



MHD mixed convection in a lid-driven cavity filled by a nanofluid with sinusoidal temperature distribution on the both vertical walls using Buongiorno's nanofluid model



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ABSTRACT

In the present contribution, a numerical investigation is presented to study Buongiorno's nanofluid model for MHD mixed convection of a lid-driven cavity filled with nanofluid. A sinusoidal temperature and nanoparticle volume fraction distributions on both vertical sides is considered where the horizontal walls are kept adiabatic. The cavity is permeated by an inclined uniform magnetic field and the effects of Brownian motion and thermophoresis are incorporated into the nanofluids model. An accurate collocated finite volume method is employed to discretize the governing partial differential equations after converting them to a non-dimensional form using a suitable transformation variables. Comparisons with previously published work are performed and excellent agreement is obtained. The computation is carried out for wide ranges of the Hartmann number Ha ($0 \leq Ha \leq 100$), buoyancy ratio Nr ($0.1 \leq Nr \leq 1$), thermophoresis number Nt ($0.1 \leq Nt \leq 1$), Brownian motion parameter Nb ($0.1 \leq Nb \leq 1$), Lewis number Le ($1 \leq Le \leq 10$), Prandtl number Pr ($0.054 \leq Pr \leq 10$), inclined magnetic field angle γ ($0^\circ \leq \gamma \leq 3\pi/2$), Amplitude ε ($0 \leq \varepsilon \leq 1.5$), phase angle ξ ($0^\circ \leq \xi \leq 3\pi/4$) and Richardson number Ri ($0.001 \leq Ri \leq 100$). The obtained results are presented in terms of the streamlines, isotherms and nanoparticles volume fraction contours as well as local Nusselt number. Results demonstrate that, the presence of an inclined magnetic field in the flow region leads to lose the fluid movement. Also, the fluid flow is dominated by the movement of the upper wall in the case of the highest values of the buoyancy ratio.

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1. Introduction

Mixed convection heat transfer and fluid flow in cavities with moving lid are important subjects of investigation due to their effect on many engineering applications and nature phenomena especially with nanofluids and MHD. The most usage of the mixed convection flow can be found in atmospheric flows, solar energy storage, heat exchangers, lubrication technologies, drying technologies and cooling of the electronic devices. On the literature survey of this subject; MHD mixed convection with joule heating effect in a lid-driven cavity with a heated semi-circular source was considered by Rahman et al. [1] where the finite element method was used in the solution of the normalized governing equations. It was found that the average Nusselt number can be

decreased with the increasing of the Rayleigh number in the presence of Joule effect. The magnetic field can be a good control parameter for heat transfer and fluid flow. Grosan et al. [2] performed a numerical investigation for steady magnetohydrodynamic free convection in a rectangular enclosure filled with a fluid-saturated porous medium and with internal heat generation. Their results indicated that, the horizontal magnetic field is most effective in suppressing the convection flow for a stronger magnetic field in comparison with the vertical magnetic field. Öztöp et al. [3] studied the MHD mixed convection in a lid-driven cavity with corner heater. From which they could recorded that, the temperature distribution inside the cavity mostly stems from the right side of corner due to impinging air. Also, thermal boundary layer becomes higher with increasing of Hartmann number and isotherms fit with the corner. Hydro-magnetic combined convection in a lid-driven cavity with sinusoidal boundary conditions on both sidewalls was investigated by Sivasankaran et al. [4]. Their study showed; the heat transfer rate increases on increasing the

