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Recovering methane from quartz sand-bearing hydrate with gaseous CO₂

Shuanshi Fan, Xi Wang, Yanhong Wang, Xuemei Lang*

Key Lab of Enhanced Heat Transfer and Energy Conservation, Ministry Education, School of Chemistry and Chemical Engineering, South China University of Technology, Guangzhou 510640 Guangdong, China

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ABSTRACT

The replacement method by CO₂ is regarded as a new approach to natural gas hydrate (NGH) exploitation method, by which methane production and carbon dioxide sequestration might be obtained simultaneously. In this study, CO₂ was used to recover CH₄ from hydrate reservoirs at different temperatures and pressures. During the CO₂–CH₄ recovery process, the pressure was selected from 2.1 to 3.4 MPa, and the temperature ranged from 274.2 to 281.2 K. Calculating the fugacity differences between the gas phase and the hydrate phase for CO₂ and CH₄ at different conditions, it has found rising pressure was positive for hydrates formation process that was helpful for the improvement of CH₄ recovery rate. Rising temperature promoted the trend of CH₄ hydrate decomposition for the whole process of CO₂–CH₄ replacement. The highest recovery rate was 46.6 % at 3.4 MPa 281.2 K for CO₂–CH₄ replacement reaction in this work.

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1. Introduction

As the demand of the clean energy increasing with global climate change, natural gas attracted more attention for its high enthalpy upon combustion and low carbon emission [1]. Natural gas hydrate (NGH) is an energy resource for methane which total reserves in the world is estimated to range between 0.82×10^{13} and 2.10×10^{15} m³ CH₄ at standard temperature and pressure (STP) [2]. It have been found under the seabed or in the permafrost regions and expected to be a next-generation energy source [3,4]. The exploitation of NGH has very important social and economic effect, especially for shortage of energy nowadays. How to efficiently and safely exploit NGH remains a huge challenge. The simple exploiting methods include thermal stimulation, depressurization and inhibitors injection [5], which destroy the phase equilibrium of hydrate reservoir to cause hydrate decomposition. It would raise concerns about landslide and seabed ecosystem destruction.

The replacement method by use of CO₂ is regarded as a safe natural gas hydrate exploitation method, which injects CO₂ into the hydrate reservoir to recover CH₄ and sequesters CO₂ through storage in the deep sea. Compared to other exploiting methods, such as thermal stimulation, depressurization and inhibitors injection, replacement recovery method can maintain the ground mechanical stability and reduce water production by reformation of CO₂ hydrate [6]. Ebinuma [7] and Ohgaki et al. [8] proposed

the idea of replacing CH₄ with CO₂ from hydrate deposits in sea floor and studied the equilibrium components. Smith et al. [9] researched the possibility of exchanging hydrate with CO₂. And the viability of replacement natural hydrate with CO₂ had been proved both in thermodynamics and kinetics [10,11]. Bai et al. [12] studied CO₂ replacing CH₄ hydrate by molecular dynamics simulations explaining the processes consist of the methane hydrate dissociation and the CO₂ hydrate formation. They thought CO₂ hydrate formation would reduce the replacement ratio as the CO₂ hydrate layer hindered the mass transfer of CH₄ and CO₂ molecules.

Many studies indicated that replacement ratio was closely related to temperature and initial pressure. Li et al. [13] examined the gaseous CO₂ replaced CH₄ in hydrate reservoirs with the experimental conditions at 271.2 to 276.0 K and 2.8 to 3.25 MPa. It showed that the CH₄ recovery ratio was increased with the temperature rising, and growing the initial pressure of CO₂ could also improve the CH₄ recovery ratio. Ota et al. [14] got the same result that CH₄ recovery ratio increased with the rise of initial pressure under CO₂ liquid pressure, while CH₄ recovery ratio did not change at higher pressures above the CO₂ liquid pressure. Ota thought the replacement ratio was dependent on pressure and phase conditions. Yuan et al. [15] showed using liquid CO₂ could obtain more CH₄ than using gaseous CO₂ for replacement process. They thought the fugacity of liquid CO₂ decreases slightly during the replacement reaction compared with gaseous CO₂. Zhou et al. [16] divided the phase equilibrium diagram into four parts on replacement of CH₄ in hydrate with CO₂, and considered Part A was an optimal area for CO₂–CH₄ replacement process, which is shown in

* Corresponding author.

