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# Applied Catalysis B: Environmental



# Effects of the pretreatment of  $CuNi/SiO<sub>2</sub>$  on ethanol steam reforming: Influence of bimetal morphology



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## A B S T R A C T

Previous research shows that bimetallic CuNi/SiO<sub>2</sub> catalysts prepared by NaBH<sub>4</sub> reduction perform well in ethanol steam reforming (ESR) compared to their monometallic counterparts. More importantly, these bimetallic catalysts yield simple products of only  $H_2$ , CO<sub>2</sub>, CO<sub>2</sub> and CH<sub>4</sub>, at high ethanol conversions. The as-prepared catalysts contain mainly alloy nanoparticles. This study shows that ESR performance can be further improved by catalyst pretreatment, i.e., calcination at 400 ◦C followed by reduction at 350 ◦C (coded hereafter as calc-CuNi-R350). Characterization using in situ X-ray diffraction (XRD) and X-ray absorption fine structure (XAFS) indicates that the calc-CuNi-R350 catalyst contains Cu-rich nanoparticles in close proximity to NiO nanocrystals. Compared to the uncalcined but reduced catalyst (asis-CuNi-R350), the calc-CuNi-R350 catalyst had higher turnover frequency for ethanol conversion and for acetaldehyde conversion and lower selectivity to  $CH_4$  formation. Increasing the steam/ethanol ( $S/E$ ) ratio from 6 to 9 significantly suppresses CH4 formation from this calc-CuNi-R350 catalyst. The results of this study suggest that the interface between NiO and Cu-rich nanoparticles improves ASR/AD (acetaldehyde steam reforming/acetaldehyde decomposition) selectivity via stabilizing the methyl (or methylene) groups from the decomposition of acetaldehyde intermediate and consequently decreases the probability of CH<sub>4</sub> evolution. If CH<sub>4</sub> evolution is suppressed, the ESR reaction produces only H<sub>2</sub>, CO, and CO<sub>2</sub>. This makes ESR an attractive sustainable route for  $H_2$  production.

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## **1. Introduction**

Currently, methane steam reforming is largely used for commercial hydrogen production and methanol steam reforming (MSR) is extensively studied for boosting devices such as fuel cells. Bioethanol is considered a carbon-neutral fuel and therefore ethanol steam reforming (ESR) is a sustainable method for producing hydrogen. ESR derives many side products other than the expected  $H_2$  and CO<sub>2</sub> and its reaction pathways and mechanism have recently been reviewed [\[1\].](#page--1-0) The more complicated reaction pathway of ESR compared to MSR arises from the necessity to break the C-C bond of ethanol. The much-used Cu catalysts for MSR are ineffective to break the C-C bond while Ni, Co, Ir, and Rh are effective [\[2,3\].](#page--1-0) Ni is relatively inexpensive and therefore many tests of Ni catalysts for ESR have been reported. However, coke formation is severe in ESR over Ni catalysts. Two approaches are typically adopted to resolve this problem, namely, using bimetal (or multi-metal) catalysts and using active support such as  $CeO<sub>2</sub>$ which can contribute lattice oxygen to enhance steam reforming. Trimm  $[4,5]$  mentioned that CeO<sub>2</sub> support can decrease the

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coke formation over Ni catalysts during steam reforming. Choi et al.  $[6]$  reported that Ni/CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> had a lower coking tendency than  $Ni/Al<sub>2</sub>O<sub>3</sub>$  during isooctane autothermal reforming. When a second metal is used, the type of metal, the composition and the alloy formation are key factors determining the catalytic performance [\[7\].](#page--1-0) Different metals have been reported to cope with Ni for ESR, such as Co, Cu, Rh, Pt. Among these second metals, Cu is relatively inexpensive and it enhances ESR performance with decreased coking tendency  $[8-14]$ . In general, ESR performance can be rated by the ethanol conversion rate, the hydrogen yield and the coking tendency of catalyst. We reported previously that a Cu/Ni ratio of 1 resulted in better ESR performance than other Cu/Ni composition over the CuNi/SiO<sub>2</sub> catalyst prepared by NaBH<sub>4</sub> reduction [\[11\].](#page--1-0) However, the optimal Cu/Ni composition seems to depend on the type of support, the catalyst preparation method and even the operating temperature. For example, Fierro et al. [\[15\]](#page--1-0) reported that Cu doped  $Ni/Al<sub>2</sub>O<sub>3</sub>$ showed the highest  $H_2$  selectivity for oxidative ESR at 923 K but it became the worst comparing to that doped with Zn, Fe, and Cr when operated at 1073 K. Mariño et al.  $[8-10]$  examined the effect of adding Cu to  $4\%$ Ni/K–Al<sub>2</sub>O<sub>3</sub> and reported that 2% Cu addition showed the highest hydrogen yield. Wang reported that 10%Ni-5%Cu/MgO-Al<sub>2</sub>O<sub>3</sub> was superior to catalysts with different Cu/Ni ratio [\[16\].](#page--1-0) De Rogatis et al. [\[14\]](#page--1-0) reported that the ESR

