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² Original Research Paper

Steady-shear magnetorheological response of fluids containing $\frac{7}{5}$ solution-combustion-synthesized Ni-Zn ferrite powder

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ABSTRACT

Magnetically soft nickel-zinc ferrite $(Ni_{0.5}Zn_{0.5}Fe_2O_4)$ powder with high saturation magnetization was 29 synthesized by solution combustion route using metal pitrate as precursors and glycine as fuel. The parsynthesized by solution combustion route using metal nitrate as precursors and glycine as fuel. The particles were found to have irregular morphology. Three different magnetorheological fluids (MRFs) were 31 prepared by dispersing 10, 20 and 40 wt% of these particles in thin silicone oil. The behaviour of the 32 MRFs was studied under steady shear conditions at different applied magnetic field strengths (B). The 33 yield strength (τ_Y) and viscosity (η) of all the MRFs were found to increase with B and particle fill fraction 34
 ϕ while the response of the MRFs was strongly influenced due to the morphology microstructure and 3 /, while the response of the MRFs was strongly influenced due to the morphology, microstructure and 35 saturation magnetization of the particles. Owing to the low density of the particles, the observed off-
36 state viscosity is high. However, the excellent thermo-oxidative and chemical stabilities of these mag- 37 netic oxide particles than metallic magnetic particles make these MRFs dependable for applications in 38 harsh working environments. In addition, the low cost and feasibility of large scale preparation of these 39 magnetic oxides makes these MRFs further attractive for industrial applications. 40

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46 1. Introduction

 Magnetorheological fluids (MRFs) are smart fluids which have the ability to tune their viscosity reversibly in split-second time, via an externally applied magnetic field. This unique ability makes the MRFs useful for applications involving mechanical shock miti- gation and vibration damping, without any permanent failure. The most relevant magnetorheological parameter deciding the effi- ciency of mechanical impact addressal is the yield strength devel- oped in the MRF on magnetic activation. Conventionally, a high yield strength value can be expected from the MRFs containing metallic magnetic (Fe, Co, Ni or their alloys) particles having high 57 saturation magnetization $[1-5]$. However, MRFs containing these metallic particles suffer from poor dispersion stability and extre- mely difficult redispersibility post-sedimentation in carrier fluid as well as chemical instability in ambience/work environments. Although there are methods to circumvent these issues by making 62 use of additives to MRFs $[6-12]$ or coating the particles $[13-17]$, these deteriorate the magnetic properties of particles leading to a decrease in speed of response of the MRF. Moreover, cumbersome synthesis [\[3,4,18–21\]](#page--1-0) and stringent conditions of preservation of

the functional magnetic particles add to the cost of such MRFs, lim- 66 iting the feasibility of their industrial scale usage. 67

Hence, in our present work, we investigate the magnetorheo-
68 logical response of MRFs containing an alternate magnetic oxide 69 powder, i.e., Ni-Zn ferrite particles. The interest in choice of 70 Ni-Zn ferrite powder is due to its excellent chemical and thermo-

71 oxidative stabilities and low mass-density (which eliminates the 72 need of additives or coating agents in the MRF). Furthermore, this 73 method of production is highly economical with low (a few min- 74 utes) production time, which is industry-friendly. Unlike metallic 75 (such as Fe) particles, the preservation of the Ni-Zn ferrite sample 76 is easy. In addition to the fact that synthesis of Ni-Zn ferrite by 77 solution combustion technique [\[22,23\]](#page--1-0) needs no sophisticated 78 techniques, it is a reproducible method which uses low-cost 79 precursors. In this study, we have chosen a specific composition, 80 $Ni_{0.5}Zn_{0.5}Fe₂O₄$, due to its best magnetic properties (compared to 81) all other compositions of Ni-Zn ferrites) in terms of saturation 82 magnetization and magnetic softness [\[24\]](#page--1-0). 83

Besides their good magnetorheological property, the MRFs con- 84 taining ferrimagnetic oxide particles also show enhanced disper- 85 sion stability against sedimentation due to their low density. 86 There are noteworthy works on magnetorheological fluids based 87 on calcium ferrite nano-crystal clusters [\[25\]](#page--1-0), manganese ferrite/- 88

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89 graphene oxide nanocomposites $[26]$ and highly magnetic zinc fer-90 rite nano-crystal clusters [\[27\].](#page--1-0)

 In the forthcoming sections, we discuss the synthesis procedure of Ni-Zn ferrite powder and their structural, morphological and magnetic properties. This is succeeded by the preparation of MRFs and their magnetorheological characterization under steady-state shear conditions, at different applied magnetic field strengths. The magnetorheological parameters viz. yield strength, ratios of on-state to off-state viscosities of MRFs, their significance and the relationship between these parameters to particle microstruc-ture and magnetic nature are discussed.

