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# Catalyzed soot filters (CSF) with $H_2S$ control function for lean $NO_x$ trap (LNT) systems

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#### ABSTRACT

A lean NOx trap (LNT) based emission control system typically consists of a LNT catalyst for NO<sub>x</sub> reduction and CO/HC oxidation and a catalyzed soot filter (CSF) for particulate filtration and CO/HC oxidation. During LNT's operation, it is required that sulfur compounds bound to the catalyst surface must be periodically removed in a reducing environment to recover the NO<sub>x</sub> storage sites. However, this desulfation process produces high levels of H<sub>2</sub>S emission, which must be suppressed. A series of catalyzed soot filters has been investigated for H<sub>2</sub>S suppression, and CuO based filters were found to be very efficient in converting H<sub>2</sub>S to SO<sub>2</sub>. Only 0.05 g/in<sup>3</sup> bulk CuO can convert 500 ppm H<sub>2</sub>S to SO<sub>2</sub> with 100% efficiency at GHSV = 34,000 h<sup>-1</sup> after a high temperature aging treatment (800 °C/16 h with 10% H<sub>2</sub>O). However, CuO was found to severely poison the precious metal (PGM) functions in the filter, dramatically reducing its CO/HC oxidation activity. The degree of poisoning is proportional to the CuO loading and also related to the proximity between CuO and the PGM within the filter microstructure. A zoned coating approach, where CuO and PGM occupy two non-overlapping zones in the axial direction, has been systematically investigated with both laboratory reactor and engine tests. The zoned H<sub>2</sub>S-CSFs, with CuO in the front of the filter and the PGM in the rear, were demonstrated to be effective catalysts that can fulfil both H<sub>2</sub>S suppression and CO/HC oxidation requirements.

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#### 1. Introduction

LNT and Selective Catalytic Reduction (SCR) are two commercially available  $NO_x$  control technologies for light-duty diesel vehicles to meet Euro 6 emission regulations [1]. Each system has certain advantages and disadvantages in cost and performance, and both are being explored to meet the Euro 6c regulations. When compared to a SCR system, a LNT system has limited efficiency at high speed/high load driving conditions (high  $NO_x$  flux) because of the limitation in  $NO_x$  storage capacity, and therefore it is mainly used for smaller cars. On the other hand, the LNT system has a lower total cost of ownership, which continues making it an attractive approach for further technology development [2]. In addition to  $NO_x$  reduction, a LNT catalyst is also a very effective Diesel Oxidation Catalyst (DOC) because it usually contains a high level of precious metals. A LNT-based system must also include a catalyzed

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http://dx.doi.org/10.1016/j.cattod.2016.12.043 0920-5861/© 2016 Elsevier B.V. All rights reserved. soot filter (CSF) for particulate filtration and other gas conversion functionalities (see Fig. 1).

A LNT catalyst accomplishes NO<sub>x</sub> abatement by decoupling of two separate processes, NO<sub>x</sub> storage in a lean period (normal diesel engine operation) and reduction of the stored NO<sub>x</sub> with a short (a few seconds) rich transient [3–5]. During the lean period, NO emitted from the combustion process is oxidized to NO<sub>2</sub> on a Pt catalyst, which is further converted to nitrate and stored on the basic components. During the rich period, the stored nitrate is liberated and reduced to N<sub>2</sub> in a way similar to NOx reduction on a Three-Way Catalyst (TWC). A conventional diesel engine exhaust is overwhelmingly lean with very high levels of O<sub>2</sub> (e.g., 10%). Typically, rich pulses are generated by in-cylinder post-injection of diesel fuel during the expansion stroke. Alkaline earth or alkali metals, such as barium, are typically used in commercial LNT formulations. Barium is a strong base which reacts with the acidic  $NO_x$  species very effectively to form  $Ba(NO_3)_2$ . However, the sulfur species in the exhaust, derived from diesel fuel and lubricating oil, also react with the barium component, forming BaSO<sub>4</sub>. Barium sulfate is more thermally stable than Ba(NO<sub>3</sub>)<sub>2</sub> by 45-60 kcal/mol between 200 and 700 °C [6], and, as a result, the LNT catalyst grad-

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Fig. 1. Schematic representation of catalyst configuration for the  $\rm H_2S$  suppression experiment.

ually loses its NO<sub>x</sub> storage capacity. To continue performing its deNO<sub>x</sub> function, sulfur must be removed from the poisoned LNT catalyst with a rich feed ( $\lambda$ <1) (or rich/lean alternating feed) at high temperatures (T>600 °C).