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product distribution was not significantly changed by the Cu/Ni ratio of  $Al_2O_3$ -supported CuNi catalysts. The formation of Cu–Ni alloy was considered beneficial for ESR [\[12,14,17\].](#page--1-0) However, the different Cu/Ni ratios reported in these references imply a need to resolve the active bimetallic structure such that the catalyst can be improved further.

The other approach utilizes the metal–support interaction to enhance the ESR performance and the stability of Ni catalysts. Support can have significant influence on the catalytic performance; for example, using acidic support can cause more dehydration and dehydrogenation during ESR which lead to high coking tendency. Additives such as K, Mg, and La are frequently used to modify  $Al_2O_3$  support where an optimal amount of basic additives is frequently sought after. Youn et al. [\[18\]](#page--1-0) reported that the best oxidative ESR performance can be obtained when using an intermediate acidity support for Ni catalysts, whereas Furtado et al. [\[19\]](#page--1-0) reported that the acidity of support had no effect on the oxidative ESR over NiCu catalysts. Additives not only change acid–base property but can also influence Ni dispersion [\[20,21\],](#page--1-0) create a carbon reservoir [\[22\],](#page--1-0) or provide high-temperature sta-bility [\[21,23\].](#page--1-0) The multiple roles that the additive may play make its optimization a complex issue. Another type of supports used for suppressing coke formation is reducible oxides, where surface oxygen from oxide may participate and consequently enhance reaction performance. Xu et al. examined  $Ni/CeO<sub>2</sub>$  for ESR and proposed that  $Ce(III)$  at Ni-CeO<sub>2</sub> interface can provide OH groups to react with the methyl groups from C-C bond breaking over Ni metal  $[24]$ . However, formation of CH<sub>4</sub> and coke are still present under their test conditions. Similar uses of reducible oxide support for mono- and bi-metallic catalysts have been reported for enhancing ESR reaction. For example,  $Ce_xZr_{1-x}O_2$  has been exam-ined as the support for Ni [\[25\]](#page--1-0) and CeO<sub>2</sub> [\[26\],](#page--1-0) Ce<sub>x</sub>Zr<sub>1-x</sub>O<sub>2</sub> [\[27\],](#page--1-0) and CeGdO<sub>x</sub> [\[28\]](#page--1-0) for CuNi catalysts. In such cases of using reducible oxide support, increasing metal–support interface is usually the primary concern in catalyst preparation and the promoting effect is usually attributed qualitatively to the participation of surface oxygen.

Although different catalysts have been reported for ESR, ESR is not as efficient a hydrogen production reaction as MSR. ESR usually runs at a much higher steam ratio and a much higher reaction temperature than MSR. Though high reaction temperatures increase cracking activity, they also lead to coke formation and high energy consumption. The reverse water gas shift reaction is also favored at high temperatures, resulting in increased  $CO/H<sub>2</sub>$  ratio that may not be suitable for downstream uses such as fuel cells. Palma and co-workers [\[29–32\]](#page--1-0) recently addressed the advantages of decreasing the reaction temperature of ESR and  $Pt/CeO<sub>2</sub>$  and Pt-Ni/CeO<sub>2</sub> were reported as effective catalysts. Approaches such as using membrane reactor to promote ESR were also reported [\[33,34\]](#page--1-0) for decreasing the reaction temperature of ESR. Lower reaction temperatures are desirable and ideally, ESR products should include only  $H_2$ , CO, and CO<sub>2</sub>, as in the case of MSR. If successful, this would make ESR an effective and sustainable route for  $H_2$  production. Our previous report demonstrated that using Cu–Ni bimetallic catalysts can limit the ESR products to include only  $H_2$ , CO, CO<sub>2</sub>, and CH<sub>4</sub> [\[11\],](#page--1-0) and a reaction scheme (Scheme 1) was proposed. Reducing  $CH<sub>4</sub>$  formation is a prerequisite to simplifying Scheme 1 and improving ESR performance for  $H_2$  production. This study reports that  $CH_4$  formation can be reduced, though not eliminated, by changing the pretreatment of  $5\%$  Cu<sub>1</sub>Ni<sub>1</sub>/SiO<sub>2</sub> catalyst. Morphology characterization by TPR, XRD, and EXAFS suggests that mixed phases in  $Cu<sub>1</sub>Ni<sub>1</sub>/SiO<sub>2</sub>$  achieve more efficient ESR than the alloy phase. This is attributed to the enhanced acetaldehyde steam reforming and the enhanced water gas shift pathways of Scheme 1 by the presence of alloy–NiO interface.