100 2. Materials and methods

101 2.1 Synthesis of $Ni_{0.5}Zn_{0.5}Fe₂O₄$ powder and preparation of MRFs

 Ni-Zn ferrite powders of different compositions can be synthe-103 sized by various methods [28-36], however, the choice of synthesis depends on the required physical and magnetic properties of the product phase. Solution combustion method initially employed 106 by Hwang et al [\[37\]](#page--1-0) was a two-step process, which involves an ini- tial sol–gel auto-ignition process followed by calcination at an ele- vated temperature to obtain crystalline ferrite powder with high 109 saturation magnetization (M_S) . The process followed in the present synthesis method is a one-step process. In this method, stoichio- metric amounts of the precursors (the oxidizer and fuel) were taken. The precursor mixture was magnetically stirred in a borosil 113 container on a hot plate (temperature not exceeding $95 °C$) with minimum water content until bubbling, after which the container was transferred to a pre-heated muffle furnace, maintained at \sim 500 (\pm 25) °C. The combustion reaction directly occurs at 500
117 °C. The oxidizers were the metal nitrates and the fuel was glycine ^oC. The oxidizers were the metal nitrates and the fuel was glycine. The choice of glycine as fuel was due to the more negative combus-119 tion heat $(-3.24 \text{ kcal g}^{-1})$ as compared to other fuels such as urea $(-2.98 \text{ kcal g}^{-1})$ and citric acid $(-2.76 \text{ kcal g}^{-1})$] [\[38\].](#page--1-0) In the above synthesis, the total metal nitrate to fuel mass ratio was 3:4.44. This ratio of oxidizer to fuel necessitates no external supply of oxygen [\[37\]](#page--1-0). The balanced equation for the reaction to obtain two $Ni_{0.5}$ $Zn_{0.5}Fe₂O₄$ powder is given below. 125

$$
\frac{1}{2}Ni(NO_3)_2 \cdot 6H_2O + \frac{1}{2}Zn(NO_3)_2 \cdot 6H_2O + 2Fe(NO_3)_3
$$

\n
$$
\cdot 9H_2O + \frac{40}{9}NH_2CH_2COOH \stackrel{\Delta}{\rightarrow} Ni_{0.5}Zn_{0.5}Fe_2O_4
$$

\n127
$$
\times \frac{80}{9} + CO_2 + \frac{100}{9}H_2O + \frac{20}{9}N_2
$$

 The combustion reaction proceeded with visible flares and the reaction got completed by about 10–15 s after the initiation of reaction. Following this, the furnace was switched off and the foamy product formed was allowed to cool naturally inside the fur- nace. The fluffy product formed was ground well using agate mor-133 tar and pestle before characterization. The obtained $\text{Ni}_{0.5}\text{Zn}_{0.5}\text{Fe}_2\text{O}_4$ powder was labelled as NZFP.

135 MRFs were prepared by dispersing 10, 20 and 40 wt% (weight 136 fractions $\phi = 0.1$, 0.2 and 0.4) of the NZFP particles in silicone oil 137 without any additives. The kinematic viscosity of silicone oil is 138 \sim 140 cSt with a specific density of (ρ) 0.96 g/cc. The MRFs were
139 **14belled as NZFP-10. NZFP-20. NZFP-40.** respectively. The MRF labelled as NZFP-10, NZFP-20, NZFP-40, respectively. The MRF 140 samples were homogenized by mechanical mixing and ultrasoni-141 cation for \sim 15 min before magnetorheological characterizations.

142 2.2 Characterization of $Ni_{0.5}Zn_{0.5}Fe₂O₄$ powder and MRFs

143 The NZFP sample was characterized by X-ray diffraction (XRD) 144 using a **PANalytical X'Pert Pro** diffractometer (λ = 1.540 Å). The phase purity ($Ni_{0.5}Zn_{0.5}Fe₂O₄$) was confirmed by performing Riet- 145 veld refinement $\left[39\right]$ of XRD pattern using **FullProf** $\left[40\right]$ and rele- 146 vant structural information were obtained. The structural and 147 magnetic properties of sample were characterized by 57 Fe Möss- 148 bauer spectroscopy at RT in transmission mode. The Mössbauer 149 spectra were least square fit using the computer program **NORMOS** 150 $[41,42]$. The morphological characterization of sample was carried 151 out by scanning electron microscopy (SEM). The magnetic property 152 of sample was characterized using **PPMS 14 T Quantum Design** 153 magnetometer at RT. 154