Extensive work on LNT desulfation and the resulting sulfur species have been reported [7–14]. High levels of H<sub>2</sub>S emission were often reported during the LNT desulfation either in lab or engine tests. The intensity of H<sub>2</sub>S formation depends on the lambda value of the desulfation feed and the mode of the desulfation operation, i.e. continuous rich vs. rich/lean modulation. The lower the lambda value (more reducing) of the desulfation feed, the higher the H<sub>2</sub>S formation (and higher desulfation efficiency). Continuous rich desulfation generates mostly H<sub>2</sub>S. The formation of H<sub>2</sub>S can be reduced by rich/lean modulation. For example, in an engine desulfation test, Erkfeldt et al. reported that the peak H<sub>2</sub>S formation was about 1150 ppm with  $\lambda$  = 0.95 at 700 °C, whereas the peak H<sub>2</sub>S was about 700 ppm with  $\lambda$  = 0.98 at the same temperature [7]. In an engine bench experiment, Asik et al. was able to reduce the peak H<sub>2</sub>S formation from 300 ppm obtained from a continuous desulfation to 160 ppm by using rich/lean modulation [8].

It is generally recognized that during LNT desulfation  $H_2S$  is formed via a two-step process: sulfate reduction to  $SO_2$  and further reduction of  $SO_2$  to  $H_2S$  [8,13,14]. The following chemical equations [Eqs. (1) and (2)] can be used to describe the desulfation process.  $H_2S$  is more likely to form than  $SO_2$ , as long as  $H_2$  is available, because the free energy of formation ( $\Delta G$ ) for Eq. (2) is -35.5 to -33.5 kcal/mol between 600 and 700 °C [6]. Thus, it is extremely difficult to avoid  $H_2S$  formation during LNT desulfation.

$$BaSO_4 + H_2 \rightarrow SO_2 + BaO + H_2O \tag{1}$$

$$SO_2 + 3H_2 \rightarrow H_2S + 2H_2O \tag{2}$$

H<sub>2</sub>S is a highly toxic gas, which exerts its toxic effects primarily as a central nervous system toxin (neurotoxin) and as a local irritant [15]. H<sub>2</sub>S has a rotten-egg smell with a smell threshold of 0.02 ppm. Although not one of the regulated emission gases, H<sub>2</sub>S as a byproduct of the LNT catalysis must be controlled. In the early days of TWC development, Ni was used as a H<sub>2</sub>S-getter to control H<sub>2</sub>S emission [16–18]. This concept was also reported for H<sub>2</sub>S control during LNT desulfation. By incorporating Ni as a component of the LNT catalyst, Asik et al. reported that the H<sub>2</sub>S emission over the FTP test cycle was reduced to 1/3 of that of a Ni-free LNT catalyst [8]. Using a stand-alone Ni-based H<sub>2</sub>S-trap placed behind a LNT catalyst, Elwart et al. conducted LNT desulfation experiments under rich/lean modulation conditions and were able to cut the maximum H<sub>2</sub>S emission by half [10]. Theis studied the desulfation with a LNT + (passive) SCR system, where the SCR catalyst is a Cu-zeolite [12]. The H<sub>2</sub>S emission was found to be significantly suppressed with the downstream Cu-zeolite based SCR catalyst.



Fig. 2. Filter-out SO<sub>2</sub> and H<sub>2</sub>S concentration profiles during LNT desulfation tests with a blank filter (A) and a CSF reference (B); GHSV (filter) = 34,000 h<sup>-1</sup>.



Fig. 3. Filter-out SO<sub>2</sub> and H<sub>2</sub>S concentration profiles during LNT desulfation tests with a blank filter (A) and a CuO-containing CSF (B); GHSV (filter) = 68,000 h<sup>-1</sup>.

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