



Augmented heat transfer with intersecting rib in rectangular channels having different aspect ratios



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ABSTRACT

This study was an experimental investigation of the effect of an intersecting rib on heat/mass transfer performance in rectangular channels with angled ribs and different aspect ratios. In a rib-roughened channel with angled ribs, heat/mass transfer performance deteriorates as the channel aspect ratio increases, since the vortices induced by angled ribs diminish with increasing aspect ratio. A longitudinal rib that bisects the angled ribs is suggested to overcome this disadvantage. The heat transfer performance of angled rib configurations with a 60° attack angle were tested with and without an intersecting rib using naphthalene sublimation method. The channel aspect ratio is varied from 1 to 4. When the intersecting rib was present, additional vortices were generated at every point of intersection with the angled ribs. Thus the heat/mass transfer performance was significantly enhanced for all channel aspect ratios when an intersecting rib was added to an ordinary angled rib configuration.

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1. Introduction

The operating temperatures of modern gas turbines have been increasing steadily to provide enhanced efficiency and power output. However, metals and other materials have heat resistance temperature limits, and their lifetimes are shortened by higher temperatures. Therefore, the development of cooling techniques for the hot components in a gas turbine is an essential part of gas turbine engine design. The most popular method of cooling the hot components of a turbine (such as nozzle vanes and rotor blades) is internal cooling, which employs internal passages for coolant air to absorb heat from hot components.

In an internal cooling passage, the heat transfer characteristics are mainly dominated by turbulent transport and secondary flow induced by geometrical features. This means that better cooling performance can be obtained by adding to or otherwise modifying the geometry of an internal passage. Certain geometric features, such as ribs [1,2], pin-fins [3–5], protrusions and dimples [6,7], have been investigated as heat transfer intensifiers. In particular, various types of rib configurations have been studied, due to their simplicity and usefulness [8–10].

An ordinary internal passage design is shown in Fig. 1. Serpentine-type multi-passage internal cooling is employed, and

rib turbulators are installed on the internal surfaces of the pressure and suction sides. Since blade thickness varies from the leading edge to the trailing edge, the aspect ratios of the internal passages are different. The fluid flow and heat transfer characteristics of an internal passage are dependent not only on the configuration of rib turbulators, but also on the aspect ratio of the channel. There has been extensive research on the heat transfer performance of rib-roughened channels with various aspect ratios [11–13].

Previous researchers have reported that ribs installed at an acute angle provide better heat transfer performance than orthogonally installed ribs [14]. These angled ribs generate strong secondary vortices adjacent to the channel surface as the flow moves in the direction of the ribs. The vortices sweep the surface, and locally intensified heat transfer occurs in these regions. Moreover, parallel ribs installed on opposite channel surfaces generate a rotational flow, which promotes mixing of the fluid [15,16]. Recently developed gas turbine blades have adopted these angled rib turbulators for improved internal cooling performance. The flow patterns induced by angled ribs are illustrated in Fig. 2.

Unfortunately, as the channel aspect ratio increases, the effect of the secondary vortices induced by angled ribs diminishes due to development of a thermal boundary layer between the ribs, so that the heat transfer performance is degraded [17]. To overcome this deficiency, a new idea is suggested for improving the heat transfer performance of angled ribs in a large-aspect-ratio channel by installing an intersecting rib. The intersecting rib is installed to

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Nomenclature

AR	aspect ratio of channel	\overline{Sh}	spanwise averaged Sherwood number
D_h	hydraulic diameter (mm)	$\overline{\overline{Sh}}$	area averaged Sherwood number
D_{naph}	mass diffusion coefficient of naphthalene vapor in air (m^2/s)	W	duct width (mm)
e	height of rib (mm)	μ	dynamic viscosity (kg/m s)
f	friction factor	ν	kinematic viscosity (m^2/s)
f_0	friction factor of fully developed turbulent flow in a smooth pipe	P	rib-to-rib pitch (mm)
H	channel height (mm)	x	coordinate and distance in the streamwise direction (mm)
k	Thermal conductivity (W/m K)	y	coordinate and distance in the lateral direction (mm)
L	channel length (mm)	z	coordinate and distance in the vertical direction (mm)
Nu	Nusselt number (hD_h/k_c)	h_m	mass transfer coefficient (m/s)
P_{naph}	naphthalene vapor pressure (N/m^2)	\dot{m}	local naphthalene mass transfer rate per unit area ($kg/m^2 s$)
Pr	Prandtl number ($\mu C_p/k$)	η	thermal performance, Eq. (8)
Re_{D_h}	Reynolds number based on hydraulic diameter (UD_h/ν)	ρ_s	density of solid naphthalene (kg/m^3)
R_{naph}	naphthalene gas constant (J/mol K)	$\rho_{(v,w)}$	vapor density of naphthalene on the surface (kg/m^3)
Sc	Schmidt number (ν_{air}/D_{naph})	$\rho_{(v,b)}$	vapor density of bulk air (kg/m^3)
Sh	Sherwood number ($h_m D_h/D_{naph}$)	Δz	sublimation depth of the naphthalene surface (mil)
Sh_0	Sherwood number, Eq. (6)	Δt	running time (s)

