e. the pennation angle is increased [3].

The spatial arrangement of pennate muscle fibres determines the muscle fibres length, the lengths of tendons and mechanical properties of muscle. That is why the contractile characteristic (i.e. force-generating capacity) depends on the pennation angle [2]. Moreover, one should take into consideration that a real pennate muscle is a non-homogenous structure: the distal muscle fascicles tend to contract more (i.e. they act at greater pennation angles) than the more proximal muscle fascicles.

Applying an imaging technique, such as nuclear magnetic resonance (MRI) or ultrasonography (US), with a motion capture technique, one might perform in vivo non-invasive measurements to estimate volumes of muscles, muscle fibres lengths and pennation angles [2]. However, one should perform invasive measurements to obtain [4]: 1) parameters describing mechanical properties of chosen muscles (by applying tensile tests and sonomicrometry); 2) muscle morphology and its architecture evaluated at the microscopic level (by using a muscle biopsy); 3) muscle static characteristic (length-force dependence); 4) muscle dynamic characteristic (velocity-force dependence); 5) muscle-tendon parameters used in the Hill-type muscle model. That is why a very limited amount of data describing mechanical properties of pennation muscles can be found in literature.

To model behaviour of pennate muscle one should take into consideration that spatial arrangement of muscle fibres influence mechanical properties and contractile properties of this muscle. Nowadays, to describe pennate muscle function in muscle biomechanics there are applied rheological models: Hill-type muscle models and Hill-Zajac muscle models [3,5–11]. However, application of these models is very limited due to

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66 problems related to the obtainment of model parameters.  
 67 To deal with these problems an optimization technique  
 68 (i.e. mathematical optimization) can be applied. However, in  
 69 this case the problem of compatibility between chosen cost  
 70 function and an alive muscle physiology should be considered.

71 The three-dimensional (3D) muscle models that take into  
 72 consideration spatial muscle fibres arrangement are also  
 73 proposed [12–18]. To apply chosen 3D muscle model, one needs  
 74 to define the 3D geometry, interaction between components of  
 75 this model (e.g. lateral transmission of tension between muscle  
 76 fibres), boundary conditions and material properties according  
 77 to the principles of continuum mechanics. The fundamental  
 78 problem consists in identification of material properties because  
 79 of constrained range of alive tissue experiments. Moreover,  
 80 these 3D muscle models are applied for static or quasi-static  
 81 solutions and are incompatible to solve forward dynamics tasks  
 82 because these models are computational expenses.

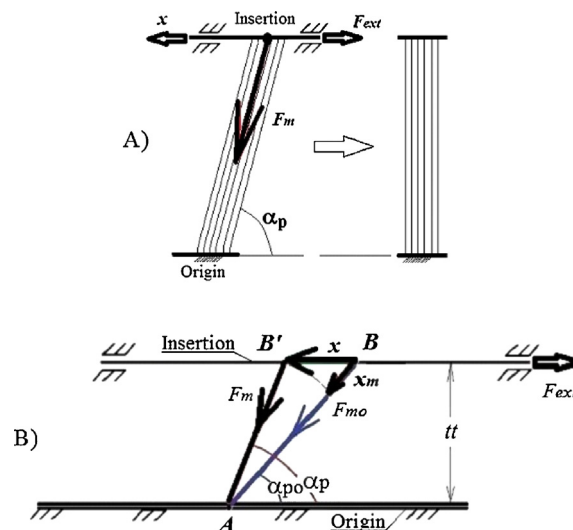
83 Deliberating an application of high-mentioned Hill-type  
 84 muscle models, Hill-Zajac muscle models or three-dimen-  
 85 sional (3D) muscle models, one should define for each muscle  
 86 examined: muscle static characteristic, muscle dynamic  
 87 characteristic, tendon static characteristic, physiological cross  
 88 section area (PCSA), optimal muscle length and optimal  
 89 muscle force. Due to limited possibility of an alive muscle  
 90 examination, these characteristics and parameters are defined  
 91 by making additional assumptions and presuming that a  
 92 muscle force can be predicted on the base of the value of PCSA  
 93 and maximum muscle stress or/and a static characteristic of  
 94 sarcomere (relationship between a sarcomere length and  
 95 isometric force of this sarcomere). Moreover, in the case of  
 96 pennate muscle modelling one should take into consideration  
 97 that muscle force depends on the spatial arrangement of  
 98 muscle fibres and that is why above-mentioned characteristics  
 99 and parameters must be estimated for each pennate muscle in  
 100 the range of its physiological behaviour.