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Nomenclature

Symbol	Description	Greek Symbols	
B	uniform magnetic field	α	thermal diffusivity, m ² /s
B ₀	magnitude of the magnetic field B	β	coefficient of thermal expansion, K ⁻¹
B _x , B _y	magnetic field component in x, y-axes	γ	magnetic field inclination angle, degree
<i>D</i> _B	Brownian diffusion coefficient	σ	electric conductivity, W/m K
<i>D</i> _T	thermophoretic diffusion coefficient	ε	amplitude
<i>e</i> _x , <i>e</i> _y	unit vectors along the coordinate axis	ξ	phase angle ξ
F	electromagnetic force	θ	dimensionless temperature
<i>g</i>	gravitational acceleration, m/s ²	ϑ	enclosure inclination angle, degree
<i>Gr</i>	Grashof number	ϕ	electric potential
<i>H</i>	length of the cavity, m	ϕ	solid volume fraction of nanoparticles
<i>Ha</i>	Hartmann number	ϕ	dimensionless solid volume fraction of nanoparticles
J	electric current density	ψ	stream function, m ² /s
<i>k</i>	thermal conductivity, W/m K	Ψ	dimensionless stream function
<i>K</i> _r	thermal conductivity ratio	Ω	vorticity function
<i>Le</i>	Lewis number	μ	dynamic viscosity, kg/m s
<i>Nu</i>	local Nusselt number	ρ	density, kg/m ³
<i>Nu</i> _a	average Nusselt number	∇	Laplace operator (dimensional) $\nabla = \partial^2/\partial x^2 + \partial^2/\partial y^2$
<i>Nb</i>	Brownian motion parameter	\blacktriangledown	Laplace operator (dimensionless) $\blacktriangledown = \partial^2/\partial X^2 + \partial^2/\partial Y^2$
<i>Nr</i>	buoyancy ratio		
<i>Nt</i>	thermophoresis number		
<i>P</i>	dimensionless pressure	Subscripts	
<i>p</i>	pressure, Pa	<i>c</i>	cold wall
<i>Pr</i>	Prandtl number	<i>E</i>	east face of the control volume
<i>Ra</i>	Rayleigh number	<i>f</i>	pure fluid
<i>Re</i>	Reynold number	<i>f</i> ₀	reference fluid
<i>Ri</i>	Richardson number	<i>L</i>	left side of the cavity
<i>T</i>	temperature, K	<i>N</i>	north face of the control volume
<i>U</i>	non-dimensional velocity component in X-direction	<i>P</i>	cell location of the control volume
<i>U</i> _p	constant reference speed of the top wall	<i>R</i>	right side of the cavity
<i>u</i>	dimensional velocity component in x-direction, m/s	<i>S</i>	south face of the control volume
<i>V</i>	non-dimensional velocity component in Y-direction	<i>W</i>	west face of the control volume
<i>v</i>	dimensional velocity component in y-direction, m/s	<i>w</i>	wall
<i>X</i>	non-dimensional coordinate in horizontal direction		
<i>x</i>	Cartesian coordinate in horizontal direction, m		
<i>Y</i>	non-dimensional coordinate in vertical direction		
<i>y</i>	Cartesian coordinate in vertical direction, m		

amplitude ratio. Also, the flow behavior and heat transfer rate inside the cavity are strongly affected by the presence of the magnetic field. Kefayati et al. [5] investigated the Lattice Boltzmann simulation of MHD mixed convection in a lid-driven square cavity with linearly heated wall. The results demonstrated that the augmentation of Richardson number causes heat transfer to increase, as the heat transfer decreases by the increment of Hartmann number for various Richardson numbers and the directions of the magnetic field. Effects of moving lid direction of the same problem was considered by Al-Salem et al. [6]. It was recorded that direction of lid is more effective on heat transfer and fluid flow in the case of mixed convection than it is the case in forced convection. Moreover, heat transfer is also decreased with increasing of magnetic field for all studied parameters. Nasrin [7] investigated the influences of physical parameters on mixed convection in a horizontal lid-driven cavity with an undulating base surface using finite element method. The results concluded that the wavy lid-driven cavity can be considered an effective heat transfer mechanism at larger wavy surface amplitude, as well as the number of waves and cavity. Chatterjee [8] studied MHD mixed convection in a lid-driven cavity including a heated source whereas Chatterjee et al. [9] investigated magneto convective transport in a vertical lid-driven cavity including a heat conducting square cylinder with joule heating. Chatterjee's study recorded that the heat transfer rate and bulk fluid temperature are both found to have increasing function of mixed convective strength.

Moreover, it was observed in the second study that the presence of the heat conducting obstacle causes more heat transfer to take place and, furthermore, the square shaped solid object improves the heat transfer rate in comparison to a similar size circular object. Numerical study on mixed convection in an inclined lid-driven cavity with discrete heating can be found by Sivasankaran et al. [10]. In which the high heat transfer was found at cavity inclination angle of $\gamma = 30^\circ$ in the buoyancy convection dominated regime when the heater is located at the middle of the cavity. Khanafer and Aithal [11] considered the problem of laminar mixed convection flow and heat transfer characteristics in a lid driven cavity with a circular cylinder. Their results showed that, for dominant mixed convection, the average Nusselt number increases with an increase in the radius of the cylinder for various Richardson numbers. Ahmed et al. [12] investigated the effect of non-uniform heating on both sidewalls on MHD mixed convection in an inclined lid-driven cavity with opposing thermal buoyancy force. It was indicated that the rate of heat transfer along the heated walls is enhanced on increasing either Hartmann number or inclination angle. Furthermore, the non-uniform heating on both walls provides higher heat transfer rate than non-uniform heating of one wall. A study for mesoscopic simulation of double-diffusive mixed convection of pseudoplastic fluids in an enclosure with sinusoidal boundary condition was done by Kefayati [13] where Selimefendigil and Öztop [14] considered the problem of numerical investigation and dynamical analysis of mixed convection in a

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