E-mail address: cexmlang@scut.edu.cn (X. Lang).

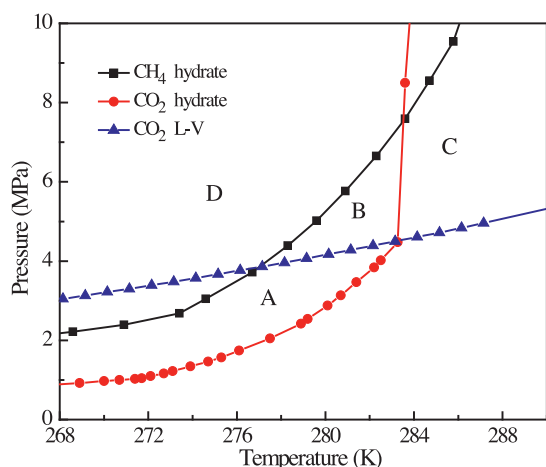


Fig. 1. Phase equilibrium diagram of replacement of CH₄ in hydrate with CO₂. Part A is CO₂ hydrate formation area with gaseous CO₂. Part B is CO₂ hydrate formation area with liquid CO₂. Part C is neither formation area of CH₄ hydrate and CO₂ hydrate. Part D is CH₄ hydrate and CO₂ hydrate simultaneous formation area.

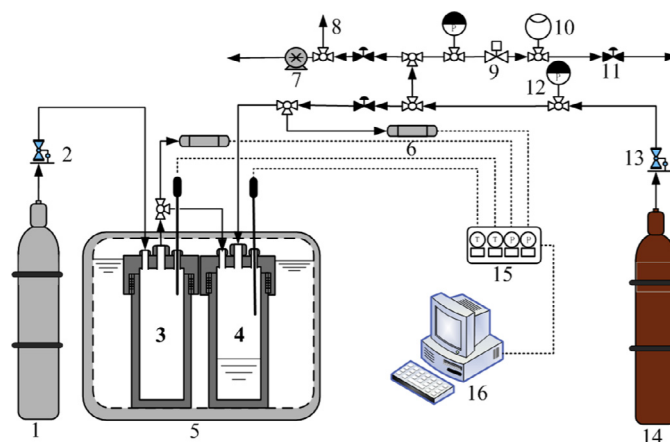


Fig. 2. Schematic of the experimental apparatus.

1-CO₂ cylinder, 2-relief valve; 3-buffer, 4-cell, 5-thermostatic bath, 6-pressure sensor, 7-vacuum pump, 8-sample connection, 9-back pressure valve, 10-mass flow meter, 11-vent valve, 12-pressure gauge, 13-CH₄ relief valve, 14-CH₄ cylinder, 15-data collector, 16-PC.

Fig. 1. CH₄ recovery ratio relied on the initial replacement condition. However, the pressure and composition were changing during the replacement processes and the trend of CH₄-CO₂ exchanging decreased with reaction time.

In this work, we investigated how the pressure and the temperature affect the methane recovery ratio during the replacement processes, considering two steps, the methane hydrate decompose and the CO₂ hydrate formation. Furthermore, the whole process of the trend of CH₄-CO₂ exchange was quantified by calculating the fugacity differences between the gas phase and the hydrate phase for CO₂ and CH₄. The driving force was described by the fugacity differences between the gas phase and the hydrate. The quantification of the driving force was essential to evaluate the kinetics of CH₄ hydrate decomposition and CO₂ hydrate formation.