Steady state shear response of all MRF samples (NZFP-10, NZFP- 155 20 and NZFP-40) were carried out using *Physica MCR* 301 (Anton 156 Paar) rheometer, augmented with magnetorheological cell (MRD 157 70/1T). The magnetorheometer was operated in parallel plate 158 geometry with a shear plate of diameter \sim 20 mm. The direction 159
of magnetic field was normal to the shear plane, with maximum 160 of magnetic field was normal to the shear plane, with maximum field strength of 1.2 T. Using water circulation, the temperature 161 of MRF was maintained at RT $(28 \pm 1 \degree C)$. 162

Before each test, the MRF sample was homogenized by shearing 163 at a rate of $100 \, \text{s}^{-1}$ for \sim 5 min. The sample height was confined to $\frac{164}{100}$ = $\frac{164}{100}$ = $\frac{165}{100}$ 0.3 mm during the entire experiment. The detailed method of mag-netorheological characterization is provided elsewhere [\[43\]](#page--1-0). The 166 applied field strengths (B) were 0.0, 86.5, 181.5, 365.2, 956.3 and 167 1200 mT. The corresponding shear stress (τ) and viscosity (η) val- 168 ues were recorded simultaneously, as a function of shear rate (γ) , 169 for each B. The maximum applied shear rate was limited to 1000 170 s^{-1} to avoid expulsion of the MRF at higher shear rates. 171

3. Results and discussion 172

The XRD pattern ([Fig. 1](#page--1-0)(a)) confirmed the formation of pure 173 phase spinel ($Fd\overline{3}m$) structured Ni_{0.5}Zn_{0.5}Fe₂O₄. The Miller indices 174 corresponding to the Bragg reflections of the XRD pattern are 175 shown in Fig. $1(a)$. The Rietveld refinement of cation occupancy 176 confirmed the stoichiometric phase. The lattice parameter (a) and 177 crystallite size (L) determined by applying Scherrer formula (for 178 (311) Bragg peak of NZFP) are 8.4399 Å and 34.2 nm, respectively. 179 The X-ray density of NZFP sample was \sim 5.2 g/cc. 180
The Mössbauer spectrum of NZFP sample (Fig. 1(b)) shows two 181

The Mössbauer spectrum of NZFP sample (Fig. $1(b)$) shows two magnetically split sextets with different isomer shift (δ) values 182 ([Table 1\)](#page--1-0), which correspond to the presence of Fe atoms at the 183 tetrahedral (Th) and the octahedral (Oh) sites. Other spectral 184 parameters such as magnetic hyperfine field (B_{bf}) and subspectral 185 area ratios and line width (Γ) are listed in [Table 1](#page--1-0), which confirm 186 the phase pure $Ni_{0.5}Zn_{0.5}Fe₂O₄$ sample. The ratio of subspectral 187 areas (Th/Oh) confirmed the stoichiometry of the sample. 188

The scanning electron micrograph for NZFP sample $(Fig, 1(c))$ 189 shows irregular shaped, network structured powder particles with 190 approximate particle size of \sim 100–1000 nm. The foamy network 191
structure is formed due to the evolution of gases during the comstructure is formed due to the evolution of gases during the combustion process and during drying/shrinkage of the slurry post 193 combustion. Evolution of higher amount of gases makes the struc- 194 ture porous $[44-50]$. However, at the synthesis temperature 195 $(\sim 500 \degree C)$, the coalescence of finer particles is difficult to achieve, 196
especially in ferrites. Furthermore, in solution combustion method. 197 especially in ferrites. Furthermore, in solution combustion method, it is very difficult to control the size/shape of the particles, rather 198 the crystallite size can be tuned using different solvents, fuel to 199 oxidizer ratios and temperatures of the reaction $[22]$. The higher 200 synthesis temperature (\sim 500 °C) facilitates in improving the mag-
netic properties (increased saturation magnetization) [37]. 202 netic properties (increased saturation magnetization) [\[37\].](#page--1-0)

The M-H loop of NZFP sample (Fig. $1(d)$) shows soft magnetic 203 nature of the samples with high M_S value (~62.4 emu/g), narrow 204
hysteresis loop (low H_c \approx 40.4 Oe and M_R \approx 3.7 emu/g) along with 205 hysteresis loop (low H_C \approx 40.4 Oe and M_R \approx 3.7 emu/g) along with 205
high value of mass susceptibility ($\gamma_m \approx 86.8$ emu/g kOe). 206 high value of mass susceptibility ($\chi_{\rm m} \approx 86.8$ emu/g kOe).

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