101 To model behaviour of chosen flat pennate muscle one  
 102 should take into account a planar kinematics, which is  
 103 described by using at least two parameters (two-dimensional  
 104 approach). The purpose of this study was to elaborate a two-  
 105 dimensional approach for unipennate and bipennate striated  
 106 skeletal muscle modelling by applying a method described in  
 107 [19]. According to this approach, a behaviour of chosen flat  
 108 pennate muscle is modelled as a rheological system composed  
 109 of serially linked passive and active fragments having different  
 110 mechanical properties. Each fragment is composed of three  
 111 elements: mass element, elastic element and viscous element.  
 112 Each active fragment furthermore contains the contractile  
 113 element. Proposed approach takes into consideration that  
 114 muscle force depends on a planar arrangement of muscle  
 115 fibres. The scope of presented study was to perform numerical  
 116 researches and to elaborate a concept of experimental  
 117 verification.

## 118 2. Method of modelling

### 119 2.1. Principles of pennate muscle modelling

120 Assuming a planar deformation schema of unipennate muscle  
 121 shown in Fig. 1, the mathematical models of unipennate



122 **Fig. 1 – Deformation schema of unipennate muscle: A)**  
 123 **directions of acting of external force  $F_{ext}$  and contractile**  
 124 **muscle force  $F_m$  towards the muscle insertion displacement**  
 125  **$x$ ; B) schema of deformation of unipennate muscle ( $AB$  – the**  
 126 **initial length of muscle (before contraction);  $AB'$  – the finish**  
 127 **length of muscle (after contraction);  $F_{m0}$  – initial contractile**  
 128 **muscle force at the length of muscle equals  $AB$ ;  $F_m$  – finish**  
 129 **contractile muscle force at the length of muscle equals  $AB'$ ;**  
 130  **$\alpha_{po}$  – the pennation angle before contraction (at the length of**  
 131 **muscle equals  $AB$ );  $\alpha_p$  – the pennation angle after**  
 132 **contraction (at the length of muscle equals  $AB'$ );  $x_m$  – change**  
 133 **of muscle length that is equal to the difference of the length**  
 134  **$AB$  and the length  $AB'$ ) [19].**

122 muscle and bipennate muscle were created. According to this  
 123 deformation schema, the muscle contraction occurs in the  
 124 plane (two-dimensional space) along muscle fibres directed at  
 125 the pennation angle  $\alpha_p$  towards the line connecting the muscle  
 126 insertion (it is a movable part with one degree of freedom) and  
 127 the muscle origin (it is a non-movable part). It is assumed that  
 128 during muscle contraction the muscle width  $tt$  is constant  
 129 (according to [20]) and muscle fibres generate a contractile  
 130 muscle force  $F_m$ , which causes the displacement of muscle  
 131 insertion  $x$  and counterbalances an external force  $F_{ext}$ :

$$132 F_{ext} = F_m \cdot \cos \alpha_p \quad (1) \quad 133$$

134 During contraction the muscle fibres are shortening and the  
 135 muscle insertion is translated from the point  $B$  to the point  $B'$   
 136 (the distance  $BB'$  is equal to the muscle insertion displacement  
 137  $x$ ). It causes the change of pennation angle: the initial value of  
 138 pennation angle  $\alpha_{po}$  (at the length of muscle equals  $AB$ ), is  
 139 changed to the value  $\alpha_p$  (at the length of muscle equals  $AB'$ ).  
 140 Analyzing the deformation schema of unipennate muscle, the  
 141 following geometric relation can be derived:  
 142

$$143 tt = AB \cdot \cos \alpha_{po} = AB' \cdot \cos \alpha_p. \quad (2) \quad 144$$

145 Taking into consideration a deformation schema of  
 146 unipennate muscle, five rheological models were created [19]:  
 147

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