cut across both the flow and the angled ribs. The main purpose of this intersecting rib is to break down the developing thermal boundary layer between the angled ribs. The present study is an experimental investigation of the effect of an intersecting rib on the heat transfer characteristics in a rectangular channel with angled ribs. Two sets of rib configurations and three different channel aspect ratios were investigated at fixed Reynolds numbers representing the fully turbulent flow regime. Detailed heat transfer distributions were determined via mass transfer experiments, utilizing the naphthalene sublimation method, and the overall thermal performance of each case was evaluated considering frictional losses.

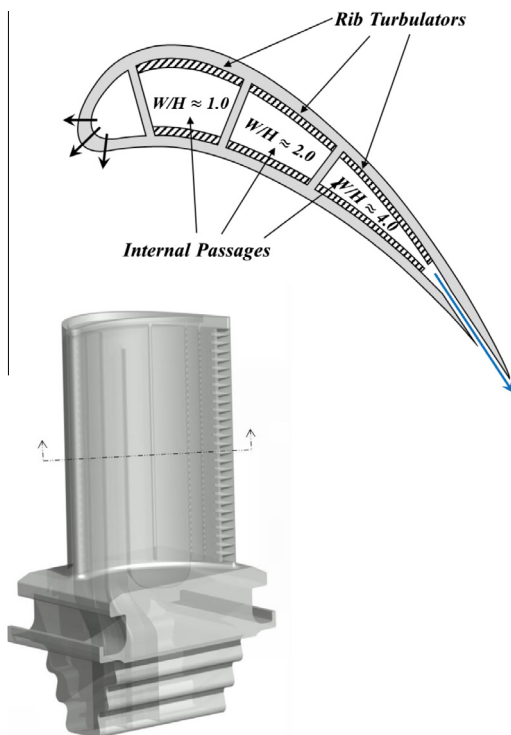


Fig. 1. Blade internal passages of various aspect ratios.

2. Experimental setup and data reduction

2.1. Experimental setup

A schematic overview of the experimental setup used in the present study is shown in Fig. 3. The experiment was carried out in an indoor laboratory, where the air temperature was held constant by the air conditioning system. The test facility was composed of an air blower, a heat exchanger with a constant-temperature water bath, an orifice flow meter, a plenum, a test channel and a monitoring computer. The airflow rate was controlled by the frequency inverter used to regulate the speed of the air blower, and the flow rate was measured by the orifice flow meter. The air discharged from the blower passed through

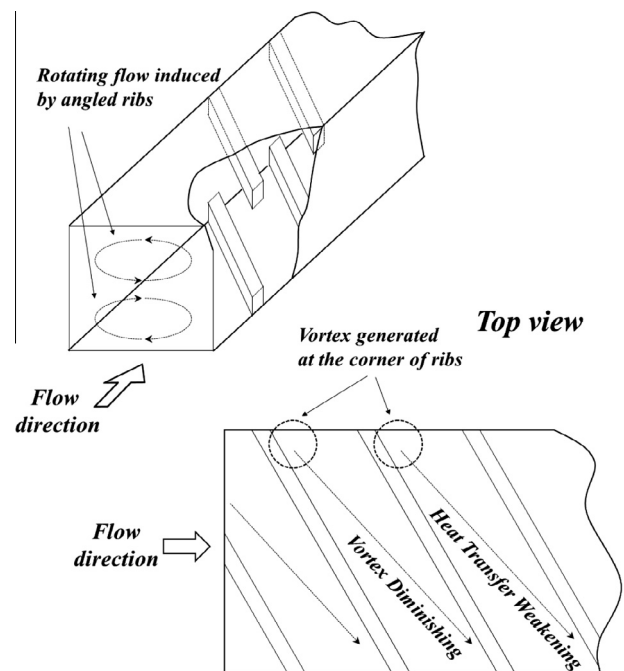


Fig. 2. Flow pattern induced by angled ribs.

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