**Scheme 1.** A simple ESR reaction pathway.

### **2. Experimental**

#### 2.1. Preparation of catalysts

Supported 5 wt.% Cu, Ni, and bimetallic Cu–Ni (1/1) catalysts were prepared [\[11\]](#page--1-0) by incipient-wetness impregnation of metal (Cu and Ni) nitrate (Aldrich, 98%) aqueous solution on  $SiO<sub>2</sub>$  support (Davison 952, 300 m<sup>2</sup>/g, used after calcinations at 550 °C). After impregnation, catalysts were dried at  $25^{\circ}$ C under rough vacuum generated by a rotary pump. Each catalyst was then dispersed in  $H<sub>2</sub>O$  and stirred for 10 min. A 5% NaB $H<sub>4</sub>$  (diluted from Aldrich, 98.5%) solution was then added drop-by-drop at room temperature until NaBH<sub>4</sub>/metal = 5 (molar ratio) [11]. After additional stirring for 30 min, the solid was recovered by centrifugation, washed thoroughly with  $H<sub>2</sub>O$  and then vacuum dried at room temperature. The supernatant was examined by ICP-AES and no loss of Cu or Ni was evident. The as-prepared catalysts (denoted as asis-) were then calcined in air at 400 $\degree$ C for 5 h (denoted as calc-).

#### 2.2. Characterizations

Temperature-programmed reduction (TPR) analysis was performed at  $5^{\circ}$ C/min using 10% H<sub>2</sub> in nitrogen and a TCD detector; the H2O formed during TPR was trapped by a molecular sieve column installed prior to the detector. The catalyst was typically purged by He at 50 °C till TCD became stable and then switched to  $H_2/N_2$  flow and the temperature was ramped. For metal surface area analysis, the catalyst was pretreated by  $H_2$  flow at the target temperature for 1 h, cooled to 25 °C under He, and then subjected to  $N_2O$  flow (50 mL/min) at 25 ◦C for 30 min. The catalyst bed was then purged with He and the  $O_{ad}$  from N<sub>2</sub>O adsorption was quantitatively analyzed by the  $H_2$  consumption in a subsequent TPR experiment. Metal dispersion was calculated by assuming an  $O_{ad}/M_S$  ratio of  $1/2$ , where  $M<sub>S</sub>$  represents the surface atoms of either Cu or Ni. This  $O_{\text{ad}}/M_S$  stoichiometry of 1/2 is typically used for the evaluation of  $Cu<sub>S</sub>$  but it was doubted for Ni<sub>S</sub> due to the possible exchange of surface and subsurface oxygen over Ni [\[35\].](#page--1-0) However, the metal dispersion obtained by assuming  $O_{ad}/M_S = 1/2$  is close to the calculated dispersion of Cu (or Ni) particles based on the average size obtained from XRD and TEM [\[11\].](#page--1-0)

In situ XRD was performed using the beamline BL01C at the National Synchrotron Radiation Research Center (NSRRC) in Hsinchu, Taiwan. The electron storage ring operated at 1.5 GeV with a beam current of 200 mA. The XRD pattern was recorded using a wavelength of 0.5167 Å for limited angular regions at room temperature. The recorded diffraction was corrected to that of  $Cu$  K $\alpha$ 1 radiation at a wavelength of 1.5418 Å. Diffraction patterns were obtained at a scan rate of 10°/min with steps of 0.05° in the 2 $\theta$  range from 20◦ to 90◦. EXAFS experiments were also performed using the BL17C beamline at the NSRRC. The Ni K-edge and Cu K-edge absorbance were measured sequentially in transmission mode at room temperature. In situ analysis was carried out in a stainless

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