2. Experimental

2.1. Materials and apparatus description

Methane and carbon dioxide were supplied by the Guangzhou Zhuozheng Gas Industry Corporation, with a stated minimum purity of 99.9 mol%. The purity of SDS was 99%, purchased from Shanghai Biological Technology Co., Ltd. The quartz sand used in the experiment was from Zhengzhou Union Water Co. with a content of 95%. Distilled water was prepared in the laboratory.

A schematic diagram of the experimental apparatus is shown in Fig. 2. The experimental apparatus mainly consists of gas supply module, reaction module and data acquisition module. The gas supply module provides CH₄ and CO₂. The reaction module is used for CH₄ hydrate formation and CH₄-CO₂ exchange included a high pressure reactor (φ44 × 200 mm), a buffer tank and a thermostatic bath (THD-3015, Tianheng Device Co., Ningbo, China). The high pressure reactor and the buffer tank can withstand a maximum pressure of 25 MPa. The system temperature is maintained with an accuracy of 0.1 K using the thermostatic bath. The data acquisition module (Agilent 34970A, Agilent Tech., China) collects the pressure and temperature of the reactor tank and the buffer tank. The gas composition is analyzed by an in-line gas chromatograph (GC9800).

2.2. Procedure

2.2.1. Formation of CH₄ hydrate

A known amount of 0.03 wt% SDS solution and quartz sand were introduced into the high pressure reactor shown in Fig. 2. The

temperature of thermostatic bath was stabilized at 274.2 K. The reactor was then sealed, vacuumed for about 30 min, and charged to CH₄ three to four times to ensure no air. CH₄ gas feed into the reactor to 15 MPa. The data acquisition module recorded the pressure and temperature. Hydrate formation could be considered completed when the experimental pressure was no change for 24 h.

2.2.2. Replacement of CH₄ with gaseous CO₂

After complete formation of the CH₄ hydrate, the temperature of the thermostatic bath adjusted to 271.2 K. The back pressure regulator was set to the desired experimental pressure, and then the free CH₄ in the reactor was released. The gaseous CO₂ was introduced into the reactor. Then, the temperature of thermostatic bath adjusted to the experimental temperature and kept constant. The replacement of CH₄ in the hydrate phase started. The gas composition in the reactor was analyzed by the gas chromatogram during the CO₂-CH₄ replacement reaction. The replacement of CH₄-CO₂ was considered completed when the composition of CH₄ in the gas phase keep stable in 24 h.

2.3. Data processing

The recovery ratio is a very important factor to evaluate CO₂-CH₄ process from the hydrate. The definitions of them as Eq. (1),

$$\eta_{\text{Re}} = \frac{n_{\text{CH}_4, \text{Re}}}{n_{\text{CH}_4, \text{H}}} \times 100\% \quad (1)$$

Where $n_{\text{CH}_4, \text{H}}$ and $n_{\text{CH}_4, \text{Re}}$ are the initial molar quantity of CH₄ in the hydrate phase and the moles of CH₄ displaced in its hydrate, respectively. These can be calculated by Eqs. (2) and (3),

$$n_{\text{CH}_4, \text{H}} = n_{\text{CH}_4, \text{Total}} - n_{\text{CH}_4, \text{G}} \quad (2)$$

$$n_{\text{CH}_4, \text{Re}} = x_{\text{CH}_4, \text{Inter}} n_{\text{Mgas, Inter}} \quad (3)$$

$n_{\text{CH}_4, \text{Total}}$ and $n_{\text{CH}_4, \text{G}}$ stand for the numbers of moles before and after the formation of CH₄ hydrate respectively. And they can be calculated on the basis of the equation of state (EoS), the temperature and pressure in vapor phase which were recorded in the process of CH₄ hydrate formation. $x_{\text{CH}_4, \text{Inter}}$ is the mole fraction of CH₄ in

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